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HOFFMAN MARITIME CONSULTANTS INC GLEN HEAD NY  
USER MANUAL FOR PROGRAM SCOMOT SECOND PART OF U.S.C.G. SHIP MOT--ETC(U)  
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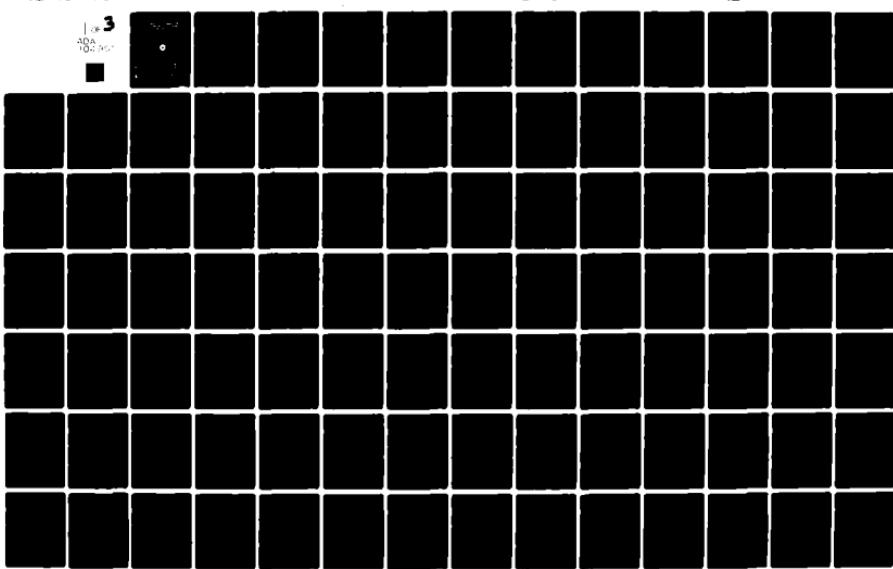
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REPORT NO. CG-M-11-80 ✓

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# USER MANUAL FOR PROGRAM SCOMOT —SECOND PART OF COAST GUARD SHIP MOTION PROGRAM

Thomas E. Zielinski

Hoffman Maritime Consultants



FEBRUARY 1981  
FINAL REPORT

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U.S. DEPARTMENT OF TRANSPORTATION  
UNITED STATES COAST GUARD  
OFFICE OF MERCHANT MARINE SAFETY  
WASHINGTON, D.C. 20593

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(18) USCG-M (19) 11-64

Technical Report Documentation Page

|   |                                      |   |
|---|--------------------------------------|---|
| 1. Report No.   | 2. Government Accession No.          | 3. Recipient's Catalog No.  |
| G-M-11-80   | FD-A304951                           |   |
| 4. Title and Subtitle   |                                      | 5. Report Date  |
| User Manual for Program SCOMOT<br>Second Part of U.S.C.G. Ship Motion Program   |                                      | February 1981   |
| 6. Performing Organization Code   |                                      | 11  |
| 7. Author(s)  |                                      | 7. Author(s)  |
| 12 Thomas E. Zielinski  |                                      | 14 HMC-80161A/  |
| 8. Performing Organization Name and Address   |                                      | 10. Work Unit No. (TRAIS)   |
| Hoffman Maritime Consultants Inc.<br>9 Glen Head Road<br>Glen Head, New York 11545  |                                      | 15  |
| 12. Sponsoring Agency Name and Address  |                                      | 11. Contract or Grant No.   |
| Commandant (G-MMT-4/13)<br>U.S. Coast Guard<br>2100 2nd St., S.W.<br>Washington, D.C. 20593   |                                      | DOT-CG-958905-A   |
| 15. Supplementary Notes   |                                      | 13. Type of Report and Period Covered   |
| Program SCOMOT is proprietary software. It has been made available to the U.S.C.G. and is intended for their internal use. (Ref: Contract CG-74080-B dgc)   |                                      | 9 Final Manual  |
| 16. Abstract  |                                      |   |
| A description of program SCOMOT, the second part of the revised and enhanced SCORES program is presented, with the theoretical basis, organization and structure, data input and output formats described. A sample computation using the SL-7 containership is included to aid in the understanding of the input and output formats. This program computes the six-degree of freedom ship motions of heave, pitch, surge, sway, yaw and roll and wave induced sea loads of vertical bending moment and shear force, lateral bending moment and shear force and torsion for a ship advancing at constant speed. The transfer functions for a range of frequency and wave headings are calculated. A variety of spectral definitions ranging from an analytical formulation of the Bretschneider type, to measure spectra, to a hindcast and forecast data can be accepted as a single spectrum or families of spectra divided into wave height groups. Both short term and long term analysis for all responses are performed, and in addition slamming and shipping of water statistics presented. |                                      |   |
| 17. Key Words   |                                      | 18. Distribution Statement  |
| Ship motion, RAO's, linear superposition transfer functions, wave induced sea loads spectral families, hindcast, forecast slamming, shipping of water, point motions SL-7   |                                      | This document is available to the U.S. public through the National Technical Information Service, Springfield, Virginia 22161 |
| 19. Security Classif. (of this report)  | 20. Security Classif. (of this page) | 21. No. of Pages  |
| Unclassified  | Unclassified                         | 62 Text<br>129 Appendix   |
| 22. Price   |                                      |   |

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This User Manual for Program SCOMOT is for public release. The software part of Project SCOMOT is proprietary and is not included in this document. It will be released in three years per Mr. Paul Cojeen, USCG/Office of Merchant Marine Safety.

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| 4. Inspection         | <input type="checkbox"/>            |
| 5. Other              | <input type="checkbox"/>            |
| 6. Distribution       | <input type="checkbox"/>            |
| 7. Availability Codes | <input type="checkbox"/>            |
| 8. All other          | <input type="checkbox"/>            |
| 9. Other              | <input type="checkbox"/>            |
| Initials _____        |                                     |

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**SCOMOT Program - User Manual  
Record of Changes**

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|      |                       |      |             |

Abstract

A description of SCOMOT, the second part of the revised SCORES program, developed by Hoffman Maritime Consultant Inc. (HMC) for use by the U.S. Coast Guard, is presented. This program computes the six-degree-of-freedom ship motions and wave induced sea loads for a ship advancing at constant speed in both regular or irregular waves. Program theory, organization and structure, data input and output formats are described. A sample computation using the SL-7 containership is included to aid in the understanding of input and output formats.

## I. INTRODUCTION

Program SCOMOT is the second half of the new modified SCORES Program (1)\* which predicts ship motions and dynamic loads for a vessel in both a regular and an irregular seaway. The basic input for this procedure, the geometric, weight, and two-dimensional hydrodynamic properties, is prepared by Program STATIC (2). Three levels of vessel responses are calculated:

1. Response Amplitude Operators (RAO)
  - Response to regular sinusoidal waves
2. Short Term Results
  - Response to irregular waves
3. Long Term Results
  - Extrapolation of short term results using a combined Normal and Rayleigh distributions

The motions of displacement, velocity, and acceleration can be calculated for heave, pitch, surge, sway, yaw, and roll as well as for any specific location. The dynamic loads of vertical and lateral shear forces, bending moments and torsional moments are computed. Slamming, shipping of water and propeller racing statistics are available.

Program SCOMOT is a separate program in the modified SCORES procedure, with a stand alone capability. The lengthy calculation of the two-dimensional properties (TDP) in Program STATIC is performed prior to the motion computations.

SCOMOT is written in the FORTRAN IV language, checked out and run on the United Computing Services (UCS) CDC-6600 Computer System.

The method of analysis is outlined below in Section II. The input scheme and data preparation is described in Section III.

\*Numbers in parentheses refer to list of references at end of this report.

Typical runs showing input and output formats are shown in Section IV using the Sealand 7 containership. Section V contains error messages and their meaning as well as typical running times for various tasks.

## II. OUTLINE OF THEORY

The basic analysis used in SCOMOT can be divided into three topics:

- A. Response Amplitude Operators
- B. Short Term Analysis
- C. Long Term Extrapolation

Each of these areas will be discussed in the following sections.

### A. Response Amplitude Operators

Since the original work was performed nearly ten years ago, (3) SCORES has undergone many changes and modifications. The updated theory will be presented in this section.

The ship is considered to be advancing at a constant forward speed with arbitrary heading in regular sinusoidal waves. It is assumed that the six-degree-of-freedom motions are linear and harmonic and that for a given ship speed, heading angle and frequency of encounter,  $\omega_e$  the motion displacements are

$$\delta_i = a_i \cos(\omega_e t - \epsilon_i) \quad i = 1 \dots 6 \quad [1]$$

where  $a_i$  is the amplitude of the motion

with  $\delta_i = 1 \dots 6$  referring to heave, pitch, surge, sway, yaw and roll respectively. The right handed coordinate system is shown in Figure 1 with the x-axis positive forward, y-axis to starboard, and z-axis positive, downwards with the origin G at the ship's center of gravity.

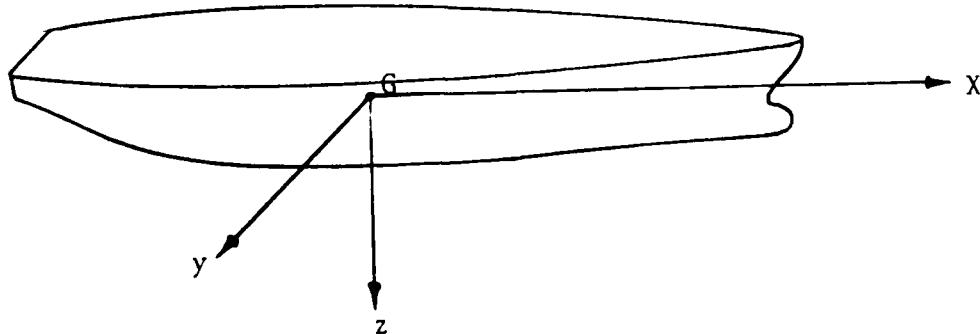


Figure 1.

A ship advancing through regular sinusoidal waves at a constant forward speed  $V$ , and heading angle  $\beta$  will have an encounter frequency,  $\omega_e$ , of

$$\omega_e = \omega - \frac{\omega^2 V}{g} \cos\beta \quad [2]$$

where  $\omega$  is the wave frequency,  $g$  is the acceleration of gravity and  $\beta$  is the heading angling with  $0^\circ$  being following seas and  $180^\circ$  head seas, as shown in Figure 2.

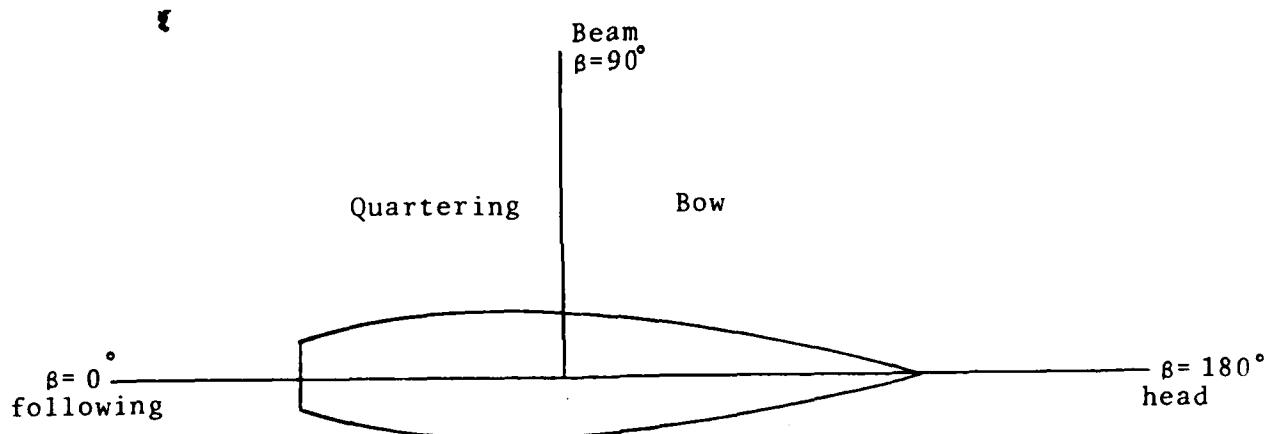


Figure 2.

Under the assumptions that the responses are linear and harmonic the six linear coupled differential equations of motion can be written using subscript notation as follows:

[3]

$$\sum_{k=1}^6 [(M_{jk} + A_{jk})\ddot{\delta}_k + B_{jk}\dot{\delta}_k + C_{jk}\delta_k] = F_j e^{i\omega_e t} \quad j=1\dots 6$$

where  $M_{jk}$  generalized mass matrix

$A_{jk}$  added mass coefficient

$B_{jk}$  damping coefficient

$C_{jk}$  hydrostatic restoring coefficient

$F_j$  exciting forces  
 $\delta_k$  velocity  
 $\ddot{\delta}_k$  acceleration

If there is lateral symmetry and the center of gravity is located on the centerline, the six coupled equations of motion [3] reduce to two sets of three coupled equations. The vertical plane equations for heave, pitch and surge can be written as follows:

$$\sum_{k=1}^3 [(M_{jk} + A_{jk})\ddot{\delta}_k + B_{jk}\dot{\delta}_k + C_{jk}\delta_k] = F_j e^{i\omega_e t} \quad j = 1, 2, 3 \quad [4]$$

and the lateral plane of sway, yaw, and roll as

$$\begin{aligned} \sum_{k=4}^6 & [(M_{jk} + A_{jk})\ddot{\delta}_k + B_{jk}\dot{\delta}_k + C_{jk}\delta_k] \\ & = F_j e^{i\omega_e t} \quad j = 4, 5, 6 \end{aligned} \quad [5]$$

### 1. Vertical Plan Equations

The coupled equations for heave,  $\delta_1$  (positive downward), pitch,  $\delta_2$  (positive bow up) and surge  $\delta_3$  (positive forward) are given below:

$$\begin{aligned} & [M + A_{11}]\ddot{\delta}_1 + B_{11}\dot{\delta}_1 + C_{11}\delta_1 + A_{12}\ddot{\delta}_2 + B_{12}\dot{\delta}_2 + C_{12}\delta_2 + \\ & A_{13}\ddot{\delta}_3 + B_{13}\dot{\delta}_3 + C_{13}\delta_3 = Z_w \end{aligned}$$

$$\begin{aligned} & A_{21}\ddot{\delta}_1 + B_{21}\dot{\delta}_1 + C_{21}\delta_1 + [I_2 + A_{22}]\ddot{\delta}_2 + B_{22}\dot{\delta}_2 + C_{22}\delta_2 + \\ & A_{23}\ddot{\delta}_3 + B_{23}\dot{\delta}_3 + C_{23}\delta_3 = M_w \end{aligned}$$

$$\begin{aligned} & A_{31}\ddot{\delta}_1 + B_{31}\dot{\delta}_1 + C_{31}\delta_1 + A_{32}\ddot{\delta}_2 + B_{32}\dot{\delta}_2 + C_{32}\delta_2 + \\ & [M + A_{33}]\ddot{\delta}_3 + B_{33}\dot{\delta}_3 + C_{33}\delta_3 = X_w \end{aligned}$$

[6]

where  $Z_w$ ,  $M_w$ , and  $X_w$  are the exciting forces for heave, pitch, and surge respectively..

Using strip theory the coefficients for these equations are calculated by integrating the two dimensional hydrodynamic properties from Program STATIC. These coefficients are defined as follows:

$$A_{11} = \int A'_{33} dx$$

$$B_{11} = \int N'_z dx - V \int \frac{dA'_{33}}{dx} dx$$

$$C_{11} = \rho g \int B^* dx - V \int \frac{dN'_z}{dx} dx$$

$$A_{12} = - \int_x A'_{33} dx$$

$$B_{12} = - \int_x N'_z dx + V \int_x \frac{dA'_{33}}{dx} dx + 2V \int A'_{33} dx - \frac{V^2}{\omega_c^2} \int \frac{dN'_z}{dx} dx$$

$$C_{12} = - \rho g \int_x B^* dx - V^2 \int \frac{dA'_{33}}{dx} dx + 2V \int N'_z dx + V \int_x \frac{dN'_z}{dx} dx$$

$$A_{13} = 0.0$$

$$B_{13} = 0.0$$

$$C_{13} = 0.0$$

$$A_{21} = - \int x A'_{33} dx$$

$$B_{21} = - \int x N'_z dx + V \int x \frac{dA'_{33}}{dx} dx$$

$$C_{21} = - \rho g \int x B^* dx + V \int x \frac{dN'_z}{dx} dx$$

$$A_{22} = \int x^2 A'_{33} dx$$

$$B_{22} = \int x^2 N_z' dx - V \int x^2 \frac{dA_{33}'}{dx} dx - 2V \int x A_{33}' dx - \frac{V^2}{\omega_e^2} \int x \frac{dN_z'}{dx} dx$$

$$C_{22} = \rho g \int x^2 B^* dx + V^2 \int x \frac{dA_{33}'}{dx} dx - 2V \int x N_z' dx - V \int x^2 \frac{dN_z'}{dx} dx$$

$$A_{23} = (KG - KB) A_{33}$$

$$B_{23} = (KB - KG) B_{33}$$

$$C_{23} = 0.0$$

$$A_{31} = 0.0$$

$$B_{31} = 0.0$$

$$C_{31} = 0.0$$

$$A_{32} = (KG - KB) A_{33}$$

$$B_{32} = (KG - KB) B_{33}$$

$$C_{32} = 0.0$$

$$A_{33} = \int A_x' dx$$

$$B_{33} = \left( \frac{dR_t}{dv} \right)_{V=v_0} + \int N_x' dx$$

$$C_{33} = 0.0$$

M = ship's mass

$$I_2 = \text{longitudinal mass moment of inertia} = k_{yy}^2 M$$

where  $A_{33}'$  - Sectional heave added mass (from STATIC)

$A_x'$  - Sectional surge added mass

$B^*$  - Local section beam (from STATIC)

$N_x'$  - Sectional surge damping

$N_z'$  - Sectional heave damping (from STATIC)

|          |                                  |
|----------|----------------------------------|
| V        | - Ship's velocity                |
| $k_{yy}$ | - pitch or longitudinal gyradius |
| $\rho$   | - Mass density                   |
| g        | - acceleration of gravity        |

All the integrations are over the length of the ship.

The wave excitation, the right hand side of equation [6] is given by

$$z_w = \int \frac{dz_w}{dx} dx$$

$$M_w = \int x \frac{dz_w}{dx} dx + \int \frac{dx_w}{dx} (\bar{z} + OG) dx \quad [8]$$

$$x_w = \int \frac{dx_w}{dx} dx$$

The local sectional vertical wave force acting on the ship section is represented as:

$$\frac{dz_w}{dx} = - \frac{D}{Dt} [ (A'_{33} + N'_z) \dot{n} ] e^{-kh} - \rho g B^* n e^{-kh} \quad [9]$$

where  $n$  is the surface wave elevation, positive upwards, and is defined in complex form as follows:

$$n = A i e^{-i(-kx \cos \beta + ky \sin \beta + \omega t)} \quad [10]$$

where  $k$  is the wave number and  $\beta$  is the wave heading angle. This expression [9] for local vertical wave force is expanded to the following form:

$$\frac{dz_w}{dx} = - [(\rho g B^* - \frac{\omega}{\omega_e} V \frac{dN'_z}{dx}) n + (N'_z \frac{\omega}{\omega_e} - V \frac{dA'_{33}}{dx}) \dot{n} + A'_{33} \ddot{n}] e^{-kh} \quad [11]$$

where  $h$  is the mean section draft. In a similar manner the local longitudinal wave excitation force is as follows:

$$\frac{dx_w}{dx} = -akge^{-kh} \cos\beta S(x) \cos(-kx \cos\beta + \omega_e t) \quad [13]$$

where  $S(x)$  = local sectional area

The wave induced vertical shear force and bending moment at any location  $x_0$  along the ship's length is as follows:

$$SF_z(x_0) = \left[ \int_{x_s}^{x_0} \text{or} \int_{x_0}^{x_b} \right] \frac{df_z}{dx} dx$$

$$BM_z(x_0) = \left[ \int_{x_s}^{x_0} \text{or} \int_{x_0}^{x_b} \right] \left[ (x-x_0) \frac{df_z}{dx} - (z + \bar{OG}) \left( -m\ddot{\delta}_3 + \frac{dx_h}{dx} + \frac{dx_w}{dx} \right) \right] dx \quad [14]$$

where

$$\frac{df_z}{dx} = -m(\ddot{\delta}_1 - x\ddot{\delta}_2) + \frac{dz_h}{dx} + \frac{dz_w}{dx} \quad [15]$$

$m$  = local section mass

$\bar{z}$  = local sectional center of buoyancy, from waterline

and

$$\frac{dz_h}{dx} = V \frac{dA'_{33}}{dx} (\dot{\delta}_1 - x\dot{\delta}_2 + V\delta_2) + V \frac{dN'_z}{dx} (\dot{\delta}_1 - x\dot{\delta}_2 - V\dot{\delta}_2 / \omega_e^2)$$

$$-A'_{33}(\ddot{\delta}_1 - x\ddot{\delta}_2 + 2V\dot{\delta}_2) - N'_z(\dot{\delta}_1 - x\dot{\delta}_2 + 2V\delta_2) \quad [16]$$

$$\frac{dx_h}{dx} = A'_x [\ddot{\delta}_3 + (KG-KB) \ddot{\delta}_2] + \left[ \left( \frac{1}{L} \left( \frac{dR_t}{dv} \right) \right)_{V=v_0} + N'_x \right] [\dot{\delta}_3 + (KG-KB) \dot{\delta}_2]$$

[17]

## 2. Lateral Plane Equations

The coupled equations of motion for sway,  $\delta_4$ , (positive to starboard), yaw,  $\delta_5$ , (positive bow-starboard), and roll,  $\delta_6$ , (positive starboard down) are given as:

$$M\ddot{\delta}_4 = \int \frac{dYh}{dx} dx + Y_w \quad [18]$$

$$I_z \ddot{\delta}_6 - I_{xz} \ddot{\delta}_5 = \int \frac{dYh}{dx} x dx + N_w \quad [19]$$

$$I_x \ddot{\delta}_6 - I_{xz} \ddot{\delta}_5 = \int \frac{dKh}{dx} dx - Mg \overline{GM} \delta_6 + K_w \quad [20]$$

where

$$\begin{aligned} I_z &= \text{mass moment of inertia of ship about z-axis (yaw)} \\ &= k_z^2 M \end{aligned}$$

$$k_z = \text{yaw radius of gyration}$$

$$\begin{aligned} I_x &= \text{mass moment of inertia of ship about x-axis (roll)} \\ &= k_x^2 M \end{aligned}$$

$$k_x = \text{roll radius of gyration}$$

$$\begin{aligned} I_{xz} &= \text{mass product of inertia of ship in x-z plane} \\ &= k_{xz}^2 M \end{aligned}$$

$$k_{xz} = \text{roll-yaw radius of gyration}$$

$$\frac{dYh}{dx} = \text{local sectional lateral hydrodynamic force}$$

$$\frac{dKh}{dx} = \text{local sectional hydrodynamic rolling moment}$$

$$Y_w, N_w, K_w = \text{wave excitation force and moments}$$

$$\overline{GM} = \text{initial metacentric height}$$

The hydrodynamic sway force is as follows:

$$\begin{aligned} \frac{dYh}{dx} &= \frac{-D}{dt} [(M_s + \frac{N_s}{i\omega_e}) (\dot{\delta}_4 + x\dot{\delta}_5 - V\delta_5)] + \frac{D}{dt} [(F_{rs} + \frac{N_{rs}}{i\omega_e}) \dot{\delta}_5] \\ &\quad + \overline{OG} \frac{D}{dt} [(M_s + \frac{N_s}{i\omega_e}) \dot{\delta}_6] \end{aligned} \quad [21]$$

This is expanded to give:

$$\frac{dYh}{dx} = V \frac{dM_s}{dx} (\dot{\delta}_4 + x\dot{\delta}_5 - V\delta_5) + V \frac{dN_s}{dx} (\dot{\delta}_4 + x\dot{\delta}_5 + \frac{V}{\omega_e^2} \dot{\delta}_6) \quad [22]$$
$$- M_s (\ddot{\delta}_4 + x\ddot{\delta}_5 - 2V\dot{\delta}_5) - N_s (\delta_4 + x\delta_5 - 2V\delta_5) + \delta_6 (F_{rs} + \overline{OG} M_s)$$
$$+ \delta_6 [N_{rs} + OG N_s - V(\frac{dF_{rs}}{dx} + \overline{OG} \frac{dM_s}{dx})] - \delta_6 V (\frac{dN_{rs}}{dx} + \overline{OG} \frac{dN_s}{dx})$$

where  $\overline{OG}$  = distance of ship C.G. from waterline, positive up  
and the following sectional hydrodynamic properties are from  
program STATIC

$M_s$  = sway added mass

$N_s$  = sway damping

$F_{rs}$  = roll sway added mass

$N_{rs}$  = roll sway damping

In a similar manner the hydrodynamic roll moment is as follows:

$$\frac{dKh}{dx} = \frac{D}{Dt} [(M_{s\phi} + \frac{N_{s\phi}}{i\omega_e}) (\dot{\delta}_4 + x\dot{\delta}_5 - V\delta_5)] - \frac{D}{Dt} [(I_r + \frac{N_r}{i\omega_e}) \dot{\delta}_6]$$
$$- \overline{OG} \frac{D}{Dt} [(M_{s\phi} + \frac{N_{s\phi}}{i\omega_e}) \delta_6] - \overline{OG} \frac{dYh}{dx} \quad [23]$$

This can be expressed as:

$$\begin{aligned}
 \frac{dKh}{dx} = & -V \frac{dM_{S\phi}}{dx} (\dot{\delta}_4 + x\dot{\delta}_5 - V\delta_5) - V \frac{dN_{S\phi}}{dx} (\dot{\delta}_4 + x\dot{\delta}_5 + \frac{V}{\omega_e^2} \ddot{\delta}_5) \\
 & + M_{S\phi} (\ddot{\delta}_4 + x\ddot{\delta}_5 - 2V\dot{\delta}_5) + N_{S\phi} (\dot{\delta}_4 + x\dot{\delta}_5 - 2V\delta_5) \quad [24] \\
 & - \ddot{\delta}_6 (I_r + \overline{OG} M_{S\phi}) - \dot{\delta}_6 [N_r + N_r^* + \overline{OG} N_{S\phi} - V(\frac{dI_r}{dx} + \overline{OG} \frac{dM_{S\phi}}{dx})] \\
 & + \delta_6 V [\frac{d(N_r + N_r^*)}{dx} + \overline{OG} \frac{dN_{S\phi}}{dx}] - \overline{OG} \frac{dYh}{dx}
 \end{aligned}$$

where the two dimensional hydrodynamic properties are defined as follows:

$M_{S\phi}$  = sway-roll added mass moment of inertia

$N_{S\phi}$  = sway-roll damping

$I_r$  = roll added mass moment of inertia

$N_r$  = roll damping

In order to accurately define roll motions near resonance viscous roll damping,  $N_r^*$ , must be considered. Two choices for calculating this value are available. The first is the simplest and is as follows:

$$N_r^* = \zeta_\phi C_c / L - N_r(\omega_\phi) dx \quad [25]$$

where

$\zeta_\phi$  = fraction of critical roll damping (empirical data)

$C_c$  = critical roll damping

$$= 2 Mg \overline{GM} / \omega_\phi$$

$L$  = ship length

$\omega_\phi$  = natural roll (resonant) frequency

$$= \left[ \frac{Mg \overline{GM}}{I_x + \int I_r(\omega_\phi) dx} \right]^{1/2}$$

$N_r(\omega\phi)$  = roll damping at frequency  $\omega\phi$

$I_r(\omega\phi)$  = roll added mass moment of inertia at frequency  $\omega\phi$

The viscous roll damping effect can also be calculated for skin friction (4) and eddy making resistances (5) using roll velocity,  $\dot{\delta}_6$ , as follows:

$$N_r^* = K \dot{\delta}_6 \quad [26]$$

where  $K$  depends upon the frequency, the viscosity, the bilge keel dimensions and the hull geometry. This is an interative approach that first assumes a roll velocity, calculates the viscous roll damping and then solves the equations of motion for roll. If the final roll is signficantly different from the initial one this process is repeated.

The equations of motion for the lateral plane motions of sway, yaw and roll are as follows:

$$[M + A_{44}] \ddot{\delta}_4 + B_{44} \dot{\delta}_4 + C_{44} \delta_4 + A_{45} \ddot{\delta}_5 + B_{45} \dot{\delta}_5 + C_{45} \delta_5 + A_{46} \ddot{\delta}_6 + B_{46} \dot{\delta}_6 + C_{46} \delta_6 = Y_w$$

$$A_{54} \ddot{\delta}_4 + B_{54} \dot{\delta}_4 + C_{54} \delta_4 + [I_z + A_{55}] \ddot{\delta}_5 + B_{55} \dot{\delta}_5 + C_{55} \delta_5 +$$

[27]

$$[-I_{xz} + A_{56}] \ddot{\delta}_6 + B_{56} \dot{\delta}_6 + C_{56} \delta_6 = N_w$$

$$A_{64} \ddot{\delta}_4 + B_{64} \dot{\delta}_4 + C_{64} \delta_4 + [-I_{xz} + A_{65}] \ddot{\delta}_5 + B_{65} \dot{\delta}_5 + C_{65} \delta_5 +$$

$$[I_x + A_{66}] \ddot{\delta}_6 + B_{66} \dot{\delta}_6 + C_{66} \delta_6 = K_w$$

These coefficients  $A$ ,  $B$ , and  $C$  are as follows:

$$A_{44} = \int M_S dx$$

$$B_{44} = \int N_S dx - V \int \frac{dM_S}{dx} dx$$

$$C_{44} = -V \int \frac{dN_S}{dx} dx$$

$$A_{45} = \int x M_S dx$$

$$B_{45} = \int x N_S dx - 2V \int M_S dx - V \int x \frac{dM_S}{dx} dx - \frac{V^2}{\omega_e^2} \int \frac{dN_S}{dx} dx$$

$$C_{45} = V^2 \int \frac{dM_S}{dx} dx - V \int x \frac{dN_S}{dx} dx - 2V \int N_S dx$$

$$A_{46} = - \int F_{rs} dx - \overline{OG} \int M_x dx$$

$$B_{46} = V \int \frac{dF_{rs}}{dx} dx - \int N_{rs} dx + \overline{OG} V \int \frac{dM_S}{dx} dx - \overline{OG} \int N_S dx$$

$$C_{46} = V \int \frac{dN_{rs}}{dx} dx + \overline{OG} V \int \frac{dN_S}{dx} dx$$

$$A_{54} = \int x M_S dx$$

$$B_{54} = \int x N_S dx - V \int x \frac{dM_S}{dx} dx$$

$$C_{54} = -V \int x \frac{dN_S}{dx} dx$$

$$A_{55} = \int x^2 M_S dx$$

$$B_{55} = \int x^2 N_S dx - 2V \int x M_S dx - V \int x^2 \frac{dM_S}{dx} dx - \frac{V^2}{\omega_e^2} \int x \frac{dN_S}{dx} dx$$

$$C_{55} = V^2 \int x \frac{dM_S}{dx} dx - V \int x^2 \frac{dN_S}{dx} dx - 2V \int x N_S dx$$

$$A_{56} = - \int x F_{rs} dx - \overline{OG} \int x M_S dx$$

$$B_{56} = V \int x \frac{dF_{rs}}{dx} dx - \int x N_{rs} dx + \overline{OG} V \int x \frac{dM_S}{dx} dx - \overline{OG} \int x N_S dx$$

$$C_{56} = V \int x \frac{dN_{rs}}{dx} dx + \overline{OG} V \int x \frac{dN_s}{dx} dx$$

$$A_{64} = - \int M_{s\phi} dx - \overline{OG} A_{44}$$

$$B_{64} = - \int N_{s\phi} dx + V \int \frac{dM_{s\phi}}{dx} - \overline{OG} B_{44}$$

$$C_{64} = V \int \frac{dN_{s\phi}}{dx} dx - \overline{OG} C_{44}$$

$$A_{65} = - \int x M_{s\phi} dx - \overline{OG} A_{45}$$

$$B_{65} = - \int x N_{s\phi} dx + 2V \int M_{s\phi} dx + V \int x \frac{dM_{s\phi}}{dx} dx + \frac{V^2}{\omega_e z} \int \frac{dN_{s\phi}}{dx} dx - \overline{OG} B_{45}$$

$$C_{65} = -V^2 \int \frac{dM_{s\phi}}{dx} dx + V \int x \frac{dN_{s\phi}}{dx} dx + 2V \int N_{s\phi} dx - \overline{OG} C_{45}$$

$$A_{66} = \int I_r dx + \overline{OG} \int M_{s\phi} dx - \overline{OG} A_{46}$$

$$B_{66} = -V \int \frac{dI_r}{dx} dx + \int (N_r + N_r^*) dx - \overline{OG} V \int \frac{dM_{s\phi}}{dx} dx + \overline{OG} \int N_{s\phi} dx - \overline{OG} B_{46}$$

$$C_{66} = Mg \overline{GM} - V \int \frac{d(N_r + N_r^*)}{dx} dx - \overline{OG} V \int \frac{dN_{s\phi}}{dx} dx - \overline{OG} C_{46}$$

with all the integrations over the ship length.

The wave excitation, the right-hand sides of Equation [27] is given by

$$Y_w = \int \frac{dY_w}{dx} dx \quad [28]$$

$$N_w = \int x \frac{dY_w}{dx} dx \quad [29]$$

$$K_w = \int \frac{dK_w}{dx} dx \quad [30]$$

The local sway sectional excitation force becomes:

$$\frac{dY_w}{dx} = \left[ (\rho S + M_s) \frac{Dv_w}{Dt} - V v_w \frac{dM_s}{dx} + k(-F_{rs} \frac{Dv_w}{Dt} + V \frac{dF_{rs}}{dx} v_w) + \frac{\omega}{\omega_e} N_s v_w + \frac{V}{\omega \omega_e} \frac{dN_s}{dx} \frac{Dv_w}{Dt} \right] \frac{\sin(\frac{\pi B^*}{\lambda} \sin \beta)}{\frac{\pi B^*}{\lambda} \sin \beta} \quad [31]$$

and the local roll sectional excitation moment

$$\frac{dK_w}{dx} = \left[ -\frac{D}{Dt} (F_{rs} v_w) + \rho \left( \frac{B^*}{12} - S \bar{z} \right) \frac{Dv_w}{Dt} - \frac{\omega}{\omega_e} N_{rs} v_w - \frac{V}{\omega \omega_e} \frac{dN_{rs}}{dx} \frac{Dv_w}{Dt} \right] \frac{\sin(\frac{\pi B^*}{\lambda} \sin \beta)}{\frac{\pi B^*}{\lambda} \sin \beta} - \overline{OG} \frac{dY_w}{dx} \quad [32]$$

where  $v_w$  = lateral orbital wave velocity

$S$  = local section area

$\bar{z}$  = local sectional center of buoyancy from waterline

The lateral orbital wave velocity in complex form is as follows:

$$v_w = -A k c e^{-kh} \sin \beta e^{-i(k \cos \beta + k y \sin \beta + \omega_e t)} \quad [33]$$

and

$$\frac{Dv_w}{Dt} = -Akg e^{-kh} \sin\beta e^{-i(-kx\cos\beta + ky \sin\beta + \omega_e t)} \quad [34]$$

where  $c$  = wave celerity (speed)

$k$  = wave number

$\lambda$  = wave length

The wave induced lateral shear force, the lateral bending moment, and the torsional moment are defined as follows:

$$SF_y(x_0) = \left[ \int_{x_s}^{x_0} \text{or} \int_{x_0}^{x_b} \right] \frac{dfy}{dx} dx \quad [35]$$

$$BM_y(x_0) = \left[ \int_{x_s}^{x_0} \text{or} \int_{x_0}^{x_b} \right] (x - x_0) \frac{dfy}{dx} dx \quad [36]$$

$$TM_x(x_0) = \left[ \int_{x_s}^{x_0} \text{or} \int_{x_0}^{x_b} \right] \frac{dtx}{dx} dx \quad [37]$$

where

$$\frac{dfy}{dx} = -m(\ddot{\delta}_4 + x\ddot{\delta}_5 - \zeta\ddot{\delta}_6) + \frac{dY_h}{dx} + \frac{dY_w}{dx} \quad [38]$$

$$\frac{dtx}{dx} = -m\gamma^2\ddot{\delta}_6 + m\zeta(\ddot{\delta}_4 + x\ddot{\delta}_5) - \rho g \left[ \frac{B^*^3}{12} - S(\bar{z} + \bar{OG}) \right] \ddot{\delta}_6$$

$$- g m \zeta \ddot{\delta}_6 + \frac{dKh}{dx} + \frac{dKw}{dx} \quad [39]$$

where  $\zeta$  = local section's center of gravity (relative to ship C. G.) positive down

$\gamma$  = local section's mass gyradius in roll

Point motions for vertical, lateral and longitudinal directions can be calculated using the six primary motions. The displacements at a point,  $x_0$ ,  $y_0$ ,  $z_0$  measured from the ship's center of gravity, are as follows:

$$\delta_7 = \delta_1 - x_0\delta_2 + y_0\delta_6$$

$$\delta_8 = \delta_4 + x_0\delta_5 - z_0\delta_6$$

$$\delta_9 = \delta_3 + z_0\delta_2 + y_0\delta_5$$

[40]

where  $\delta_7$ ,  $\delta_8$ , and  $\delta_9$  are the vertical lateral and longitudinal displacements respectively. Velocity and acceleration are obtained by successive differentiations of Equation [40].

Relative point motions are computed by using the point motion Eq. [40], minus the wave motion as given in Equation [10].

Once the motions responses have been calculated for a range of frequencies and wave headings, the short term analysis can be performed.

### B. Short Term Analysis

The basic input for the short term analysis is the response amplitude operators and the wave spectra. This section will be divided into two parts, first the discussions of the wave spectra and then the numerical procedure to evaluate the short term responses.

The wave spectrum can either be a long crested sea spectrum, that is uni-directional as in the case of swell, or a short crested sea spectrum where the energy is coming from many directions

The short-crested sea spectrum is obtained by combining a point spectrum with a spreading function. The point spectrum can either be analytical, such as the ISSC, ITTC or JONSWAP formulations, all being forms of the Bretschneider spectra, or a measured spectrum, such as those from Stations I, K and P or any other source.

If the two-dimensional sea spectrum,  $S\xi(\omega, x_j)$ , is assumed to be the product of the one-dimensional sea spectrum,  $S\xi(\omega)$ , and a spreading function  $f(x_j)$ , then

$$S\xi(\omega, x_j) = S\xi(\omega) \cdot f(x_j) \quad [41]$$

where  $x_j$  is the wave direction angle. A commonly used form of this is the cosine-squared spreading function:

$$\begin{aligned} f(x_j) &= \frac{2}{\pi} \cos^2(x_j) \quad \text{for } |x_j| \leq \frac{\pi}{2} \\ &= 0.0 \quad \text{for } |x_j| > \frac{\pi}{2} \end{aligned} \quad [42]$$

Figure 3 shows the resulting directional wave energy topography for a typical directional spectrum based on the above spreading function.

A more general formulation of the spreading function has been adopted here so that spreadings other than  $\pm \pi/2$  and other powers of the cosine function can be used. An extremely confused sea with waves from different storm areas might have spreading larger than  $\pm \pi/2$ ; conversely waves in a restricted waterway

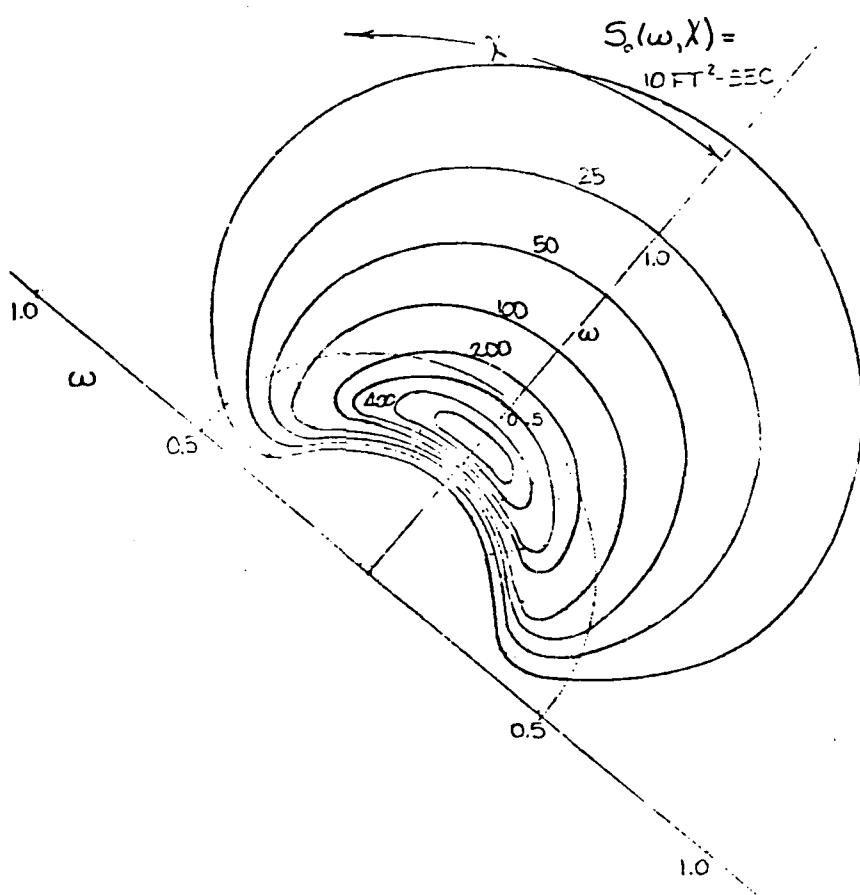


Figure 3.

might be less than  $\pm \pi/2$ , with the limiting case being 0 for long-crested waves.

The general spreading formula is:

$$\begin{aligned} F(x_j) &= \frac{1}{A} \cos^{2v} \frac{x_j}{x_{jo}} && \text{for } |x_j| \leq x_{jo} \\ &= 0.0 && \text{for } |x_j| \geq x_{jo} \end{aligned} \quad [43]$$

with  $A = \int_{-x_{jo}}^{+x_{jo}} \cos^{2v} x_{jo} dx$

where  $x_{jo}$  is the angular spread and  $2v$  is the power of the cosine function.

The energy spectrum is customarily given in length<sup>2</sup> -second units at frequencies specified in radians per second. The spectra are usually divided into several groups, based on wave height intervals, with each group containing from one to 15 spectra. Typical analytical formulations for the point spectrum are now given.

#### Neumann Spectrum (1953)

This frequency spectrum (as used) is given by:

$$S(\omega) = 0.000827 g^2 \pi^3 \omega^{-6} e^{-2g^2 \omega^{-2} U^{-2}} \quad [44]$$

where  $U$  = wind speed

#### Pierson-Moskowitz (1964) (ITTC Spectrum)

This is given by:

$$S(\omega) = \frac{0.0081 g^2}{\omega^5} \exp \left( -\frac{0.0324 g^2}{H_1 / 3 \omega^4} \right) \quad [45]$$

or

$$S(\omega) = 0.0081 g^2 \omega^{-5} e^{-0.74 g^4 \omega^{-4} U^{-4}}$$

and was derived on the basis of fully arisen seas.

Two Parameter (1967) (ISSC Spectrum)

$$S(\omega) = \underline{A} \cdot \underline{B}^{-5} e^{-\underline{B}\omega^{-4}} \quad [46]$$

where  $A = 0.25 H_{1/3}^2$   
 $B = (0.817 \frac{2\pi}{T_1})^4$

$H_{1/3}$  = significant wave height ( $= 2.0a_{1/3}$ )

$T_1$  = mean wave period

JONSWAP

$$S_2(\omega) = S(\omega) \cdot \frac{1}{ISSC F_1} \gamma \exp \left[ -\frac{1}{2\sigma^2} (.2043\omega \cdot T - 1)^2 \right] \quad [47]$$

where  $F_1$  = ratio of area of JONSWAP spectra to area of ISSC spectrum. This corrects JONSWAP to required wave height.

$\sigma$  = Spectra widths to each side of the spectral peak

$$= 0.07 \omega \leq 4.848/T,$$

$$0.09 \omega > 4.848/T,$$

$\gamma$  = is the ratio of the maximum spectral energy to the maximum of the corresponding Pierson-Moskowitz spectrum. The examination of the Great Lakes wave data has shown the mean gamma to be 2.3.

Ideally, measured spectra representing a wide range of heights and periods should be used to represent an irregular seaway in conjunction with an assumed spreading function. Files of wave data representing typical ocean areas such as Station "India" in the northeast Atlantic or Station "Papa" in the northwest Pacific at

the entrance to the Gulf of Alaska are currently available. Another source of wave data in a spectral ordinate form is hindcast and forecast weather from a spectral ocean wave model (SOWM).

Once the wave spectra is defined using the principles of linear superposition the short term responses can be calculated.

The rms response for a particular ship heading,  $x_i$ , relative to the dominant wave direction, for a particular wave spectrum, indicated by  $n$ , is:

$$\text{RESP} (x_i, n) = \left[ \int_{\omega} \int_x \text{RAO}^2 (\omega, x) S_{\zeta n} (\omega) f(x_j) dx d\omega \right]^{\frac{1}{2}} \quad [48]$$

where  $X$

is the relative ship wave angle, defined as,  $x_j - x_i$ ,  $\text{RAO} (\omega, X)$  is the response amplitude operator as a function of angle  $x$ , and frequency  $\omega$ ;  $S_{\zeta n} (\omega)$  is the spectral energy for a particular point spectrum,  $n$ , as a function of frequency  $\omega$ ; and  $f(x_j)$  is the spreading function versus component angle  $x_j$ .

In any wave group the response calculation can be carried out for many spectra,  $N$ , and for headings ranging from 0 to  $180^\circ$ . At each heading the mean rms response,  $\mu(x_i)$  and standard deviation  $\sigma(x_i)$  can be calculated as follows:

$$\mu(x_i) = \frac{1}{N} \sum_{n=1}^N \text{RESP} (x_i, n) \quad [49]$$

$$\sigma^2(x_i) = \frac{1}{N} \sum_{n=1}^N \left[ (\text{RESP} (x_i, n) - \mu(x_i))^2 \right] = \left[ \frac{1}{N} \sum_{n=1}^N [\text{RESP} (x_i, n)]^2 \right] - \mu^2(x_i) \quad [50]$$

The average response of the ship to all headings for a given wave group is then,

$$\bar{\mu} = \sum_{i=0}^{360} P(x_i) \mu(x_i)$$

where  $p(x_i)$  is the probability of occurrence of each heading angle. The standard deviation (squared) is then, as given in (7) ,

$$\sigma^2 = \sum_{i=0}^{360} P(x_i) [ \mu^2 (x_i) + \sigma^2(x_i) ] - \mu^2 \quad [51]$$

The calculation of the means and standard deviations of a response for each wave heading and each wave height group provide the basis for obtaining a cumulative long-term distribution of the response.

### C. Long Term Statistics

The long-term distribution for each wave (weather) group can be determined assuming that the actual peak to trough values of the responses over the short term are Rayleigh distributed and the short term r.m.s. values for any wave height are normally distributed. Using the mean and standard deviation for each wave height group, a cumulative long term distribution of response by the summation of many Rayleigh distributions can be obtained (8). Using the probability of occurrence of the wave height groups, these long-term curves can then be combined to give a single long term curve covering all sea conditions. This long term theory has been extensively covered in (8) with hand verification in (9) and computer program and documentation in (10).

### III. DESCRIPTION OF INPUT SCHEME

There are three separate data files used in running SCOMOT:

- (1) Two dimensional hydrostatic and hydrodynamic properties (TDP) file.
- (2) Job control data file.
- (3) Spectral family file.

The TDP file is prepared by Program STATIC and contains the two-dimensional hydrodynamic added mass and damping for vertical and lateral motions. The wetted offsets as well as the geometry to the main deck is also included for each station. The spectral data file is used for calculating the short-term and long-term responses. This file consists of spectral energy ordinates for a series of frequencies and can be a measured, hindcast forecast, or mathematical spectrum. The job control file directs the execution of the program and can be prepared by Program STATIC.

In order to have a uniform naming procedure for datafiles, the use of 2 two letter prefixes are employed for each datafile type. A limit of seven letters for a filename exists on the present computer system, therefore 5 letters, indicated by "X", can be used to describe the ship and its loading condition. Summarizing the datafiles for program STATIC and SCOMOT the following conventions have been adopted:

- |                           |   |
|---------------------------|---|
| (1) OFXXXXX or<br>MMTXXXX | Ship offset file  |
| (2) D2XXXXX               | Job control file for STATIC   |
| (3) DWXXXXX               | Weight description for STATIC   |
| (4) TDXXXXX               | Two dimensional hydrodynamic properties file created by STATIC and used in SCOMOT |
| (5) DMXXXXX               | Job control file for ship motion program SCOMOT                                   |
| (6) SPXXXXX               | Spectral datafile of hindcast, forecast, measured, etc. point energy spectra.     |

#### A. Two Dimensional Properties

This file contains the two dimensional properties (TDP) for each ship section and is prepared by program STATIC. The output from program STATIC for this example is shown in Appendix D. The full offsets to the main deck with the origin at the intersection of the keel and centerline are stored in the TDP file along with the wetted geometry for each station, using the water-plane and centerline as the reference axis. The two-dimensional hydrodynamic added mass and damping coefficients for 25 frequencies are also stored for each section. These hydrodynamic properties are as follows:

| <u>SYMBOL</u>       | <u>DESCRIPTION</u>                      | <u>DIMENSION</u>      |
|---------------------|---|-----------------------|
| Frequency Parameter | $\frac{\omega^2 D}{g}$                  | Non-Dimensional       |
| $A'_{33}$           | Heave added mass                        | $F \cdot sec^2 / L^2$ |
| $N'_z$              | Heave damping                           | $F \cdot sec / L^2$   |
| $M_s$               | Sway added mass                         | $F \cdot sec^2 / L^2$ |
| $N_s$               | Sway damping                            | $F \cdot sec / L^2$   |
| $F_{rs}$            | Added mass for sway-roll cross coupling | $F \cdot sec$         |
| $N_{rs}$            | Damping for sway-roll cross coupling    | $F \cdot sec / L$     |

| <u>SYMBOL</u> | <u>DESCRIPTION</u>   | <u>DIMENSION</u>    |
|---------------|--|---------------------|
| $I_r$         | Added moment of inertia in roll                                      | $F \cdot sec^2$     |
| $N_r$         | Roll damping   | $F \cdot sec$       |
| $M_{s\theta}$ | Roll-sway added mass moment of inertia (same as $Frs$ - not printed) | $F \cdot sec^2 / L$ |
| $N_{s\theta}$ | Roll-sway damping (same as $Nrs$ - not printed)                      | $F \cdot sec / L$   |

where

F is force units  
L is length units  
D is station draft  
 $\omega$  is frequency (radians/second)  
g is acceleration of gravity

This file is in binary form and cannot be listed, therefore, a small program and explanation are given in Appendix D so that this file can be interpreted.

B. Job Control Data File (DMXXXXX)

This data file controls the execution of program SCOMOT using control tags and other information separated into data sets given below. This file is created by Program STATIC and can be edited for specific conditions desired for each run.

|             |  |
|-------------|--|
| Data Set 1  | File Names   |
| 2           | Ship Name or Title                                   |
| 3           | Program Option Control                               |
| 4           | Units Specification (i.e., Metric or English)        |
| 5           | Length and Displacement                              |
| 6           | Two-dimensional Geometric Properties                 |
| 7           | Vertical Center of Gravity & Roll Gyradius           |
| 8           | Summary Weight Properties                            |
| 9           | Sectional Weight Properties                          |
| 10          | Moment Station and Resistance Variation<br>for Surge |
| Data Set 11 | Slamming, Shipping of Water and<br>Propeller Racing  |
| 12          | Input Point Coordinates                              |
| 13          | Run Control  |
| 14          | Ship Speeds  |
| 15          | Wave Frequencies                                     |
| 16          | Wave Angle   |
| 17          | Roll Damping   |
| 18          | Analytical Spectra                                   |
| 19          | Heading Probability                                  |
| 20          | Wave Group Distribution                              |
| 21          | Spreading Function                                   |
| 22          | Long Term Limits                                     |
| 23          | Response Control                                     |

In the following section, the data input format is divided into three types:

- |   |              |  |
|---|--------------|--|
| A | Alphanumeric | - Combination of letter and numbers. This is used as a title or descriptive header |
| I | Integer      | - A whole number which must be right justified in input field                      |
| F | Real         | - A real number that contains a decimal point                                      |

DATA SET 1

The name of the two-dimensional hydrodynamic coefficient data file (TDPname) and the transfer function file (RAOname) are included in this data set.

| <u>Letter Code</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>   |
|--------------------|----------------|---------------|--|
| TDPname            | 1-7            | A             | TDP input file name  |
| RAOname            | 11-17          | A             | Input or output file name of transfer functions  |
| SPEname            | 21-27          | A             | Spectral family input data file name. This is needed if spectral family wave option is selected. |

DATA SET 2

Title of Ship Name

This is the title that normally identifies the owner, the ship name, and/or the loading condition.

DATA SET 3

| <u>Letter Code</u> | <u>Columns</u> | <u>Format</u> | <u>OPTION CONTROL CARD</u>   |
|--------------------|----------------|---------------|--|
| A                  | 1-2            | I             | TDP file option control tag  |
| B                  | 3-4            | I             | Unit option control tag  |
| C                  | 5-6            | I             | Speed option control tag   |
| D                  | 7-8            | I             | Wave spectra option control tag  |
| E                  | 9-10           | I             | Wave frequency option control tag                                      |
| F                  | 11-12          | I             | RAO selection option control tag                                       |
| G                  | 13-14          | I             | Degrees of freedom option control tag                                  |
| H                  | 15-16          | I             | Number of motion input points  |
| I                  | 17-18          | I             | Slamming, shipping of water, and propeller emersion option control tag |

| <u>Letter Code</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>                              |
|--------------------|----------------|---------------|---|
| J                  | 19-20          | I             | Roll damping option                       |
| K                  | 21-22          | I             | Terminal type                             |
| L                  | 23-24          | I             | Directionality option<br>control tag      |
| M                  | 25-26          | I             | Mass input option con-<br>trol tag        |
| N                  | 27-28          | I             | Heading probability<br>option control tag |
| O                  | 29-30          | I             | Wave distribution option<br>control tag   |
| P                  | 31-32          | I             | Speed input option con-<br>trol tag       |
| Q                  | 33-34          | I             | Frequency input option<br>control tag     |
| R                  | 35-36          | I             | Wave angle input option<br>control tag    |

Definition of Option Control Tags

A. TDP file option control tag

(two dimensional properties such as added mass and damping)

Options Available

0---read TDP file from file TDPname and no printout

1---read TDP file from file TDPname and printout data

B. Unit Option--sets, units and constants for program (GRAV is acceleration of gravity GAMMA is the density of water and VNY is the kinematic viscosity of salt water at 59°F)

0---British Units (feet, L. Tons)

    GRAV = 32.174, GAMMA = .02857143, VNY =  $1.2791 \times 10^{-5}$

1---Metric Units (Meters, M. Tons)

    GRAV = 9.807, GAMMA = 1.025, VNY =  $1.1883 \times 10^{-6}$

2---British Units (Feet, Pounds)

    GRAV = 32.174, GAMMA = 64.0, VNY =  $1.2791 \times 10^{-5}$

3---Metric Units (Meters, K. Gram)

    GRAV = 9.807, GAMMA = 1025.0, VNY =  $1.1883 \times 10^{-6}$

4---Input desired constants and units in program  
on Data set 4

Note:  $VNY \leq 1.23 \times 10^{-5}$

C. Ship Speed Option

used when J = 1

0---Ship speed is input in knots

1---Ship speed is input in velocity units consistent  
with the ship's length units. (i.e., feet/sec or  
meters/sec) on Data Set 14 in conjunction with option  
control tag P.

D. Wave Spectra Option

0---Regular wave - transfer functions only

1 or 6---Generate Neumann spectra from inputed wind speed.  
Print spectral properties if D=6; no print if D=1

2 or 7---Generate Pierson-Moskowitz spectra from inputed  
wind speed. Print spectral properties if D=7; no  
print if D=2

3 or 8---Generate ISSC two parameter spectra from inputed  
significant wave height ( $H_{1/3}$ ) and mean period ( $T_1$ ).  
Print spectral properties if D=8; no print if D=3

4 or 9---Generate JONSWAP spectra from inputed significant  
wave height ( $H_{1/3}$ ) mean period ( $T_1$ ) and Gamma para-  
meter. Print spectral properties if D=9; no print  
if D=4

- 5 or 10---Spectral family using inputed spectral ordinates as described in Section III,C. Print spectral properties if D=10: no print if D= 5.
- E. Wave Frequency (must be coordinated with option tag Q)
- 0---Radian/second used for frequencies in calculation of transfer functions
  - 1---Cycles/second (Hz) used for frequencies in calculation of transfer functions
  - 2---Wave lengths (Ft. or M) used for calculation of transfer functions
- F. RAO Selection Option - change F to a 1 after initial execution.
- 0---Calculate transfer functions and store in file RAOname
  - 1---Read transfer functions calculated previously and stored in file RAOname
- G. Degrees of Freedom Option
- 0---Vertical and lateral plane including surge
  - 1---Vertical plane only including surge effect
  - 2---Lateral plane only
  - 3---Vertical and lateral plane (no surge)
  - 4---Vertical plane only (no surge)
- H. Number of Acceleration (Relative Motion) Points
- If greater than zero, program will read these points in data set 12. (Maximum of 30 points)
- I. Slamming, Shipping of Water and Propeller Emersion Option
- 0---Slamming, shipping of water and propeller emersion calculations are not performed
  - 1---Slamming and shipping of water calculations are performed at forward perpendicular. Depth at forward perpendicular is read from data set 11. Propeller emersion at AP is performed with propeller height and diameter read from data set 11.
- J. Roll Damping Option
- 0---Use shortened roll damping routine and input roll damping factor on data set 17.
  - 1---Use detailed roll damping routine accounting for viscous and bilge keel effects. Read data set 17.

K. Terminal Type

- 0---Terminal with form feed and 132 character width
- 1---Terminal with form feed and 80 character width
- 2---Terminal without form feed and 132 character width
- 3---Terminal without form feed and 80 character width

L. Directionality Option Control Tag

- 0---Cosine squared at  $\pm$  90 degrees - spreading is used
- 1---Uni-directional waves (i.e., long crested)
- 2---Read power of cosine function and wave spreading from data set 21.

M. Mass Input Option

- 0---Input weight distribution
- 1---Input summary weight properties pitch radius of gyration and longitudinal center of gravity in data set 8

N. Heading Probability Option Control Tag

- 0---Equal probability of heading used in short and long term analysis
- 1---Read probability of heading in data set 19

O. Wave Height Distribution Option Control Tag

- Need only for long term calculations
- 0---If not running long term calculations or if option tag D=5' or 10 and probabilities are read from file SPename
- 1---Read new wave height distributions from data set 20

P. Speed Input Option Control Tag

- 0---Input initial, final and increment of speed in data set 14
- 1---Input number of speeds and ship speeds in data set 14

Q. Frequency Input Option Control Tag

- 0---Program assumes frequency range from .02 to 1.85 in steps of .05 radians/sec
- 1---Input initial frequency (wave length), final frequency (wave length) and increment of frequency (wave length) in data set 15
- 2---Input number of frequencies (wave length) and frequencies (wave lengths) in data set 15

R. Wave Heading Input Option Control Tag

- 0---Program assumes wave heading of 0 degrees to 180 degrees in 15 degree increments <= usual  
1---Input initial, final and increment of wave heading in data set 16  
2---Input number of wave headings and wave headings in data set 16

DATA SET 4

This card is read only if unit option control tag (B) is 4.

| Column : | Format | <u>Entry</u>                                |
|----------|--------|---|
| 5-10     | A      | Length Unit (i.e.METERS)                    |
| 11-20    | A      | Weight Unit (i.e.POUNDS)                    |
| 21-30    | F      | Acceleration of gravity [L/T <sup>2</sup> ] |
| 31-40    | F      | Density of water [F/L <sup>3</sup> ]        |
| 41-50    | F      | Kinematic Viscosity [L <sup>2</sup> /T]     |

DATA SET 5

|       |   | <u>LENGTH CARD</u> |
|-------|---|--------------------|
| 1-10  | F | Ship length        |
| 11-20 | F | Ship displacement  |
| 29-30 | I | Number of Stations |

DATA SET 6

|       |   | <u>SECTIONAL PROPERTIES CARD</u>   |
|-------|---|--|
| 1-10  | F | Section distance from the forward perpendicular                                |
| 11-20 | F | Section waterline breadth  |
| 21-30 | F | Section area coefficient   |
| 31-40 | F | Section draft measured from waterline to hull intersection with the centerline |
| 41-50 | F | Section centroid measured downwards from the waterline                         |

One card is required for each station starting with the bow proceeding aft. If no entries are given for the section centroid approximate values are calculated based on the area coefficient and draft (using a two-dimensional version of the Moorish Approximation). These cards are normally prepared by STATIC.

DATA SET 7

Columns

Format

1-10

F

LATERAL PLANE CARD

Entry

Ship's vertical center of gravity measured from waterline positive upwards

11-20

F

Radius of gyration in roll

DATA SET 8

Columns

Format

1-10

F

SUMMARY MASS PROPERTIES CARD

Entry

Radius of gyration in pitch (longitudinal)

11-20

F

Ship's longitudinal center of gravity measured from a midships (positive forward)

This card is used only if the mass input option tag, M is 1.

DATA SET 9

Columns

Format

1-10

F

SECTIONAL MASS PROPERTIES CARDS

Entry

Segment weight or mass (tons or tons-sec<sup>2</sup>/ft.)

11-20

F

Segment vertical c.g. (ft.)

21-20

F

Segment roll gyradius (ft.)

These cards are used only if the mass input option tag, M, is 0, in lieu of the summary mass properties card above. One card is used for each section to be specified, in a similar manner as the hull form cards described earlier.

The second entry, the segment vertical center of gravity, is necessary only for lateral bending moment calculations, and is measured positive downwards with respect to the ship's overall vertical center, as specified on the lateral plane data card above. Since it is required that the vertical mass moment integral satisfy the specified overall v.c.g., the input segment v.c.g.'s are shifted by an equal amount, up or down as necessary, to exactly balance the vertical moment for the hull. This minimizes the effort required to obtain precise balance in input data preparation. The third card entry, the segment roll gyra-radius, is needed only for torsional moment calculations. If no entries are given, the overall ship value is used at each segment.

DATA SET 10

Column

Format

1-2

I

First station for moment cal-  
culations

3-4

I

Last station for moment cal-  
culations

5-6

I

Increment between stations

11-20

I

Total resistance variation  
at first speed (mass time)/length

21-30

F

Total resistance variation at  
second speed (mass time)/length

31-40

F

Total resistance variation at  
third speed (mass time)/length

The parameters on this card determine where along the ship hull the moment calculations are to be performed. Station numbers are defined as zero at the forward end of the first segment, increasing to N, the number of the segment at the after end of the ship. If the calculations are required only at one station, then the first two entries on the card should be equal to that station number.

It is possible to input four total resistance variation

values corresponding to four speeds. If the program during execution performs more than four speeds in a run, then the fourth value of total resistance variation is used. If the resistance variation is not known, the surge procedure can still be run with this value as zero.

DATA SET 11

SLAMMING, SHIPPING OF WATER  
AND PROPELLER EMERGENCE CARD

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>   |
|----------------|---------------|--|
| 1-10           | F             | Depth to main deck at forward perpendicular (measured from baseline) |
| 11-20          | F             | Distance to center of the propeller from the ship's baseline         |
| 21-30          | F             | Diameter of propeller  |

This card is used only if the slamming, shipping of water and propeller emergence option control tag, I, is 1.

DATA SET 12

INPUT COORDINATE POINT CARDS

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>   |
|----------------|---------------|--|
| 1-10           | F             | X-coordinate (measured aft from the forward perpendicular) |
| 11-20          | F             | Y-coordinate (measured toward starboard from centerline)   |
| 21-30          | F             | Z-coordinate (measured upward from baseline)               |
| 31-32          | I             | Point Number   |

Input acceleration points are calculated only if acceleration control tag (H) is greater than 0. One card is read for each point specified in Option H. Points are used for calculation of vertical, lateral, and longitudinal accelerations and relative vertical motions, velocities, and accelerations. If no point number is given, the program assigns them sequentially starting with 1. Maximum number of points is 30.

DATA SET 13

| <u>Columns</u> | <u>Format</u> | <u>RUN CONTROL TAG</u> |
|----------------|---------------|------------------------|
| 1-10           | F             | Entry                  |
|                |               | Run control tag        |

The run card determines the program continuity. If it is greater than zero, the program executes; if less than zero, the program terminates execution.

DATA SET 14

SHIP SPEED CARDS

Ship speed may be input in either of two ways, depending on the speed option control tag (P). To obtain RAO's for a range of vessel speeds, i.e., possibly to compare with model test results, it is possible to input a range and increment of speeds (P=0) or a number of discrete values (P=1). The speeds should be consistent with control Option C in either knots or distance per second. Maximum of 20 speeds for the two possible choices of Option (P) the input is as follows:

(a) For P=0

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>            |
|----------------|---------------|-------------------------|
| 1-10           | F             | Initial ship speed      |
| 11-20          | F             | Final ship speed        |
| 21-30          | F             | Increment of ship speed |

(b) For P=1 (two or more cards)

|         |   |                       |
|---------|---|-----------------------|
| 1. 4-5  | I | Number of ship speeds |
| 2. 1-10 | F | First ship speed      |
| 11-20   | F | Second ship speed     |
| 21-30   | F | Third ship speed      |

Repeat card (2) for more than eight speed entries

DATA SET 15

FREQUENCY CARDS

The data read from this card is dependent upon the frequency control option tag (Q). This data can be inputted as frequency in radians per second or hertz, or as wave lengths depending

on wave frequency option control tag (E). Maximum of 34 frequencies. For the three possible choices of this option (Q) the input is as follows:

(a) For Q=0

No input card, program assumes a frequency range of 0.20 to 1.85 in 0.05 radian/second increments.

(b) For Q=1

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                                 |
|----------------|---------------|--|
| 1-10           | F             | First wave frequency (or wave length)        |
| 11-20          | F             | Last wave frequency (or wave length)         |
| 21-30          | F             | Increment of wave frequency (or wave length) |

(c) For Q=2 (read two or more cards)

|    |       |   |  |
|----|-------|---|--|
| 1. | 1-5   | F | Number of wave frequencies (or wave lengths) |
| 2. | 1-10  | F | First wave frequency (or wave length)        |
|    | 1-20  | F | Second wave frequency (or wave length)       |
|    | 21-30 | F | Third wave frequency (or wave length)        |
| :  | :     | : | :  |

Repeat card (2) for more than 8 frequency entries.

DATA SET 16

WAVE ANGLE CARD

The data read from this card is dependent upon the heading control option control tag (R). Maximum of 25 wave headings. For the three possible choices of this option (R) the input is as follows:

(a) For R=0

No card necessary, the program assumes a wave heading range of 0 degrees (following seas) to 180 degrees (head seas) in 15

degree increments.

(b) For R=1

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>            |
|----------------|---------------|-------------------------|
| 1-10           | F             | First wave angle        |
| 11-20          | F             | Last wave angle         |
| 21-30          | F             | Increment in wave angle |

(c) For R=2 (read two or more cards)

|    |       |   |                       |
|----|-------|---|-----------------------|
| 1. | 1-5   | I | Number of wave angles |
| 2. | 1-10  | F | First wave angle      |
|    | 11-20 | F | Second wave angle     |
|    | 21-30 | F | Third wave angle      |
|    | :     | : | :                     |

Repeat card (2) for more than 8 heading entries

DATA SET 17

ROLL DAMPING CARD

The data read from these cards is dependent upon the roll damping option control tag (J). For the two possible choices of this option (J) the input is as follows:

(a) For J=0

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                      |
|----------------|---------------|-----------------------------------|
| 1-10           | F             | Fraction of critical roll damping |

The calculated roll frequency is increased so that the total damping is the specified fraction of the critical damping. The additional roll damping is then used for all subsequent calculations.

(b) For J=1

| <u>Card 1</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>  |
|---------------|----------------|---------------|---|
| IBILGE        | 1-2            | I             | Integer specifying ship has no bilge keels (0) or ships has bilge keels (1) |
| IB1           | 3-4            | I             | First station number for bilge keel   |

| <u>Card 1</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>  |
|---------------|----------------|---------------|---|
| IB2           | 5-6            | I             | Last station number for bilge keel  |
| IMOD          | 7-8            | I             | Control for type of flow around hull. If equal to 0 turbulent flow is assumed, if 1, laminar flow is assumed. |

If IBILGE is equal to 1, the next set of cards are read for stations IB1 to IB2. (see figure)

Card 2

|       |   |   |
|-------|---|---|
| 1-10  | F | First station's bilge keel height above baseline  |
| 11-20 | F | Second station's bilge keel height above baseline |
| 21-30 | F | Third station's bilge keel height above baseline  |
| ⋮     |   |   |

Use additional cards if necessary (up to 8 on one card).

Card 3

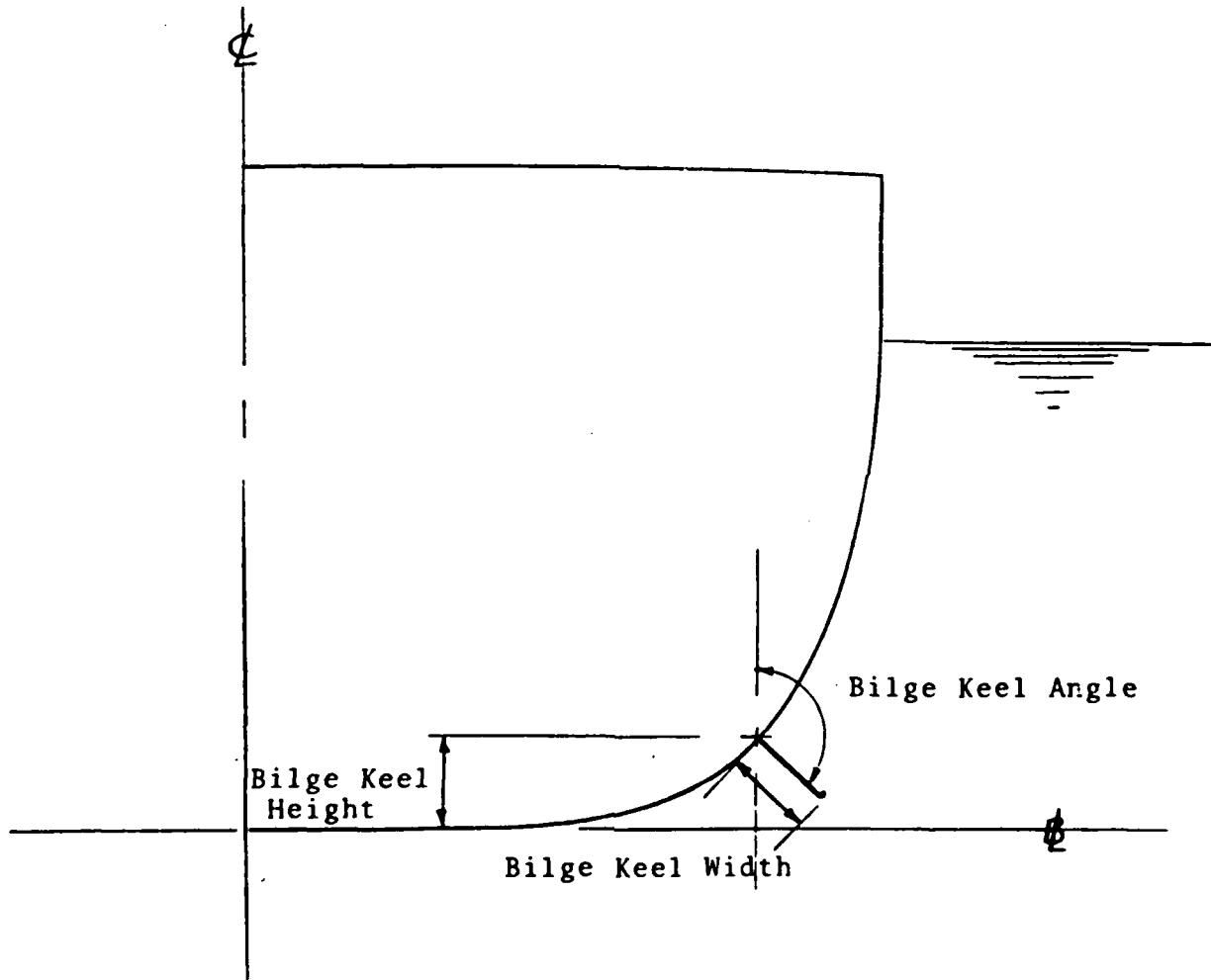
|       |   |                                |
|-------|---|--------------------------------|
| 1-10  | F | 1st station's bilge keel width |
| 11-20 | F | 2nd station's bilge keel width |
| 21-30 | F | 3rd station's bilge keel width |
| ⋮     |   |                                |

Use additional cards if necessary (up to 8 on one card).

Card 4

|       |   |                                    |
|-------|---|------------------------------------|
| 1-10  | F | Angle of bilge keel at 1st station |
| 11-20 | F | Angle of bilge keel at 2nd station |
| 21-30 | F | Angle of bilge keel at 3rd station |

Use additional card if necessary (up to 8 on each card)



Spectral Wave Input Cards

The wave input is controlled by the wave option control tag (D). The short term responses can either be calculated for individual spectra or groups of spectra. The latter will be referred to as a spectral family. The spectral family may contain up to 15 groups of spectra, usually formulated on the basis of significant wave height. Within each group there can be up to 12 individual spectra so that a short term response, RMS, and standard deviation are calculated for each group.

DATA SET 18

Card 1

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>  |
|----------------|---------------|---|
| 4-5            | I             | Number of wave spectra groups   |
| 9-10           | I             | Specifies whether there are more than one spectra in each group, if equal to 1, more than one spectra in a group. |

If one spectra per group

Card 2

|       |   |  |
|-------|---|--|
| 1-10  | F | First group wind speed<br>(significant wave height)  |
| 11-20 | F | Second group wind speed<br>(significant wave height) |
| 21-30 | F | Third group wind speed<br>(significant wave height)  |
| :     | : | :  |

If more than 8 wave groups use a second card.

Card 3 - Only if wave control tag = 3, 4 8, or 9

|       |   |                                    |
|-------|---|------------------------------------|
| 1-10  | F | First group mean period ( $T_1$ )  |
| 11-20 | F | Second group mean period ( $T_1$ ) |
| 21-30 | F | Third group mean period ( $T_1$ )  |
| :     | : | :                                  |

If more than 8 spectra within group, use second card.

18  
DATA SET ~~15~~ (cont')

-46-

Card 4 - Only if wave control card = 4 or 9

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                        |
|----------------|---------------|-------------------------------------|
| 1-10           | F             | Gamma for first JONSWAP wave group  |
| 11-20          | F             | Gamma for second JONSWAP wave group |
| 21-30          | F             | Gamma for third JONSWAP wave group  |
| :              | :             | :                                   |

If more than 8 wave groups, use a second card.

If more than one spectra per group

The following sets of cards are repeated for each wave group.

Card 2

|       |   |  |
|-------|---|--|
| 1-10  | F | Wind speed (significant wave height) for first wave spectrum in group  |
| 11-20 | F | Wind speed (significant wave height) for second wave spectrum in group |
| 21-30 | F | Wind speed (significant wave height) for third wave spectrum in group  |
| :     | : | :  |

If more than 8 spectra within group, use a second card.

Card 3 - Only if wave control tag = 3, 4, 8, or 9

|       |   |   |
|-------|---|---|
| 1-10  | F | Mean period ( $T_1$ ) for first wave spectrum in group  |
| 11-20 | F | Mean period ( $T_1$ ) for second wave spectrum in group |
| 21-30 | F | Mean period ( $T_1$ ) for third wave spectrum in group  |
| :     | : | :   |

If more than 8 spectra within group, use a second card.

Card 4 - Only if wave control card = 4 or 9

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                                    |
|----------------|---------------|---|
| 1-10           | F             | Gamma for first JONSWAP wave spectrum in group  |
| 11-20          | F             | Gamma for second JONSWAP wave spectrum in group |
| 21-30          | F             | Gamma for third JONSWAP wave spectrum in group  |
| :              | :             | :   |

If more than 8 spectra within group, use a second card.

DATA SET 19

HEADING PROBABILITY

This card is read only if the heading probability option control tag (N) is not zero. If the tag is zero, an equal probability of heading is assumed to calculate the average root-mean-square and standard deviation for each group and also for the long term calculations. If the option tag is equal to 1, the percentage of heading is read for two times the number of wave angles minus two values. This is to consider both sides of the ship in the short term and long term analysis while generally the transfer functions consider only one side of the ship. If the heading angles are considered,  $\theta_i$   $i = 1$  to  $N$  (i.e.,  $0^\circ$  to  $180^\circ$  in steps of  $15^\circ$ ), the remaining angles are

$$\theta_i = 360^\circ - \theta_{2N-i} \quad \text{for } i = N + 1 \text{ to } 2N - 2$$

(i.e.,  $195^\circ$  to  $345^\circ$  in steps of  $15^\circ$ ) Note that  $180^\circ$  represents the head sea condition.

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                              |
|----------------|---------------|---|
| 1-10           | F             | Heading probability for first wave angle  |
| 11-20          | F             | Heading probability for second wave angle |
| 21-30          | F             | Heading probability for third wave angle  |
| :              | :             | :   |

If more than 8 entries, use a second card.

DATA SET 20

WAVE GROUP DISTRIBUTION

Each area location in the oceans has a different distribution of wave groups. These cards are read only if option control tag (O) is not zero. This distribution is used in combining the short term results to calculate long term results. If long term results are desired, the input cards are as follows:

Card 1

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                    |
|----------------|---------------|---------------------------------|
| 1-24           | A             | Location or routing description |

Card 2

|       |   |                         |
|-------|---|-------------------------|
| 1-10  | F | First group percentage  |
| 11-20 | F | Second group percentage |
| 21-30 | F | Third group percentage  |
| :     | : | :                       |

If more than 8 groups, use a second card.

DATA SET 21

SPREADING FUNCTION CARD

This card is read only if directionality option control tag (L) is 2. The power of the cosine spreading function and the spreading is read. In a narrow or restricted waterway, the spreading might be less than  $\pm 90^\circ$ . The data is entered as follows:

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                           |
|----------------|---------------|--|
| 1-10           | F             | Spreading of waves                     |
| 11-20          | F             | Power of the cosine spreading function |

DATA SET 22

LONG TERM LIMITS

|       |   |  |
|-------|---|--|
| 4-5   | I | Number of long term calculation time periods     |
| 11-20 | F | Number of hours for first long term calculation  |
| 21-30 | F | Number of hours for second long term calculation |

DATA SET 22 (cont')

| <u>Columns</u> | <u>Format</u> | <u>Entry</u>                                    |
|----------------|---------------|---|
| 31-40          | F             | Number of hours for third long term calculation |

Maximum of ten input times.

DATA SET 23

RESPONSE CONTROL CARDS

These cards control the printing and execution of the program. Each line of data consists of 10 integer values as follows:

| <u>Name</u> | <u>Column</u> | <u>Format</u> | <u>Entry</u>  |
|-------------|---------------|---------------|---|
| I2          | 1-2           | I             | Type of response desired  |
| IMOT        | 3-4           | I             | Specified motion, whether displacement velocity or acceleration             |
| IR          | 5-6           | I             | Transfer function print option  |
| IS          | 7-8           | I             | Short term output option  |
| IL          | 9-10          | I             | Long term output option   |
| IPLRAO      | 11-12         | I             | Transfer function plot control  |
| IPLSTM      | 13-14         | I             | Short term results plot control   |
| J1          | 15-16         | I             | First index of motion coordinates for stations number for above calculation |
| J2          | 17-18         | I             | Last index of motion coordinates or station number for above calculation    |
| JINC        | 19-20         | I             | Increment of motion coordinate or station number for above calculation      |

Entry 1 - IZ - Response Type

| <u>IZ</u> | <u>Response</u> |
|-----------|-----------------|
| 1         | Heave motion    |
| 2         | Pitch motion    |
| 3         | Surge motion    |
| 4         | Sway motion     |
| 5         | Yaw motion      |
| 6         | Roll motion     |

| <u>I2</u> | <u>Response</u>  |
|-----------|--|
| 7         | Vertical bending moment  |
| 8         | Lateral bending moment   |
| 9         | Torsional moment   |
| 10        | Vertical shear force   |
| 11        | Lateral shear force  |
| 12        | Vertical motion at forward perpendicular                         |
| 13        | Vertical motion at ship's center of gravity                      |
| 14        | Vertical motion at after perpendicular                           |
| 15        | Vertical motion at port or starboard side of vessel              |
| 16        | Relative vertical motion at forward perpendicular                |
| 17        | Relative vertical motion after perpendicular                     |
| 18        | Vertical motion of input coordinate point starboard side of ship |
| 19        | Vertical motion of input coordinate points port side of ship     |
| 20        | Lateral motion of input coordinate points                        |
| 21        | Longitudinal motion of input coordinate points                   |
| 22        | Relative vertical motion of input coordinate points              |
| 23        | Slamming and shipping of water for input coordinate points       |
| 99        | Program terminates   |

Entry 2 - IMOT - Motion Type

- 1      Specifies displacement response, i.e., heave displacement, relative vertical displacement, etc.
- 2      Specifies velocity, i.e., heave velocity, realtive vertical,etc.

Entry 2 - IMOT - Motion Type (cont')

| <u>IZ</u> | <u>Response</u>  |
|-----------|--|
| 3         | Specifies acceleration, i.e.,<br>heave acceleration, relative<br>vertical acceleration |

Entry 3 - IR - Transfer function print option

|   |                                 |
|---|---------------------------------|
| 0 | Do not print transfer functions |
| 1 | Print transfer functions        |

Entry 4 - IS - Short Term Print Option

|   |  |
|---|--|
| 0 | Do not print short term responses  |
| 1 | Print detailed short term<br>results for all heading and<br>wave heights |
| 2 | Abbreviated short term printout<br>for just wave height groups           |

Entry 5 - IL - Long Term Print Option

|   |  |
|---|--|
| 0 | Do not print or calculate long<br>term results |
| 1 | Print and calculate long term<br>results       |

Entry 6 - IPLRAO - Transfer Function Plot Option

|     |  |
|-----|--|
| 0   | Do not plot transfer functions   |
| > 1 | If one plot transfer functions<br>for every wave angle. If two,<br>plot every other wave angle, etc. |

Entry 7 - PPLSTM - Short Term Plot Option

|     |   |
|-----|---|
| 0   | Do not plot short term results  |
| > 1 | If one, plot short term results<br>for every wave angle. If two,<br>plot every other wave angle, etc. |

Entry 8 - J1 - First Index Number

First index for motion calculation using coordinate points or moment and force calculations using station numbers. If it is equal to zero, J1=1 is assumed for coordinate points or J1=MINKR1 from Data Set 10 is assumed for bending moment and shear force calculation.

Entry 9 - J2 - Last Index Number

Last index for motion calculations using coordinate points or moment and force calculations using station numbers. If it is equal to zero, J2=NPTS from option control tag, H, Data Set 3 for last coordinate point or last station, J2MAXKR1 from Data Set 10 is assumed for bending moment and shear force calculations.

Entry 10 - JINC - Index Increment

Index increment for motion calculations using coordinate points or moment and force calculations using station numbers. If it is equal to zero, JINC=1 for coordinate motion calculations and JINC=INCRES from Data Set 10 for bending moment and shear force calculations.

### C. Spectral Data

The extension of the regular wave results to short term values by means of linear superposition requires an energy spectrum. Program SCOMOT has the capability of calculating several forms of analytical spectra and also of reading a spectral data file. Wave data representing typical ocean areas such as India (11), Papa (12), and Kilo (13) as well as hindcast and forecast information are available for a more realistic appraisal of a vessel's short term responses. A common way of representing this information is dividing the total sample into wave height groups and then selecting a limited sample of spectra to represent the total group so that computational time will be reduced. The format of this input will be as follows:

| <u>Data Set</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>   |
|-----------------|----------------|---------------|--|
| 1               | 1-32           | A             | Spectra name or location   |
| 2               | 9-10           | I             | Number of wave height groups (maximum of 15)                     |
|                 | 11-20          | F             | Acceleration of gravity for spectra so that units are determined |
| 3               | 9-10           | I             | Number of frequencies (maximum of 50)                            |
| 4               | 1-10           | F             | First spectral frequency   |
|                 | 11-20          | F             | Second spectral frequency  |
|                 | 21-30          | F             | Third spectral frequency   |
|                 | :              | :             | :  |

If more than 8 frequencies continue with additional cards.

For each wave height group repeat the following two data sets (5 & 6)

|   |       |   |  |
|---|-------|---|--|
| 5 | 1-10  | F | Wave height of this group                        |
|   | 19-20 | I | Number of spectral in this group (maximum of 12) |

| <u>Data Set</u> | <u>Columns</u> | <u>Format</u> | <u>Entry</u>                                       |
|-----------------|----------------|---------------|--|
| 5               | 21-30          | F             | Percent of occurrence of<br>this wave height group |

For each spectra in this group read:

|   |       |   |                          |
|---|-------|---|--------------------------|
| 6 | 1-10  | F | First spectral ordinate  |
|   | 11-20 | F | Second spectral ordinate |
|   | 21-30 | F | Third spectral ordinate  |
|   | ⋮     | ⋮ | ⋮                        |

If more than eight frequencies continue with additional cards.

The spectral frequencies are given in radius per second and the inputted accelerations of gravity on Data Set 2. The spectral ordinates are interpolated to the ship's response amplitude operator frequencies and the units are also converted (i.e., feet to meters). An example spectral data file for the Great Lakes can be seen below:

GREAT LAKES SPECTRA  
6 32-17400



|          |          |          |          |           |           |          |  |
|----------|----------|----------|----------|-----------|-----------|----------|--|
| 20.5053  | 3        | 0.00090  |          |           |           |          |  |
| 0.00000  | 0.00000  | 11.25000 | 56.25000 | 78.75000  | 48.37500  | 33.75000 |  |
| 13.95000 | 19.12500 | 9.22500  | 5.62500  | 4.50000   | 2.92500   | 2.70000  |  |
| 1.12500  | 1.12500  | 0.32400  | 0.90000  | 0.67500   | 0.45000   | 0.22500  |  |
| 0.15750  | 0.11250  | 0.09000  | 0.06750  | 0.04500   | 0.02250   | 0.02250  |  |
| 0.02250  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 28.80000  | 90.72000  | 43.20000 |  |
| 25.92000 | 10.08000 | 7.20000  | 4.32000  | 3.60000   | 2.88000   | 1.44000  |  |
| 1.44000  | 1.44000  | 1.29600  | 1.15200  | 1.00800   | 0.86400   | 0.72000  |  |
| 0.57600  | 0.43200  | 0.28800  | 0.14400  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 61.87500 | 84.37500  | 39.37500  | 12.37500 |  |
| 23.62500 | 15.75000 | 8.55000  | 6.75000  | 3.15000   | 2.25000   | 2.25000  |  |
| 2.25000  | 1.57500  | 1.12500  | 0.90000  | 0.67500   | 0.45000   | 0.22500  |  |
| 0.22500  | 0.22500  | 0.22500  | 0.22500  | 0.22500   | 0.22500   | 0.22500  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 29.2754  | 3        | 0.00020  |          |           |           |          |  |
| 0.00000  | 0.00000  | 1.17023  | 8.27606  | 55.80913  | 115.52696 | 79.52720 |  |
| 39.54649 | 29.12303 | 24.80403 | 22.27055 | 19.90596  | 16.64862  | 12.42610 |  |
| 7.76935  | 5.04284  | 3.42624  | 3.42624  | 2.71445   | 2.20775   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.06273  | 0.74074  | 2.65413  | 11.66611 | 110.17053 | 155.24234 | 99.84340 |  |
| 57.32914 | 28.56805 | 28.25440 | 20.30408 | 16.21431  | 11.26798  | 9.42210  |  |
| 8.22779  | 5.94766  | 4.58440  | 3.42624  | 2.71445   | 1.71312   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.15684  | 1.25468  | 3.59514  | 18.33762 | 129.88346 | 157.92061 | 78.29670 |  |
| 39.95670 | 37.97816 | 31.65651 | 21.42604 | 12.52266  | 9.79614   | 8.56560  |  |
| 6.85248  | 5.13936  | 5.13936  | 3.42624  | 3.42624   | 1.71312   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |
| 0.00000  | 0.00000  | 0.00000  | 0.00000  | 0.00000   | 0.00000   | 0.00000  |  |

)

IV. DESCRIPTION OF OUTPUT SCHEME

A description of the output format will be given with a sample run shown in Appendix A, using the input file given below. The name of this file is DMTEMP where DM stands for Datafile Motions and TEMP is a descriptor for defining the present example.

08/01/80. 09.22.39.

LIST OF DMTEMP

| TDPSL7F                             | RAOSL7F  | SPENAME |          |            | DATA SET 1 |
|-------------------------------------|----------|---------|----------|------------|------------|
| SL-7 - NORMAL FULL LOAD DEPARTURE   |          |         |          |            | DATA SET 2 |
| 0 4 0 3 0 0 0 0 0 0 1 0 0 0 1 0 0 0 |          |         |          |            | DATA SET 3 |
| FEET                                | L.TONS   | 32.1740 | .0285714 | 1.1057E-05 | DATA SET 4 |
| 880.5000                            | 47727.65 | 21      |          |            | DATA SET 5 |
| 0.0000                              | 6.8217   | 1.0000  | 32.5905  | 22.2506    |            |
| 44.0250                             | 6.0099   | 1.7202  | 32.6084  | 19.1009    |            |
| 88.0500                             | 15.8877  | .9570   | 32.6264  | 16.8238    |            |
| 132.0750                            | 29.0487  | .7593   | 32.6444  | 14.9912    |            |
| 176.1000                            | 44.8461  | .7117   | 32.6624  | 14.0373    |            |
| 220.1250                            | 60.5858  | .7220   | 32.6803  | 13.8515    |            |
| 264.1500                            | 75.1694  | .7543   | 32.6983  | 14.1066    |            |
| 308.1750                            | 87.5194  | .8027   | 32.7163  | 14.4761    |            |
| 352.2000                            | 97.0852  | .8514   | 32.7343  | 14.9014    |            |
| 396.2250                            | 103.1777 | .8944   | 32.7523  | 15.2506    |            |
| 440.2500                            | 105.4993 | .9331   | 32.7702  | 15.5470    | DATA SET 6 |
| 484.2750                            | 105.5000 | .9460   | 32.7882  | 15.6588    |            |
| 528.3000                            | 105.5000 | .9344   | 32.8062  | 15.5500    |            |
| 572.3250                            | 105.5000 | .9047   | 32.8242  | 15.2558    |            |
| 616.3500                            | 105.5000 | .8493   | 32.8421  | 14.7393    |            |
| 660.3750                            | 103.2483 | .7761   | 32.8601  | 13.9642    |            |
| 704.4000                            | 95.5739  | .6947   | 32.8781  | 13.0293    |            |
| 748.4250                            | 83.7448  | .5989   | 32.8961  | 11.9877    |            |
| 792.4500                            | 66.9123  | .4948   | 32.9141  | 10.8378    |            |
| 836.4750                            | 44.8880  | .5134   | 21.9084  | 7.8858     |            |
| 880.5000                            | 19.1267  | .6031   | 6.7033   | 2.6247     |            |
| 9.5145                              | 37.3100  |         |          |            | DATA SET 7 |
| 389.1025                            | 0.0000   | 0.0000  |          |            |            |
| 792.4049                            | 0.0000   | 0.0000  |          |            |            |
| 1243.8223                           | 0.0000   | 0.0000  |          |            |            |
| 1034.9353                           | 0.0000   | 0.0000  |          |            |            |
| 1681.7071                           | 0.0000   | 0.0000  |          |            |            |
| 2040.0422                           | 0.0000   | 0.0000  |          |            |            |
| 2508.4206                           | 0.0000   | 0.0000  |          |            | DATA SET 9 |
| 2578.8111                           | 0.0000   | 0.0000  |          |            |            |
| 3053.3377                           | 0.0000   | 0.0000  |          |            |            |
| 3591.3250                           | 0.0000   | 0.0000  |          |            |            |
| 3530.8231                           | 0.0000   | 0.0000  |          |            |            |
| 3175.7759                           | 0.0000   | 0.0000  |          |            |            |
| 3725.5737                           | 0.0000   | 0.0000  |          |            |            |

The output can either be printed or plotted. The program option in Data Set 23 allows for the plotting of response amplitude operators as a function of heading and frequency and short term results as a function of heading and wave height. These plots are performed on a ZETA plotter at UCS center.

The printed output from SCOMOT depends on the option control tags set in data set 3 and the response selection from data set 23. Each output section will be described and can be seen in the sample output. The output is paginated for ease in binding and to facilitate the incorporation of output into reports. Each page has the program name, date and time of run, ship title and other descriptive headers.

The first part of the output is a listing of the basic input geometric and weight data (Page A1 to A2 of Appendix A). This is followed by the computed geometric and weight properties (page A3) and point motions data. The conditional cards for defining the speeds, headings and frequencies are given (Page A4). The output for the viscous roll damping is dependent upon which option is selected. If the simpler option is selected a natural roll frequency and added viscous roll damping is calculated. The other option displays hull properties and bilge keel description. The wave spectra and properties, probability of heading, type of sea spectrum and probability of each wave height group is printed (Page A5 to A6).

A table of frequency of encounter for various wave frequencies and wave lengths is outputed (Page A7 to A8). For each response selected in data set 23 the response amplitude operators, the short term values and long term statistics are printed (A9 to A73). Slamming, shipping of water and racing of the propeller statistics would be the final output (not shown). The results mentioned in this paragraph would be repeated for each speed selected.

## V. TIMING AND ERROR MESSAGES

The compilation time required for program SCOMOT is 6 cpu with about 64K of core needed to load the program and 56K for execution. The job file for compilation is shown in Table 1, Appendix C. The compiled (binary) version of SCOMOT is stored in a file called SMOTBIN and can be used for subsequent runs, therefore saving the compilation costs. Table 2, Appendix C, shows the job sequence needed for the execution of program SCOMOT using the compiled program.

The computation time for running Program SCOMOT varies tremendously and is a function of many variables. For computation time, it is convenient to discuss the program in two parts; the response amplitude operator calculation, and the short-term and long term responses.

The time to run regular wave responses are directly proportional to the number of speeds, the number of wave headings, the number of frequencies, and the number of ship sections. The SL-7 with 21 stations, one speed, 13 wave headings and 34 frequencies required 30 cpu for the regular wave response calculation. The short and long term calculations are a function of the number of wave groups, the number of spectra in each group, the number of frequencies, and the number of responses to be investigated. The SL-7 for the same run as above with 10 wave height groups, one spectra in each group, and 11 responses required 8 cpu of computation time in addition to the regular wave responses.

Various error messages may appear in the output and cause program termination. Each will be labeled with the subroutine which found the error, and a brief write-up explaining the error. Some of the messages are given below:

| <u>Subroutine</u> | <u>Error No.</u> | <u>Explanation</u>                                 |
|-------------------|------------------|--|
| PRELIMB/C         | 0                | Too many sta<br>wave lengths, wave<br>angles, etc. |

| <u>Subroutines</u> | <u>Error No.</u> | <u>Explanation</u>                                     |
|--------------------|------------------|--|
| PRELIMB            | 1                | Weight does not equal buoyancy                         |
| PRELIMB            | 2                | Integrated buoyancy does not equal given buoyancy      |
| PRELIMB            | 3                | Longitudinal centers of buoyancy and gravity not equal |

Array exceedance is caused by inputting more data than permitted. The following is a list of maximum numbers used by SCOMOT and is repeated in Chapter III.

|                               |    |
|-------------------------------|----|
| Stations                      | 21 |
| Speeds                        | 20 |
| Wave Headings                 | 25 |
| Wave Frequency                | 34 |
| Input motion points           | 30 |
| Wave height groups            | 15 |
| Spectra per wave height group | 12 |

If a file is to be used by SCOMOT, it must be saved on your user number. An error message will tell you if the program cannot find a file. The most common reason for this error is a misspelling of the file name. The second problem associated with the file manipulation involves an output file. It is not possible to save a file, such as the RAO file, if one already exists on the system with the same name.

VI. REFERENCES

1. Hoffman, D. and Zielinski, T.E., "Integrated Seakeeping Analysis (ISA) Computer Program", Hoffman Maritime Consultant, Inc., HMC Report 7660H, Oct. 1976.
2. Zielinski, T.E., "User Manual Program STATIC", USCG Report No. CG-M-6-79, July 1979.
3. Raff, A.I., "Program SCORES -- Ships Structural Response in Waves", SSC-230, 1972. NTIS AD 752468
4. Tanaka, "A Study on the Bilge Keels, Part 4, On the Eddy-Making Resistance to the Rolling of a Ship Hull," Journal of Naval Architects of Japan, Vol. 109 (1960).
5. Kato, "On the Frictional Resistance to the Rolling of Ships," Journal of Naval Architects of Japan, Vol. 102 (1958) (NSRDC Translation by C.M. Lee, 1966).
6. Comstock, J.P., ed., Principles of Naval Architecture, SNAME, New York, 1967.
7. Hoffman, D., Williamson, J. and Lewis, E.V., "Correlation of Model and Full Scale Results in Predicting Wave Bending Moment Trends", SSC-233, 1972. NTIS AD 753223
8. Hoffman, D. and Lewis, E.V., "Analysis and Interpolation of Full Scale Data on Midship Bending Stresses of Dry Cargo Ship", SSC-196, January 1969. NTIS AD 689657
9. Band, E.G.U., "Analysis of Ship Data to Predict Long Term Trends of Hull Bending Moments", ABS Report, November 1966.
10. Zubaly, R.B., "A Computer Program for Obtaining a Long Term Load Distribution", Lecture Notes, Summer Seminar on Application of Probability to Hull Structural Design, Webb Institute, August 1973.
11. Hoffman, D., "Further Analysis of Ocean Wave Spectra at Station India", Webb Report submitted to SNAME, March 1972.
12. Hoffman, D., "Analysis of Wave Spectra at Station "PAPA", NMRC-KP-173, October 1976.
13. Hoffman, D., "Analysis of Wave Spectra at Station K", for Naval Ship Systems Command, General Hydrodynamic Research Program, SNAME T & R Bulletin 1-38, 1980.

APPENDIX A

SAMPLE OUTPUT

## BASIC INPUT DATA

SL-7 - NORMAL FULL LOAD DEPARTURE

## JOB OPTION CONTROL TAGS

|   |   |   |   |   |   |   |   |   |   |    |   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|---|---|---|----|---|---|---|---|---|---|---|
| A | B | C | D | E | F | G | H | I | J | K  | L | M | N | O | P | Q | R |
| - | - | - | - | - | - | - | - | - | - | -  | - | - | - | - | - | - | - |
| 0 | 4 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 1 | 0 | 0 | C |

## SHIP DATA

## ENVIRONMENTAL DATA

SHIP LENGTH = 880.500 FEET  
 DISPLACEMENT= 47727.65 L.TONS

WATER DENSITY= .02857 L.TONS/ FEET \*\*\*3  
 ACCEL GRAVITY= 32.1740 FEET /SECOND\*\*2  
 K. VISCOSITY =1.106E-05 FEET \*\*2/SECOND

## SHIP SECTION DATA

| STATION<br>( FEET ) | SECTION<br>BREADTH<br>( FEET ) | SECTION AREA<br>COEFFICIENT | SECTION<br>DRAFT<br>( FEET ) | SECTION<br>CENTROID<br>( FEET ) |
|---------------------|--------------------------------|-----------------------------|------------------------------|---------------------------------|
| 0.0000              | 6.8217                         | 1.0000                      | 32.5905                      | 22.2506                         |
| 44.0250             | 6.0099                         | 1.7202                      | 32.6084                      | 19.1009                         |
| 88.0500             | 15.8877                        | .9570                       | 32.6264                      | 16.8238                         |
| 132.0750            | 29.0487                        | .7593                       | 32.6444                      | 14.9912                         |
| 176.1000            | 44.8461                        | .7117                       | 32.6624                      | 14.0373                         |
| 220.1250            | 60.5858                        | .7220                       | 32.6803                      | 13.8515                         |
| 264.1500            | 75.1694                        | .7543                       | 32.6983                      | 14.1066                         |
| 308.1750            | 87.5194                        | .8027                       | 32.7163                      | 14.4761                         |
| 352.2000            | 97.0852                        | .8514                       | 32.7343                      | 14.9014                         |
| 396.2250            | 103.1777                       | .8944                       | 32.7523                      | 15.2506                         |
| 440.2500            | 105.4993                       | .9331                       | 32.7702                      | 15.5470                         |
| 484.2750            | 105.5000                       | .9460                       | 32.7882                      | 15.6588                         |
| 528.3000            | 105.5000                       | .9344                       | 32.8062                      | 15.5500                         |
| 572.3250            | 105.5000                       | .9047                       | 32.8242                      | 15.2558                         |
| 616.3500            | 105.5000                       | .8493                       | 32.8421                      | 14.7393                         |
| 660.3750            | 103.2483                       | .7761                       | 32.8601                      | 13.9642                         |
| 704.4000            | 95.5739                        | .6947                       | 32.8781                      | 13.0293                         |
| 748.4250            | 83.7448                        | .5989                       | 32.8961                      | 11.9877                         |
| 792.4500            | 66.9123                        | .4948                       | 32.9141                      | 10.8378                         |
| 836.4750            | 44.8880                        | .5134                       | 21.9084                      | 7.8858                          |
| 880.5000            | 19.1267                        | .6031                       | 6.7033                       | 2.6247                          |

## BASIC INPUT DATA (CONTINUED)

SL-7 - NORMAL FULL LOAD DEPARTURE

## LATERAL PLANE DATA

-----  
VERTICAL C.G. ( ABOVE W.L. ) = 9.5145 FEET  
ROLL GYRADIUS = 37.3100 FEET

## SECTIONAL MASS PROPERTIES

| SEGMENT<br>WEIGHT<br>(L.TONS) | SEGMENT<br>VERTICAL C.G.<br>( FEET ) | SEGMENT<br>ROLL GYRADIUS<br>( FEET ) |
|-------------------------------|--------------------------------------|--------------------------------------|
| 389.1025                      | 0.0000                               | 37.3100                              |
| 792.4049                      | 0.0000                               | 37.3100                              |
| 1243.8223                     | 0.0000                               | 37.3100                              |
| 1034.9353                     | 0.0000                               | 37.3100                              |
| 1681.7071                     | 0.0000                               | 37.3100                              |
| 2040.0422                     | 0.0000                               | 37.3100                              |
| 2508.4206                     | 0.0000                               | 37.3100                              |
| 2578.8111                     | 0.0000                               | 37.3100                              |
| 3053.3377                     | 0.0000                               | 37.3100                              |
| 3591.3250                     | 0.0000                               | 37.3100                              |
| 3530.8231                     | 0.0000                               | 37.3100                              |
| 3175.7759                     | 0.0000                               | 37.3100                              |
| 3725.5737                     | 0.0000                               | 37.3100                              |
| 3530.6277                     | 0.0000                               | 37.3100                              |
| 2595.3904                     | 0.0000                               | 37.3100                              |
| 3151.4265                     | 0.0000                               | 37.3100                              |
| 2534.0626                     | 0.0000                               | 37.3100                              |
| 1915.6687                     | 0.0000                               | 37.3100                              |
| 1761.7314                     | 0.0000                               | 37.3100                              |
| 1430.9584                     | 0.0000                               | 37.3100                              |
| 1494.0527                     | 0.0000                               | 37.3100                              |

## MOMENT STATION DATA

-----  
FIRST STATION = 10  
LAST STATION = 10  
STATION INCREMENT = 1

## TOTAL RESISTANCE VARIATION

-----  
-0.0000 -0.0000 -0.0000 -0.0000

## COMPUTED RESULTS

## SL-7 - NORMAL FULL LOAD DEPARTURE

|                                   |   |          |        |
|-----------------------------------|---|----------|--------|
| WEIGHT                            | = | 47760.00 | L.TONS |
| DISPLACEMENT                      | = | 47703.13 | L.TONS |
| LONGITUDINAL C.B. (FROM MIDSHIPS) | = | -38.3886 | FEET   |
| LONGITUDINAL C.G. (FROM MIDSHIPS) | = | -38.6308 | FEET   |
| LONGITUDINAL GYRADIUS             | = | 213.2567 | FEET   |
| METACENTRIC HEIGHT (GM)           | = | 2.9028   | FEET   |
| VERTICAL C.G. (ABOVE KEEL)        | = | 42.3005  | FEET   |
| VERTICAL C.B. (ABOVE KEEL)        | = | 18.2290  | FEET   |

SHIP MOTION PROGRAM 77.1

02/23/81

12.29.26

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CONDITIONAL INPUT DATA

SL-7 - NORMAL FULL LOAD DEPARTURE

SHIP SPEEDS ( KNOTS )

25.0000

WAVE FREQUENCY ( RADIANS/SECOND )

|        |        |        |        |        |
|--------|--------|--------|--------|--------|
| .2000  | .2500  | .3000  | .3500  | .4000  |
| .4500  | .5000  | .5500  | .6000  | .6500  |
| .7000  | .7500  | .8000  | .8500  | .9000  |
| .9500  | 1.0000 | 1.0500 | 1.1000 | 1.1500 |
| 1.2000 | 1.2500 | 1.3000 | 1.3500 | 1.4000 |
| 1.4500 | 1.5000 | 1.5500 | 1.6000 | 1.6500 |
| 1.7000 | 1.7500 | 1.8000 |        |        |

WAVE ANGLE ( DEGREES )

|          |          |          |          |          |
|----------|----------|----------|----------|----------|
| 0.0000   | 15.0000  | 30.0000  | 45.0000  | 60.0000  |
| 75.0000  | 90.0000  | 105.0000 | 120.0000 | 135.0000 |
| 150.0000 | 165.0000 | 180.0000 |          |          |

ROLL DAMPING DATA

FRACTION OF CRITICAL ROLL DAMPING = 9.0000E-02

NATURAL ROLL FREQUENCY = .23847  
CALCULATED WAVE DAMPING IN ROLL = .1435E+04  
ADDITIONAL VISCOUS DAMPING IN ROLL = .1031E+06

## WAVE SPECTRA INPUT DATA

-----  
MATHEMATICAL SPECTRAL FORMULATION - TWO PARAMETER ISSC  
-----

|       |              |         |
|-------|--------------|---------|
| GROUP |              | 1       |
| 1     | SIG. WAVE HT | 2.4129  |
|       | MEAN PERIOD  | 6.9962  |
| GROUP |              | 1       |
| 2     | SIG. WAVE HT | 4.9325  |
|       | MEAN PERIOD  | 7.4339  |
| GROUP |              | 1       |
| 3     | SIG. WAVE HT | 7.3858  |
|       | MEAN PERIOD  | 8.2753  |
| GROUP |              | 1       |
| 4     | SIG. WAVE HT | 10.5710 |
|       | MEAN PERIOD  | 8.2770  |
| GROUP |              | 1       |
| 5     | SIG. WAVE HT | 13.9410 |
|       | MEAN PERIOD  | 8.8778  |
| GROUP |              | 1       |
| 6     | SIG. WAVE HT | 18.0000 |
|       | MEAN PERIOD  | 8.6434  |
| GROUP |              | 1       |
| 7     | SIG. WAVE HT | 23.6566 |
|       | MEAN PERIOD  | 9.3472  |
| GROUP |              | 1       |
| 8     | SIG. WAVE HT | 28.9330 |
|       | MEAN PERIOD  | 9.9297  |
| GROUP |              | 1       |
| 9     | SIG. WAVE HT | 37.2166 |
|       | MEAN PERIOD  | 11.2107 |
| GROUP |              | 1       |
| 10    | SIG. WAVE HT | 47.6925 |
|       | MEAN PERIOD  | 11.4870 |

## WAVE SPECTRA INPUT DATA

---

## WEIGHTED PROBABILITY OF HEADING ANGLES

---

|         |         |         |         |         |
|---------|---------|---------|---------|---------|
| 1.00000 | 1.00000 | 1.00000 | 1.00000 | 1.00000 |
| 1.00000 | 1.00000 | 1.00000 | 1.00000 | 1.00000 |
| 1.00000 | 1.00000 | 1.00000 | 1.00000 | 1.00000 |
| 1.00000 | 1.00000 | 1.00000 | 1.00000 | 1.00000 |
| 1.00000 | 1.00000 | 1.00000 | 1.00000 | 1.00000 |

## SHORT CRESTED SEA SPECTRUM

---

SPREADING = +/- 90.0000

POWER OF THE COSINE SPREADING FUNCTION = 2.00000

## PERCENT OCCURANCE OF EACH WAVE HEIGHT GROUP FOR - NORTH ATLANTIC ROUTING

---

|          |          |          |          |         |
|----------|----------|----------|----------|---------|
| 11.21001 | 36.52396 | 25.91602 | 13.68993 | 7.54400 |
| 2.23254  | 2.12576  | .74277   | .01212   | .00290  |

---

\*\*\*\*\* END OF WAVE INPUT DATA \*\*\*\*\*

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## FREQUENCY OF ENCOUNTER FOR VARIOUS HEADINGS ( RAD/SEC )

| WAVE   | WAVE/SHIP |          |          |          | W A V E  | A N G L E |       |        |
|--------|-----------|----------|----------|----------|----------|-----------|-------|--------|
| FREQ.  | LENGTH    | 0.00     | 15.00    | 30.00    | 45.00    | 60.00     | 75.00 | 90.00  |
| .2000  | 5.7398    | .1475    | .1493    | .1546    | .1629    | .1738     | .1864 | .2000  |
| .2500  | 3.6735    | .1680    | .1708    | .1790    | .1920    | .2090     | .2288 | .2500  |
| .3000  | 2.5510    | .1819    | .1860    | .1978    | .2165    | .2410     | .2694 | .3000  |
| .3500  | 1.8742    | .1893    | .1948    | .2108    | .2364    | .2697     | .3084 | .3500  |
| .4000  | 1.4349    | .1901    | .1973    | .2182    | .2516    | .2951     | .3457 | .4000  |
| .4500  | 1.1338    | .1844    | .1934    | .2200    | .2622    | .3172     | .3813 | .4500  |
| .5000  | .9184     | .1721    | .1832    | .2160    | .2681    | .3360     | .4151 | .5000  |
| .5500  | .7590     | .1532    | .1667    | .2064    | .2694    | .3516     | .4473 | .5500  |
| .6000  | .6378     | .1278    | .1439    | .1910    | .2661    | .3639     | .4778 | .6000  |
| .6500  | .5434     | .0958    | .1147    | .1700    | .2581    | .3729     | .5066 | .6500  |
| .7000  | .4686     | .0573    | .0792    | .1434    | .2455    | .3786     | .5336 | .7000  |
| .7500  | .4082     | .0121    | .0373    | .1110    | .2283    | .3811     | .5590 | .7500  |
| .8000  | .3587     | -.0395   | -.0109   | .0730    | .2064    | .3802     | .5827 | .8000  |
| .8500  | .3178     | -.0977   | -.0654   | .0292    | .1799    | .3761     | .6047 | .8500  |
| .9000  | .2834     | -.1625   | -.1263   | -.0202   | .1487    | .3687     | .6250 | .9000  |
| .9500  | .2544     | -.2338   | -.1935   | -.0752   | .1129    | .3581     | .6436 | .9500  |
| 1.0000 | .2296     | -.3117   | -.2670   | -.1360   | .0725    | .3441     | .6605 | 1.0000 |
| 1.0500 | .2082     | -.3962   | -.3469   | -.2024   | .0274    | .3269     | .6757 | 1.0500 |
| 1.1000 | .1897     | -.4872   | -.4331   | -.2746   | -.0223   | .3064     | .6892 | 1.1000 |
| 1.1500 | .1736     | -.5848   | -.5257   | -.3524   | -.0767   | .2826     | .7010 | 1.1500 |
| 1.2000 | .1594     | -.6889   | -.6245   | -.4358   | -.1357   | .2556     | .7111 | 1.2000 |
| 1.2500 | .1469     | -.7996   | -.7297   | -.5250   | -.1993   | .2252     | .7195 | 1.2500 |
| 1.3000 | .1359     | -.9168   | -.8413   | -.6198   | -.2675   | .1916     | .7262 | 1.3000 |
| 1.3500 | .1260     | -.10406  | -.9592   | -.7204   | -.3404   | .1547     | .7313 | 1.3500 |
| 1.4000 | .1171     | -.1.1710 | -.1.0834 | -.8266   | -.4180   | .1145     | .7346 | 1.4000 |
| 1.4500 | .1092     | -.1.3079 | -.1.2139 | -.9384   | -.5001   | .0710     | .7362 | 1.4500 |
| 1.5000 | .1020     | -.1.4514 | -.1.3508 | -.1.0560 | -.5870   | .0243     | .7361 | 1.5000 |
| 1.5500 | .0956     | -.1.6014 | -.1.4941 | -.1.1792 | -.6784   | -.0257    | .7343 | 1.5500 |
| 1.6000 | .0897     | -.1.7580 | -.1.6436 | -.1.3081 | -.7745   | -.0790    | .7309 | 1.6000 |
| 1.6500 | .0843     | -.1.9212 | -.1.7995 | -.1.4427 | -.8752   | -.1.3556  | .7257 | 1.6500 |
| 1.7000 | .0794     | -.2.0909 | -.1.9617 | -.1.5830 | -.9806   | -.1.9555  | .7188 | 1.7000 |
| 1.7500 | .0750     | -.2.2672 | -.2.1303 | -.1.7290 | -.1.0906 | -.2.586   | .7103 | 1.7500 |
| 1.8000 | .0709     | -.2.4500 | -.2.3052 | -.1.8806 | -.1.2052 | -.3.250   | .7000 | 1.8000 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## FREQUENCY OF ENCOUNTER FOR VARIOUS HEADINGS ( RAD/SEC )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |        |        |        |        |        |
|---------------|---------------------|---------------------|--------|--------|--------|--------|--------|
|               |                     | 105.00              | 120.00 | 135.00 | 150.00 | 165.00 | 180.00 |
| .2000         | 5.7398              | .2136               | .2262  | .2371  | .2454  | .2507  | .2525  |
| .2500         | 3.6735              | .2712               | .2910  | .3080  | .3210  | .3292  | .3320  |
| .3000         | 2.5510              | .3306               | .3590  | .3835  | .4022  | .4140  | .4181  |
| .3500         | 1.8742              | .3916               | .4303  | .4636  | .4892  | .5052  | .5107  |
| .4000         | 1.4349              | .4543               | .5049  | .5484  | .5818  | .6027  | .6099  |
| .4500         | 1.1338              | .5187               | .5828  | .6378  | .6800  | .7066  | .7156  |
| .5000         | .9184               | .5849               | .6640  | .7319  | .7840  | .8168  | .8279  |
| .5500         | .7590               | .6527               | .7484  | .8306  | .8936  | .9333  | .9468  |
| .6000         | .6378               | .7222               | .8361  | .9339  | 1.0090 | 1.0561 | 1.0722 |
| .6500         | .5434               | .7934               | .9271  | 1.0419 | 1.1300 | 1.1853 | 1.2042 |
| .7000         | .4686               | .8664               | 1.0214 | 1.1545 | 1.2566 | 1.3208 | 1.3427 |
| .7500         | .4082               | .9410               | 1.1189 | 1.2717 | 1.3890 | 1.4627 | 1.4879 |
| .8000         | .3587               | 1.0173              | 1.2198 | 1.3936 | 1.5270 | 1.6109 | 1.6395 |
| .8500         | .3178               | 1.0953              | 1.3239 | 1.5201 | 1.6708 | 1.7654 | 1.7977 |
| .9000         | .2834               | 1.1750              | 1.4313 | 1.6513 | 1.8202 | 1.9263 | 1.9625 |
| .9500         | .2544               | 1.2564              | 1.5419 | 1.7871 | 1.9752 | 2.0935 | 2.1338 |
| 1.0000        | .2296               | 1.3395              | 1.6559 | 1.9275 | 2.1360 | 2.2670 | 2.3117 |
| 1.0500        | .2082               | 1.4243              | 1.7731 | 2.0726 | 2.3024 | 2.4469 | 2.4962 |
| 1.1000        | .1897               | 1.5108              | 1.8936 | 2.2223 | 2.4746 | 2.6331 | 2.6872 |
| 1.1500        | .1736               | 1.5990              | 2.0174 | 2.3767 | 2.6524 | 2.8257 | 2.8848 |
| 1.2000        | .1594               | 1.6889              | 2.1444 | 2.5357 | 2.8358 | 3.0245 | 3.0889 |
| 1.2500        | .1469               | 1.7805              | 2.2748 | 2.6993 | 3.0250 | 3.2297 | 3.2996 |
| 1.3000        | .1359               | 1.8738              | 2.4084 | 2.8675 | 3.2198 | 3.4413 | 3.5168 |
| 1.3500        | .1260               | 1.9687              | 2.5453 | 3.0404 | 3.4204 | 3.6592 | 3.7406 |
| 1.4000        | .1171               | 2.0654              | 2.6855 | 3.2180 | 3.6266 | 3.8834 | 3.9710 |
| 1.4500        | .1092               | 2.1638              | 2.8290 | 3.4001 | 3.8384 | 4.1139 | 4.2079 |
| 1.5000        | .1020               | 2.2639              | 2.9757 | 3.5870 | 4.0560 | 4.3508 | 4.4514 |
| 1.5500        | .0956               | 2.3657              | 3.1257 | 3.7784 | 4.2792 | 4.5941 | 4.7014 |
| 1.6000        | .0897               | 2.4691              | 3.2790 | 3.9745 | 4.5081 | 4.8436 | 4.9580 |
| 1.6500        | .0843               | 2.5743              | 3.4356 | 4.1752 | 4.7427 | 5.0995 | 5.2212 |
| 1.7000        | .0794               | 2.6812              | 3.5955 | 4.3806 | 4.9830 | 5.3617 | 5.4909 |
| 1.7500        | .0750               | 2.7897              | 3.7586 | 4.5906 | 5.2290 | 5.6303 | 5.7672 |
| 1.8000        | .0709               | 2.9000              | 3.9250 | 4.8052 | 5.4806 | 5.9052 | 6.0500 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE HEAVE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | 0.00 DEG. |        | 15.00 DEG. |        | 30.00 DEG. |        | 45.00 DEG. |        |
|---------------|---------------------|-----------|--------|------------|--------|------------|--------|------------|--------|
|               |                     | AMPL.     | PHASE  | AMPL.      | PHASE  | AMPL.      | PHASE  | AMPL.      | PHASE  |
| .2000         | 5.7398              | .9559     | 180.0  | .9583      | 180.0  | .9651      | 179.9  | .9748      | 179.9  |
| .2500         | 3.6735              | .9024     | -179.9 | .9078      | -180.0 | .9228      | 180.0  | .9444      | 179.8  |
| .3000         | 2.5510              | .8157     | -179.7 | .8256      | -179.7 | .8536      | -179.9 | .8943      | 179.8  |
| .3500         | 1.8742              | .6916     | -179.1 | .7075      | -179.2 | .7527      | -179.5 | .8198      | 179.9  |
| .4000         | 1.4349              | .5342     | -178.0 | .5562      | -178.2 | .6204      | -178.8 | .7189      | -179.7 |
| .4500         | 1.1338              | .3578     | -176.2 | .3842      | -176.5 | .4640      | -177.4 | .5934      | -179.0 |
| .5000         | .9184               | .1866     | -177.0 | .2135      | -173.6 | .2991      | -175.2 | .4502      | -177.8 |
| .5500         | .7590               | .1775     | -173.1 | .2039      | -173.6 | .1471      | -171.5 | .3017      | -175.9 |
| .6000         | .6378               | .1653     | -173.1 | .1906      | -173.6 | .0299      | -161.9 | .1637      | -173.0 |
| .6500         | .5434               | .1499     | -173.1 | .1736      | -173.5 | .0383      | 13.0   | .0522      | -169.0 |
| .7000         | .4686               | .1313     | -173.1 | .1529      | -173.5 | .0362      | 13.0   | .0215      | 17.4   |
| .7500         | .4082               | .1096     | -173.2 | .1286      | -173.4 | .0336      | 13.0   | .0548      | 25.3   |
| .8000         | .3587               | .0847     | -173.3 | .1006      | -173.2 | .0306      | 12.9   | .0550      | 37.3   |
| .8500         | .3178               | .0566     | -173.5 | .0689      | -172.9 | .0272      | 12.8   | .0377      | 56.5   |
| .9000         | .2834               | .0254     | -174.2 | .0335      | -171.7 | .0233      | 12.7   | .0346      | 56.6   |
| .9500         | .2544               | .0090     | 10.8   | .0057      | -7.5   | .0190      | 12.5   | .0311      | 56.7   |
| 1.0000        | .2296               | .0079     | 35.2   | .0098      | 24.6   | .0142      | 12.2   | .0272      | 56.8   |
| 1.0500        | .2082               | .0023     | -168.5 | .0020      | 70.8   | .0090      | 11.5   | .0228      | 57.0   |
| 1.1000        | .1897               | .0055     | -140.3 | .0054      | -146.8 | .0036      | 40.6   | .0179      | 57.4   |
| 1.1500        | .1736               | .0026     | -175.0 | .0031      | -151.8 | .0041      | -164.3 | .0126      | 58.1   |
| 1.2000        | .1594               | .0004     | 155.9  | .0024      | 115.6  | .0042      | -149.3 | .0069      | 60.0   |
| 1.2500        | .1469               | .0088     | 36.9   | .0030      | -5.8   | .0008      | 141.0  | .0008      | 94.4   |
| 1.3000        | .1359               | .0060     | -153.2 | .0069      | 98.0   | .0019      | 53.1   | .0039      | 177.7  |
| 1.3500        | .1260               | .0035     | -36.3  | .0055      | -86.5  | .0031      | 28.2   | .0026      | -166.2 |
| 1.4000        | .1171               | .0022     | 62.4   | .0016      | 16.8   | .0039      | 129.5  | .0003      | -2.7   |
| 1.4500        | .1092               | .0017     | 173.4  | .0020      | 110.2  | .0049      | -71.3  | .0017      | 24.0   |
| 1.5000        | .1020               | .0010     | -112.4 | .0014      | -155.5 | .0018      | 24.0   | .0017      | 18.6   |
| 1.5500        | .0956               | .0007     | -11.0  | .0008      | -67.8  | .0019      | 123.4  | .0006      | 22.1   |
| 1.6000        | .0897               | .0007     | 99.2   | .0006      | 35.6   | .0012      | -153.1 | .0018      | -121.8 |
| 1.6500        | .0843               | .0004     | -173.5 | .0007      | 128.8  | .0009      | -56.7  | .0038      | -103.0 |
| 1.7000        | .0794               | .0005     | -43.8  | .0004      | -114.0 | .0006      | 39.2   | .0014      | -6.1   |
| 1.7500        | .0750               | .0005     | 67.5   | .0005      | -13.2  | .0007      | 129.3  | .0021      | 116.4  |
| 1.8000        | .0709               | .0005     | 171.0  | .0006      | 105.0  | .0006      | -121.3 | .0011      | -156.0 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE HEAVE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E |       | A N G L E |        | AMPL.  | PHASE | AMPL.  | PHASE  | AMPL. | PHASE | AMPL. | PHASE |
|---------------|---------------------|---------|-------|-----------|--------|--------|-------|--------|--------|-------|-------|-------|-------|
|               |                     | 60.00   | DEG.  | 75.00     | DEG.   |        |       |        |        |       |       |       |       |
| .2000         | 5.7398              | .9855   | 179.8 | .9950     | 179.8  | 1.0018 | 179.7 | 1.0049 | 179.7  |       |       |       |       |
| .2500         | 3.6735              | .9682   | 179.7 | .9892     | 179.5  | 1.0034 | 179.4 | 1.0088 | 179.4  |       |       |       |       |
| .3000         | 2.5510              | .9394   | 179.5 | .9793     | 179.2  | 1.0055 | 178.9 | 1.0136 | 178.8  |       |       |       |       |
| .3500         | 1.8742              | .8959   | 179.3 | .9639     | 178.6  | 1.0079 | 178.1 | 1.0196 | 178.0  |       |       |       |       |
| .4000         | 1.4349              | .8348   | 179.1 | .9413     | 177.9  | 1.0104 | 177.0 | 1.0276 | 176.8  |       |       |       |       |
| .4500         | 1.1338              | .7548   | 179.0 | .9100     | 176.9  | 1.0130 | 175.5 | 1.0402 | 175.3  |       |       |       |       |
| .5000         | .9184               | .6563   | 179.0 | .8687     | 175.7  | 1.0157 | 173.4 | 1.0639 | 173.1  |       |       |       |       |
| .5500         | .7590               | .5425   | 179.1 | .8165     | 174.2  | 1.0189 | 170.6 | 1.1198 | 169.7  |       |       |       |       |
| .6000         | .6378               | .4191   | 179.5 | .7531     | 172.4  | 1.0228 | 166.9 | 1.2377 | 162.4  |       |       |       |       |
| .6500         | .5434               | .2942   | 179.8 | .6786     | 170.0  | 1.0258 | 161.8 | 1.4070 | 144.3  |       |       |       |       |
| .7000         | .4686               | .1774   | 179.6 | .5946     | 167.1  | 1.0292 | 154.8 | 1.2598 | 110.5  |       |       |       |       |
| .7500         | .4082               | .0786   | 175.3 | .5032     | 163.2  | 1.0219 | 144.6 | .7238  | 79.4   |       |       |       |       |
| .8000         | .3587               | .0169   | 106.1 | .4082     | 158.1  | .9751  | 129.7 | .3285  | 64.2   |       |       |       |       |
| .8500         | .3178               | .0485   | 35.5  | .3143     | 150.9  | .8273  | 110.4 | .1279  | 64.2   |       |       |       |       |
| .9000         | .2834               | .0669   | 34.2  | .2281     | 139.9  | .5851  | 91.6  | .0421  | 100.8  |       |       |       |       |
| .9500         | .2544               | .0637   | 39.0  | .1576     | 122.4  | .3676  | 79.1  | .0409  | 160.5  |       |       |       |       |
| 1.0000        | .2296               | .0462   | 45.4  | .1129     | 94.5   | .2220  | 73.5  | .0480  | 176.8  |       |       |       |       |
| 1.0500        | .2082               | .0237   | 49.5  | .0982     | 60.4   | .1338  | 72.6  | .0451  | -179.1 |       |       |       |       |
| 1.1000        | .1897               | .0061   | 8.7   | .1019     | 33.4   | .0816  | 75.4  | .0364  | -177.7 |       |       |       |       |
| 1.1500        | .1736               | .0125   | -62.6 | .1050     | 14.5   | .0504  | 81.9  | .0258  | -176.9 |       |       |       |       |
| 1.2000        | .1594               | .0168   | -54.5 | .1006     | -.5    | .0323  | 88.6  | .0156  | -175.7 |       |       |       |       |
| 1.2500        | .1469               | .0138   | -37.5 | .0903     | -14.7  | .0214  | 93.7  | .0075  | -171.5 |       |       |       |       |
| 1.3000        | .1359               | .0060   | -13.3 | .0757     | -30.5  | .0144  | 93.3  | .0020  | -144.2 |       |       |       |       |
| 1.3500        | .1260               | .0056   | -14.9 | .0611     | -48.9  | .0099  | 84.5  | .0020  | -37.0  |       |       |       |       |
| 1.4000        | .1171               | .0052   | -16.8 | .0486     | -70.4  | .0075  | 65.3  | .0031  | -22.8  |       |       |       |       |
| 1.4500        | .1092               | .0048   | -19.3 | .0379     | -95.4  | .0070  | 43.0  | .0028  | -20.6  |       |       |       |       |
| 1.5000        | .1020               | .0044   | -22.4 | .0332     | -123.7 | .0075  | 26.9  | .0018  | -20.4  |       |       |       |       |
| 1.5500        | .0956               | .0039   | -26.6 | .0328     | -146.8 | .0079  | 17.5  | .0006  | -16.8  |       |       |       |       |
| 1.6000        | .0897               | .0035   | -32.1 | .0311     | -163.7 | .0080  | 12.1  | .0004  | 139.3  |       |       |       |       |
| 1.6500        | .0843               | .0031   | -39.6 | .0261     | -175.4 | .0075  | 8.8   | .0009  | 142.3  |       |       |       |       |
| 1.7000        | .0794               | .0027   | -49.9 | .0174     | 170.9  | .0067  | 6.6   | .0010  | 137.4  |       |       |       |       |
| 1.7500        | .0750               | .0020   | -20.9 | .0093     | 132.4  | .0056  | 5.1   | .0007  | 127.7  |       |       |       |       |
| 1.8000        | .0709               | .0011   | -19.9 | .0115     | 77.3   | .0043  | 3.8   | .0003  | 101.1  |       |       |       |       |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE HEAVE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | 120.00 DEG.<br>AMPL. | PHASE  | 135.00 DEG.<br>AMPL. | PHASE  | 150.00 DEG.<br>AMPL. | PHASE  | 165.00 DEG.<br>AMPL. | PHASE  |
|---------------|---------------------|----------------------|--------|----------------------|--------|----------------------|--------|----------------------|--------|
| .2000         | 5.7398              | 1.0044               | 179.7  | 1.0014               | 179.7  | .9975                | 179.7  | .9944                | 179.7  |
| .2500         | 3.6735              | 1.0056               | 179.4  | .9968                | 179.4  | .9864                | 179.5  | .9782                | 179.6  |
| .3000         | 2.5510              | 1.0050               | 178.9  | .9856                | 179.1  | .9639                | 179.5  | .9474                | 179.8  |
| .3500         | 1.8742              | 1.0022               | 178.3  | .9679                | 179.0  | .9320                | 179.9  | .9061                | -179.3 |
| .4000         | 1.4349              | 1.0006               | 177.6  | .9541                | 179.3  | .9128                | -178.8 | .8881                | -177.3 |
| .4500         | 1.1338              | 1.0138               | 176.8  | .9852                | 179.1  | .9823                | -179.7 | .9876                | 179.4  |
| .5000         | .9184               | 1.0825               | 174.5  | 1.1392               | 170.9  | 1.1518               | 158.5  | 1.0411               | 144.6  |
| .5500         | .7590               | 1.2745               | 163.8  | 1.1958               | 134.4  | .6414                | 101.7  | .2860                | 87.8   |
| .6000         | .6378               | 1.3298               | 129.1  | .4692                | 83.4   | .0417                | 113.9  | .0998                | -153.6 |
| .6500         | .5434               | .6884                | 84.4   | .0372                | 116.1  | .1182                | -157.8 | .1226                | -160.8 |
| .7000         | .4686               | .1827                | 65.7   | .1013                | -161.4 | .0985                | -165.6 | .0704                | -170.2 |
| .7500         | .4082               | .0390                | 157.4  | .0942                | -166.7 | .0509                | -173.0 | .0224                | -178.6 |
| .8000         | .3587               | .0805                | -169.1 | .0584                | -172.1 | .0130                | -179.6 | .0032                | -7.6   |
| .8500         | .3178               | .0776                | -170.5 | .0237                | -176.8 | .0054                | -13.8  | .0089                | -20.4  |
| .9000         | .2834               | .0560                | -173.2 | .0019                | -157.3 | .0084                | -23.6  | .0050                | -45.5  |
| .9500         | .2544               | .0313                | -175.8 | .0073                | -19.1  | .0044                | -47.7  | .0021                | -131.4 |
| 1.0000        | .2296               | .0117                | -175.6 | .0070                | -28.3  | .0019                | -135.2 | .0021                | 172.3  |
| 1.0500        | .2082               | .0014                | -66.6  | .0032                | -52.7  | .0020                | 169.5  | .0006                | 124.8  |
| 1.1000        | .1897               | .0060                | -22.2  | .0015                | -150.0 | .0008                | 129.9  | .0007                | -13.1  |
| 1.1500        | .1736               | .0059                | -25.7  | .0019                | 161.7  | .0006                | -6.1   | .0005                | -54.2  |
| 1.2000        | .1594               | .0033                | -36.5  | .0009                | 130.1  | .0006                | -46.3  | .0003                | -173.4 |
| 1.2500        | .1469               | .0007                | -93.5  | .0004                | 12.6   | .0002                | -143.8 | .0002                | 125.5  |
| 1.3000        | .1359               | .0014                | 161.1  | .0006                | -39.3  | .0002                | 139.4  | .0001                | -6.6   |
| 1.3500        | .1260               | .0015                | 140.8  | .0003                | -90.9  | .0001                | 36.8   | .0001                | -71.5  |
| 1.4000        | .1171               | .0008                | 115.5  | .0002                | 160.3  | .0001                | -57.3  | .0002                | 119.9  |
| 1.4500        | .1092               | .0003                | 20.9   | .0002                | 101.2  | .0001                | -152.0 | .0000                | 123.6  |
| 1.5000        | .1020               | .0005                | -41.4  | .0001                | -11.7  | .0000                | 76.3   | .0000                | -150.4 |
| 1.5500        | .0956               | .0004                | -76.4  | .0001                | -92.2  | .0000                | -91.3  | .0000                | 63.4   |
| 1.6000        | .0897               | .0002                | -154.9 | .0000                | -167.6 | .0000                | -162.0 | .0001                | 21.5   |
| 1.6500        | .0843               | .0002                | 126.5  | .0001                | 67.3   | .0001                | 61.6   | .0001                | -167.9 |
| 1.7000        | .0794               | .0002                | 74.3   | .0000                | -24.2  | .0000                | -28.8  | .0001                | 88.7   |
| 1.7500        | .0750               | .0001                | -7.1   | .0001                | -132.0 | .0001                | 50.9   | .0000                | -78.0  |
| 1.8000        | .0709               | .0001                | -83.0  | .0000                | 126.5  | .0000                | 94.9   | .0001                | -138.5 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE HEAVE DISPLACEMENT ( FEET / FEET )

## W A V E   A N G L E

| WAVE FREQ. | WAVE/SHIP LENGTH | AMPL. | PHASE  |
|------------|------------------|-------|--------|
| .2000      | 5.7398           | .9932 | 179.7  |
| .2500      | 3.6735           | .9751 | 179.6  |
| .3000      | 2.5510           | .9414 | 179.9  |
| .3500      | 1.8742           | .8969 | -179.0 |
| .4000      | 1.4349           | .8803 | -176.9 |
| .4500      | 1.1338           | .9891 | 178.6  |
| .5000      | .9184            | .9752 | 139.0  |
| .5500      | .7590            | .1916 | 36.5   |
| .6000      | .6378            | .1189 | -152.4 |
| .6500      | .5434            | .1174 | -162.2 |
| .7000      | .4686            | .0597 | -171.9 |
| .7500      | .4082            | .0145 | 178.9  |
| .8000      | .3587            | .0062 | -9.4   |
| .8500      | .3178            | .0084 | -24.9  |
| .9000      | .2834            | .0036 | -61.1  |
| .9500      | .2544            | .0023 | -156.2 |
| 1.0000     | .2296            | .0017 | 163.0  |
| 1.0500     | .2082            | .0004 | 56.2   |
| 1.1000     | .1897            | .0008 | -26.4  |
| 1.1500     | .1736            | .0003 | -86.7  |
| 1.2000     | .1594            | .0003 | 159.2  |
| 1.2500     | .1469            | .0001 | 65.4   |
| 1.3000     | .1359            | .0002 | -34.7  |
| 1.3500     | .1260            | .0001 | -103.0 |
| 1.4000     | .1171            | .0000 | -162.1 |
| 1.4500     | .1092            | .0000 | -140.5 |
| 1.5000     | .1020            | .0000 | 128.1  |
| 1.5500     | .0956            | .0001 | 45.1   |
| 1.6000     | .0897            | .0001 | -179.3 |
| 1.6500     | .0843            | .0005 | 66.9   |
| 1.7000     | .0794            | .0000 | 52.1   |
| 1.7500     | .0750            | .0001 | -119.2 |
| 1.8000     | .0709            | .0000 | 80.2   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM HEAVE DISPLACEMENT ( FEET )

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 2.3892E-01          | .39153           | 800.8    |
| 4.879                | 5.5412E-01          | .40328           | 778.3    |
| 7.334                | 9.9737E-01          | .45007           | 735.6    |
| 10.497               | 1.4279E+00          | .43012           | 735.6    |
| 13.867               | 2.0723E+00          | .45084           | 705.9    |
| 17.894               | 2.5851E+00          | .44271           | 717.4    |
| 23.554               | 3.7331E+00          | .46701           | 683.4    |
| 28.835               | 4.8496E+00          | .48638           | 656.5    |
| 37.139               | 6.8661E+00          | .52463           | 601.8    |
| 47.602               | 8.9415E+00          | .53200           | 590.8    |

Note:

This is abbreviated Short Term.

When detailed Short Term is specified, the "average" is weighted on basis of heading probability.

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .9609              | 1.2275E+00 | 1.3125E+00           | 1.3647E+00 | 1.3934E+00 |
| 4.879                | .9585              | 2.7864E+00 | 2.9793E+00           | 3.0978E+00 | 3.1630E+00 |
| 7.334                | .9526              | 4.8270E+00 | 5.1595E+00           | 5.3643E+00 | 5.4763E+00 |
| 10.497               | .9526              | 6.9104E+00 | 7.3863E+00           | 7.6795E+00 | 7.8398E+00 |
| 13.867               | .9478              | 9.7912E+00 | 1.0461E+01           | 1.0874E+01 | 1.1099E+01 |
| 17.894               | .9497              | 1.2325E+01 | 1.3170E+01           | 1.3692E+01 | 1.3976E+01 |
| 23.554               | .9439              | 1.7335E+01 | 1.8514E+01           | 1.9242E+01 | 1.9639E+01 |
| 28.835               | .9390              | 2.2065E+01 | 2.3559E+01           | 2.4482E+01 | 2.4984E+01 |
| 37.139               | .9286              | 2.9925E+01 | 3.1946E+01           | 3.3191E+01 | 3.3871E+01 |
| 47.602               | .9265              | 3.8619E+01 | 4.1229E+01           | 4.2834E+01 | 4.3713E+01 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM HEAVE DISPLACEMENT ( FEET )

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 3.5507E+00        | 5.2012E-02                   | 1.28                   | 5.2012E+06        | 9.4799E+07 |
| 7.1015E+00        | 7.1856E-03                   | 2.14                   | 7.1856E+05        | 4.4826E+06 |
| 1.0652E+01        | 1.3472E-03                   | 2.87                   | 1.3472E+05        | 5.8384E+05 |
| 1.4203E+01        | 2.2578E-04                   | 3.65                   | 2.2578E+04        | 1.1214E+05 |
| 1.7754E+01        | 3.3807E-05                   | 4.47                   | 3.3807E+03        | 1.9197E+04 |
| 2.1304E+01        | 5.3598E-06                   | 5.27                   | 5.3598E+02        | 2.8447E+03 |
| 2.4855E+01        | 1.1170E-06                   | 5.95                   | 1.1170E+02        | 4.2428E+02 |
| 2.8406E+01        | 2.9667E-07                   | 6.53                   | 2.9667E+01        | 8.2032E+01 |
| 3.1957E+01        | 8.2742E-08                   | 7.08                   | 8.2742E+00        | 2.1393E+01 |
| 3.5507E+01        | 2.1857E-08                   | 7.66                   | 2.1857E+00        | 6.0885E+00 |
| 3.9058E+01        | 5.2737E-09                   | 8.28                   | 5.2737E-01        | 1.6583E+00 |
| 4.2609E+01        | 1.1438E-09                   | 8.94                   | 1.1438E-01        | 4.1300E-01 |
| 4.6160E+01        | 2.2109E-10                   | 9.66                   | 2.2109E-02        | 9.2267E-02 |
| 4.9710E+01        | 3.7934E-11                   | 10.42                  | 3.7934E-03        | 1.8315E-02 |
| 5.3261E+01        | 5.7673E-12                   | 11.24                  | 5.7673E-04        | 3.2166E-03 |
| 5.6812E+01        | 7.7651E-13                   | 12.11                  | 7.7651E-05        | 4.9908E-04 |
| 6.0362E+01        | 9.2572E-14                   | 13.03                  | 9.2572E-06        | 6.8393E-05 |
| 6.3913E+01        | 9.7711E-15                   | 14.01                  | 9.7711E-07        | 8.2801E-06 |
| 6.7464E+01        | 9.1309E-16                   | 15.04                  | 9.1309E-08        | 8.8581E-07 |
| 7.1015E+01        | 7.5532E-17                   | 16.12                  | 7.5532E-09        | 8.3756E-08 |
| 7.4565E+01        | 5.5299E-18                   | 17.26                  | 5.5299E-10        | 7.0002E-09 |
| 7.8116E+01        | 3.5826E-19                   | 18.45                  | 3.5826E-11        | 5.1716E-10 |
| 8.1667E+01        | 2.0534E-20                   | 19.69                  | 2.0534E-12        | 3.3772E-11 |
| 8.5218E+01        | 1.0410E-21                   | 20.98                  | 1.0410E-13        | 1.9493E-12 |
| 8.8768E+01        | 4.6675E-23                   | 22.33                  | 4.6675E-15        | 9.9434E-14 |
| 9.2319E+01        | 1.8505E-24                   | 23.73                  | 1.8505E-16        | 4.4825E-15 |
| 9.5870E+01        | 6.4866E-26                   | 25.19                  | 6.4866E-18        | 1.7856E-16 |
| 9.9421E+01        | 2.0102E-27                   | 26.70                  | 2.0102E-19        | 6.2856E-18 |
| 1.0297E+02        | 5.5070E-29                   | 28.26                  | 5.5070E-21        | 1.9551E-19 |
| 1.0652E+02        | 1.3337E-30                   | 29.87                  | 1.3337E-22        | 5.3737E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 1.5726E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 2.0102E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 2.5151E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 3.1430E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 3.7460E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 4.2899E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 4.7758E+01 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE PITCH DISPLACEMENT (DEGREE/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   |            | A N G L E  |            | WAVE<br>AMPL. | WAVE<br>PHASE | WAVE<br>AMPL. | WAVE<br>PHASE | WAVE<br>AMPL. | WAVE<br>PHASE | WAVE<br>AMPL. | WAVE<br>PHASE |
|---------------|---------------------|-----------|------------|------------|------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
|               |                     | 0.00 DEG. | 15.00 DEG. | 30.00 DEG. | 45.00 DEG. |               |               |               |               |               |               |               |               |
| .2000         | 5.7398              | .0665     | -89.2      | .0644      | -89.2      | .0583         | -89.5         | .0483         | -90.0         | .0729         | -89.3         | .0994         | -88.1         |
| .2500         | 3.6735              | .0980     | -88.0      | .0952      | -88.2      | .0869         | -88.5         | .0729         | -89.3         | .1248         | -86.6         | .1453         | -84.4         |
| .3000         | 2.5510              | .1284     | -86.4      | .1254      | -86.6      | .1161         | -87.1         | .1099         | -88.0         | .1566         | -82.5         | .1554         | -77.9         |
| .3500         | 1.8742              | .1513     | -84.2      | .1490      | -84.4      | .1412         | -85.1         | .1404         | -73.1         | .1574         | -79.0         | .1554         | -77.9         |
| .4000         | 1.4349              | .1601     | -81.2      | .1597      | -81.5      | .1566         | -82.5         | .1426         | -42.6         | .1597         | -71.3         | .1453         | -84.4         |
| .4500         | 1.1338              | .1499     | -77.3      | .1524      | -77.7      | .1574         | -79.0         | .1566         | -81.6         | .1524         | -77.7         | .1554         | -77.9         |
| .5000         | .9184               | .1208     | -71.9      | .1265      | -72.5      | .1412         | -74.3         | .1554         | -77.9         | .0702         | -58.8         | .1130         | -66.7         |
| .5500         | .7590               | .1156     | -71.8      | .1214      | -72.5      | .1099         | -68.0         | .1404         | -73.1         | .0994         | -88.1         | .1248         | -86.6         |
| .6000         | .6378               | .1087     | -71.6      | .1145      | -72.5      | .0702         | -58.8         | .0426         | -43.2         | .0948         | -84.2         | .0154         | -7.7          |
| .6500         | .5434               | .0999     | -71.4      | .1056      | -72.4      | .0327         | -41.9         | .0780         | -57.6         | .0948         | -84.2         | .0106         | 91.8          |
| .7000         | .4686               | .0893     | -71.1      | .0948      | -72.4      | .0307         | -41.5         | .0426         | -43.2         | .0948         | -84.2         | .0132         | 132.7         |
| .7500         | .4082               | .0769     | -70.5      | .0820      | -72.3      | .0284         | -41.0         | .0154         | -7.7          | .0948         | -84.2         | .0122         | 130.4         |
| .8000         | .3587               | .0627     | -69.7      | .0674      | -72.2      | .0257         | -40.3         | .0106         | 91.8          | .0948         | -84.2         | .0141         | 134.5         |
| .8500         | .3178               | .0468     | -68.1      | .0508      | -72.0      | .0225         | -39.3         | .0088         | 117.0         | .0948         | -84.2         | .0132         | 132.7         |
| .9000         | .2834               | .0292     | -64.4      | .0322      | -71.6      | .0190         | -37.7         | .0077         | 108.5         | .0948         | -84.2         | .0122         | 130.4         |
| .9500         | .2544               | .0104     | -45.6      | .0118      | -69.4      | .0151         | -35.0         | .0067         | 96.3          | .0948         | -84.2         | .0111         | 127.2         |
| 1.0000        | .2296               | .0077     | 49.4       | .0071      | 10.1       | .0108         | -29.9         | .0100         | 123.0         | .0948         | -84.2         | .0088         | 117.0         |
| 1.0500        | .2082               | .0088     | 120.2      | .0086      | 95.4       | .0064         | -16.7         | .0061         | 79.4          | .0948         | -84.2         | .0077         | 108.5         |
| 1.1000        | .1897               | .0058     | -157.5     | .0065      | 161.3      | .0072         | 74.6          | .0049         | -56.9         | .0948         | -84.2         | .0067         | 96.3          |
| 1.1500        | .1736               | .0068     | -63.2      | .0058      | -97.2      | .0063         | 133.3         | .0034         | 24.5          | .0948         | -84.2         | .0056         | -147.6        |
| 1.2000        | .1594               | .0051     | 25.8       | .0058      | -21.5      | .0044         | -135.2        | .0033         | -125.2        | .0948         | -84.2         | .0043         | -154.8        |
| 1.2500        | .1469               | .0056     | 148.7      | .0045      | 89.6       | .0049         | -56.9         | .0031         | -60.9         | .0948         | -84.2         | .0038         | 143.2         |
| 1.3000        | .1359               | .0033     | -98.0      | .0048      | -160.4     | .0034         | 24.5          | .0020         | 11.9          | .0948         | -84.2         | .0020         | 11.9          |
| 1.3500        | .1260               | .0018     | 15.2       | .0022      | -39.1      | .0036         | 129.2         | .0018         | 99.9          | .0948         | -84.2         | .0016         | -32.1         |
| 1.4000        | .1171               | .0014     | 78.1       | .0014      | 48.7       | .0032         | -138.3        | .0015         | 35.7          | .0948         | -84.2         | .0015         | 35.7          |
| 1.4500        | .1092               | .0007     | -173.9     | .0010      | 109.3      | .0018         | -17.9         | .0008         | -132.0        | .0948         | -84.2         | .0010         | 140.6         |
| 1.5000        | .1020               | .0006     | -94.3      | .0007      | -133.3     | .0013         | 53.8          | .0008         | 123.5         | .0948         | -84.2         | .0010         | -147.6        |
| 1.5500        | .0956               | .0005     | 2.9        | .0005      | -54.3      | .0006         | -48.4         | .0005         | 144.2         | .0948         | -84.2         | .0010         | -147.6        |
| 1.6000        | .0897               | .0004     | 95.1       | .0005      | 36.3       | .0006         | 40.1          | .0005         | -124.9        | .0948         | -84.2         | .0010         | 140.6         |
| 1.6500        | .0843               | .0004     | -153.3     | .0004      | 146.6      | .0006         | -48.4         | .0005         | 104.1         | .0948         | -84.2         | .0010         | -147.6        |
| 1.7000        | .0794               | .0004     | -44.3      | .0004      | -119.3     | .0006         | 40.1          | .0005         | 144.2         | .0948         | -84.2         | .0010         | -147.6        |
| 1.7500        | .0750               | .0004     | 65.0       | .0004      | -1.7       | .0005         | 144.2         | .0005         | -124.9        | .0948         | -84.2         | .0010         | 140.6         |
| 1.8000        | .0709               | .0004     | -169.6     | .0004      | 104.1      | .0005         | -141.6        | .0948         | -84.2         | .0948         | -84.2         | .0010         | -147.6        |

**SL-7 - NORMAL FULL LOAD DEPARTURE**

SPEED = 25,000 KNOTS

REGULAR WAVE PITCH DISPLACEMENT (DEGREE/ FEET )

| WAVE   | WAVE/SHIP | 60.00 DEG. |        | W A V E    | A N G L E  |             |        |
|--------|-----------|------------|--------|------------|------------|-------------|--------|
| FREQ.  | LENGTH    | AMPL.      | PHASE  | 75.00 DEG. | 90.00 DEG. | 105.00 DEG. |        |
| .2000  | 5.7398    | .0348      | -90.8  | .0185      | -92.9      | .0012       | -156.8 |
| .2500  | 3.6735    | .0533      | -90.5  | .0287      | -93.2      | .0021       | -164.9 |
| .3000  | 2.5510    | .0743      | -89.9  | .0408      | -93.4      | .0033       | -173.1 |
| .3500  | 1.8742    | .0966      | -88.9  | .0545      | -93.4      | .0048       | 178.3  |
| .4000  | 1.4349    | .1182      | -87.6  | .0695      | -93.3      | .0066       | 169.2  |
| .4500  | 1.1338    | .1369      | -85.9  | .0851      | -93.1      | .0087       | 159.6  |
| .5000  | .9184     | .1502      | -83.6  | .1008      | -92.7      | .0113       | 149.2  |
| .5500  | .7590     | .1557      | -80.8  | .1158      | -92.2      | .0144       | 137.6  |
| .6000  | .6378     | .1518      | -77.1  | .1290      | -91.5      | .0182       | 124.3  |
| .6500  | .5434     | .1380      | -72.5  | .1395      | -90.6      | .0233       | 108.9  |
| .7000  | .4686     | .1152      | -66.7  | .1462      | -89.5      | .0296       | 89.0   |
| .7500  | .4082     | .0862      | -59.1  | .1482      | -88.2      | .0373       | 64.3   |
| .8000  | .3587     | .0549      | -48.5  | .1449      | -86.5      | .0442       | 32.6   |
| .8500  | .3178     | .0262      | -29.5  | .1357      | -84.5      | .0452       | -4.6   |
| .9000  | .2834     | .0088      | 42.4   | .1210      | -82.0      | .0374       | -40.2  |
| .9500  | .2544     | .0157      | 120.5  | .1013      | -78.8      | .0272       | -67.3  |
| 1.0000 | .2296     | .0201      | 144.1  | .0779      | -74.8      | .0192       | -86.0  |
| 1.0500 | .2082     | .0171      | 161.4  | .0523      | -68.9      | .0139       | -98.9  |
| 1.1000 | .1897     | .0096      | 178.1  | .0274      | -58.7      | .0102       | -108.3 |
| 1.1500 | .1736     | .0010      | -168.2 | .0071      | -10.7      | .0075       | -114.0 |
| 1.2000 | .1594     | .0053      | 38.4   | .0152      | 97.7       | .0056       | -118.1 |
| 1.2500 | .1469     | .0074      | 61.9   | .0265      | 115.1      | .0043       | -121.7 |
| 1.3000 | .1359     | .0056      | 96.4   | .0311      | 126.1      | .0031       | -123.0 |
| 1.3500 | .1260     | .0049      | 94.3   | .0288      | 137.9      | .0023       | -122.7 |
| 1.4000 | .1171     | .0042      | 91.4   | .0212      | 154.2      | .0016       | -121.5 |
| 1.4500 | .1092     | .0033      | 86.6   | .0114      | -170.9     | .0011       | -117.4 |
| 1.5000 | .1020     | .0025      | 78.2   | .0093      | -89.6      | .0007       | -109.6 |
| 1.5500 | .0956     | .0017      | 60.6   | .0160      | -42.7      | .0004       | -96.8  |
| 1.6000 | .0897     | .0013      | 22.9   | .0206      | -18.0      | .0003       | -76.6  |
| 1.6500 | .0843     | .0017      | -18.9  | .0206      | 5.5        | .0002       | -51.1  |
| 1.7000 | .0794     | .0026      | -39.8  | .0168      | 35.9       | .0002       | -28.5  |
| 1.7500 | .0750     | .0019      | 54.7   | .0130      | 82.7       | .0001       | -13.5  |
| 1.8000 | .0709     | .0015      | 140.2  | .0135      | 139.2      | .0001       | -2.7   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE PITCH DISPLACEMENT (DEGREE/ FEET )

| WAVE   | WAVE/SHIP | 120.00 DEG. |        | 135.00 DEG. |        | 150.00 DEG. |        | 165.00 DEG. |        |
|--------|-----------|-------------|--------|-------------|--------|-------------|--------|-------------|--------|
| FREQ.  | LENGTH    | AMPL.       | PHASE  | AMPL.       | PHASE  | AMPL.       | PHASE  | AMPL.       | PHASE  |
| .2000  | 5.7398    | .0356       | 90.6   | .0508       | 89.5   | .0626       | 88.8   | .0699       | 88.4   |
| .2500  | 3.6735    | .0571       | 89.5   | .0815       | 87.9   | .1002       | 86.8   | .1118       | 86.1   |
| .3000  | 2.5510    | .0849       | 87.6   | .1209       | 85.1   | .1479       | 83.3   | .1645       | 82.2   |
| .3500  | 1.8742    | .1200       | 84.6   | .1697       | 80.8   | .2058       | 77.9   | .2271       | 76.0   |
| .4000  | 1.4349    | .1636       | 79.9   | .2286       | 74.0   | .2726       | 69.2   | .2964       | 65.8   |
| .4500  | 1.1338    | .2171       | 72.8   | .2964       | 63.2   | .3422       | 54.6   | .3604       | 48.3   |
| .5000  | .9184     | .2809       | 61.7   | .3637       | 45.1   | .3866       | 28.2   | .3681       | 15.2   |
| .5500  | .7590     | .3512       | 43.5   | .3832       | 12.4   | .2779       | -15.5  | .1885       | -30.2  |
| .6000  | .6378     | .3780       | 12.6   | .2290       | -27.2  | .0981       | -46.7  | .0425       | -58.0  |
| .6500  | .5434     | .2601       | -22.6  | .0884       | -49.2  | .0112       | -68.8  | .0143       | 123.0  |
| .7000  | .4686     | .1340       | -42.8  | .0176       | -62.0  | .0196       | 110.5  | .0258       | 104.4  |
| .7500  | .4082     | .0583       | -53.4  | .0126       | 107.1  | .0229       | 99.2   | .0183       | 91.9   |
| .8000  | .3587     | .0169       | -56.8  | .0202       | 99.6   | .0146       | 87.7   | .0070       | 73.1   |
| .8500  | .3178     | .0056       | 87.0   | .0164       | 91.2   | .0049       | 67.1   | .0018       | -49.1  |
| .9000  | .2834     | .0138       | 95.6   | .0088       | 80.0   | .0019       | -66.8  | .0033       | -102.3 |
| .9500  | .2544     | .0143       | 91.8   | .0021       | 48.5   | .0031       | -105.3 | .0019       | -134.0 |
| 1.0000 | .2296     | .0108       | 85.9   | .0022       | -87.3  | .0018       | -134.7 | .0008       | 129.4  |
| 1.0500 | .2082     | .0058       | 77.4   | .0027       | -111.3 | .0007       | 132.6  | .0009       | 70.6   |
| 1.1000 | .1897     | .0016       | 55.0   | .0015       | -137.4 | .0009       | 71.2   | .0003       | 9.7    |
| 1.1500 | .1736     | .0013       | -86.2  | .0006       | 133.6  | .0004       | 23.2   | .0003       | -105.8 |
| 1.2000 | .1594     | .0021       | -108.4 | .0008       | 69.3   | .0003       | -95.4  | .0002       | -162.9 |
| 1.2500 | .1469     | .0016       | -124.1 | .0005       | 32.4   | .0002       | -147.4 | .0001       | 80.2   |
| 1.3000 | .1359     | .0007       | -154.9 | .0002       | -67.3  | .0001       | 108.1  | .0001       | 8.1    |
| 1.3500 | .1260     | .0004       | 96.6   | .0003       | -132.8 | .0001       | 27.5   | .0001       | -122.8 |
| 1.4000 | .1171     | .0006       | 55.0   | .0001       | 168.8  | .0000       | -78.0  | .0001       | 116.7  |
| 1.4500 | .1092     | .0004       | 25.3   | .0001       | 57.3   | .0001       | 178.2  | .0000       | -42.8  |
| 1.5000 | .1020     | .0002       | -41.8  | .0001       | -10.7  | .0000       | 31.7   | .0000       | -175.5 |
| 1.5500 | .0956     | .0002       | -123.8 | .0001       | -118.4 | .0000       | -62.2  | .0000       | 102.0  |
| 1.6000 | .0897     | .0002       | -169.2 | .0001       | 156.0  | .0000       | 162.0  | .0001       | -23.5  |
| 1.6500 | .0843     | .0001       | 122.0  | .0000       | 52.0   | .0000       | 66.0   | .0000       | -144.8 |
| 1.7000 | .0794     | .0001       | 39.6   | .0000       | -44.6  | .0000       | -46.8  | .0000       | 67.3   |
| 1.7500 | .0750     | .0001       | -19.4  | .0000       | -146.0 | .0001       | -138.1 | .0000       | -29.5  |
| 1.8000 | .0709     | .0001       | -90.0  | .0000       | 124.2  | .0000       | 80.0   | .0000       | -176.0 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE PITCH DISPLACEMENT (DEGREE/ FEET )

## W A V E   A N G L E

| WAVE FREQ. | WAVE/SHIP LENGTH | AMPL. | PHASE  |
|------------|------------------|-------|--------|
| .2000      | 5.7398           | .0725 | 88.3   |
| .2500      | 3.6735           | .1158 | 85.9   |
| .3000      | 2.5510           | .1700 | 81.8   |
| .3500      | 1.8742           | .2340 | 75.3   |
| .4000      | 1.4349           | .3034 | 64.6   |
| .4500      | 1.1338           | .3644 | 46.0   |
| .5000      | .9184            | .3550 | 10.3   |
| .5500      | .7590            | .1603 | -34.7  |
| .6000      | .6378            | .0279 | -63.3  |
| .6500      | .5434            | .0197 | 118.4  |
| .7000      | .4686            | .0258 | 102.3  |
| .7500      | .4082            | .0159 | 88.7   |
| .8000      | .3587            | .0047 | 63.0   |
| .8500      | .3178            | .0026 | -75.2  |
| .9000      | .2834            | .0032 | -109.5 |
| .9500      | .2544            | .0013 | -152.9 |
| 1.0000     | .2296            | .0010 | 102.7  |
| 1.0500     | .2082            | .0008 | 57.7   |
| 1.1000     | .1897            | .0003 | -47.3  |
| 1.1500     | .1736            | .0003 | -123.7 |
| 1.2000     | .1594            | .0001 | 151.0  |
| 1.2500     | .1469            | .0001 | 53.4   |
| 1.3000     | .1359            | .0001 | -42.2  |
| 1.3500     | .1260            | .0001 | -149.7 |
| 1.4000     | .1171            | .0000 | -125.9 |
| 1.4500     | .1092            | .0000 | -91.0  |
| 1.5000     | .1020            | .0000 | 135.9  |
| 1.5500     | .0956            | .0000 | .3     |
| 1.6000     | .0897            | .0000 | -82.6  |
| 1.6500     | .0843            | .0002 | -115.0 |
| 1.7000     | .0794            | .0000 | -3.0   |
| 1.7500     | .0750            | .0000 | -122.4 |
| 1.8000     | .0709            | .0000 | 123.2  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM PITCH DISPLACEMENT (DEGREE)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 6.0073E-02          | .47875           | 771.5    |
| 4.879                | 1.4125E-01          | .47610           | 754.7    |
| 7.334                | 2.5666E-01          | .47790           | 724.1    |
| 10.497               | 3.6746E-01          | .47791           | 724.1    |
| 13.867               | 5.3024E-01          | .48246           | 703.8    |
| 17.894               | 6.6366E-01          | .48047           | 711.5    |
| 23.554               | 9.4500E-01          | .48700           | 688.8    |
| 28.835               | 1.2037E+00          | .49329           | 671.5    |
| 37.139               | 1.6009E+00          | .50805           | 637.6    |
| 47.602               | 2.0514E+00          | .51126           | 631.0    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN<br>24.0 HRS | HIGHEST OCCURANCE IN<br>48.0 HRS | HIGHEST OCCURANCE IN<br>72.0 HRS |
|----------------------|--------------------|------------|----------------------------------|----------------------------------|----------------------------------|
| 2.380                | .9410              | 2.7581E-01 | 2.9449E-01                       | 3.0602E-01                       | 3.1232E-01                       |
| 4.879                | .9416              | 6.5490E-01 | 6.9862E-01                       | 7.2551E-01                       | 7.4033E-01                       |
| 7.334                | .9412              | 1.2371E+00 | 1.3205E+00                       | 1.3711E+00                       | 1.3996E+00                       |
| 10.497               | .9412              | 1.7712E+00 | 1.8907E+00                       | 1.9632E+00                       | 2.0039E+00                       |
| 13.867               | .9400              | 2.6258E+00 | 2.8079E+00                       | 2.9199E+00                       | 2.9808E+00                       |
| 17.894               | .9405              | 3.2547E+00 | 3.4776E+00                       | 3.6139E+00                       | 3.6893E+00                       |
| 23.554               | .9388              | 4.7571E+00 | 5.0940E+00                       | 5.2991E+00                       | 5.4139E+00                       |
| 28.835               | .9372              | 6.1474E+00 | 6.5913E+00                       | 6.8583E+00                       | 7.0128E+00                       |
| 37.139               | .9332              | 8.2881E+00 | 8.9033E+00                       | 9.2675E+00                       | 9.4806E+00                       |
| 47.602               | .9324              | 1.0627E+01 | 1.1419E+01                       | 1.1887E+01                       | 1.2161E+01                       |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM PITCH DISPLACEMENT (DEGREE)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 1.0247E+00        | 3.7104E-02                   | 1.43                   | 3.7104E+06        | 9.6290E+07 |
| 2.0493E+00        | 4.6471E-03                   | 2.33                   | 4.6471E+05        | 3.2457E+06 |
| 3.0740E+00        | 8.1953E-04                   | 3.09                   | 8.1953E+04        | 3.8276E+05 |
| 4.0986E+00        | 1.3134E-04                   | 3.88                   | 1.3134E+04        | 6.8819E+04 |
| 5.1233E+00        | 1.9089E-05                   | 4.72                   | 1.9089E+03        | 1.1225E+04 |
| 6.1479E+00        | 2.8967E-06                   | 5.54                   | 2.8967E+02        | 1.6192E+03 |
| 7.1726E+00        | 5.6805E-07                   | 6.25                   | 5.6805E+01        | 2.3286E+02 |
| 8.1973E+00        | 1.4460E-07                   | 6.84                   | 1.4460E+01        | 4.2346E+01 |
| 9.2219E+00        | 3.9329E-08                   | 7.41                   | 3.9329E+00        | 1.0527E+01 |
| 1.0247E+01        | 1.0220E-08                   | 7.99                   | 1.0220E+00        | 2.9109E+00 |
| 1.1271E+01        | 2.4424E-09                   | 8.61                   | 2.4424E-01        | 7.7778E-01 |
| 1.2296E+01        | 5.2762E-10                   | 9.28                   | 5.2762E-02        | 1.9147E-01 |
| 1.3321E+01        | 1.0202E-10                   | 9.99                   | 1.0202E-02        | 4.2559E-02 |
| 1.4345E+01        | 1.7561E-11                   | 10.76                  | 1.7561E-03        | 8.4462E-03 |
| 1.5370E+01        | 2.6832E-12                   | 11.57                  | 2.6832E-04        | 1.4878E-03 |
| 1.6395E+01        | 3.6337E-13                   | 12.44                  | 3.6337E-05        | 2.3198E-04 |
| 1.7419E+01        | 4.3583E-14                   | 13.36                  | 4.3583E-06        | 3.1978E-05 |
| 1.8444E+01        | 4.6277E-15                   | 14.33                  | 4.6277E-07        | 3.8955E-06 |
| 1.9468E+01        | 4.3484E-16                   | 15.36                  | 4.3484E-08        | 4.1928E-07 |
| 2.0493E+01        | 3.6150E-17                   | 16.44                  | 3.6150E-09        | 3.9869E-08 |
| 2.1518E+01        | 2.6582E-18                   | 17.58                  | 2.6582E-10        | 3.3491E-09 |
| 2.2542E+01        | 1.7286E-19                   | 18.76                  | 1.7286E-11        | 2.4853E-10 |
| 2.3567E+01        | 9.9394E-21                   | 20.00                  | 9.9394E-13        | 1.6292E-11 |
| 2.4592E+01        | 5.0525E-22                   | 21.30                  | 5.0525E-14        | 9.4341E-13 |
| 2.5616E+01        | 2.2703E-23                   | 22.64                  | 2.2703E-15        | 4.8255E-14 |
| 2.6641E+01        | 9.0171E-25                   | 24.04                  | 9.0171E-17        | 2.1802E-15 |
| 2.7666E+01        | 3.1653E-26                   | 25.50                  | 3.1653E-18        | 8.7006E-17 |
| 2.8690E+01        | 9.8198E-28                   | 27.01                  | 9.8198E-20        | 3.0671E-18 |
| 2.9715E+01        | 2.6923E-29                   | 28.57                  | 2.6923E-21        | 9.5505E-20 |
| 3.0740E+01        | 6.5238E-31                   | 30.19                  | 6.5238E-23        | 2.6271E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 4.2435E+00 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 5 CYCLES = 5.4746E+00 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 6 CYCLES = 6.8169E+00 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 7 CYCLES = 8.4875E+00 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 8 CYCLES = 1.0262E+01 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 9 CYCLES = 1.1868E+01 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\*10 CYCLES = 1.3332E+01 (AMPLITUDE)

VL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SURGE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E    A N G L E |            |            |            |        |        |        |        |
|---------------|---------------------|----------------------|------------|------------|------------|--------|--------|--------|--------|
|               |                     | 0.00 DEG.            | 15.00 DEG. | 30.00 DEG. | 45.00 DEG. | AMPL.  | PHASE  | AMPL.  | PHASE  |
| .2000         | 5.7398              | 1.6826               | -89.0      | 1.5892     | -89.0      | 1.3359 | -89.0  | .9881  | -89.0  |
| .2500         | 3.6735              | 1.9159               | -88.9      | 1.7980     | -88.9      | 1.4844 | -88.9  | 1.0694 | -88.9  |
| .3000         | 2.5510              | 2.1460               | -88.6      | 2.0015     | -88.6      | 1.6248 | -88.7  | 1.1428 | -88.8  |
| .3500         | 1.8742              | 2.3383               | -88.1      | 2.1689     | -88.2      | 1.7359 | -88.4  | 1.1980 | -88.6  |
| .4000         | 1.4349              | 2.4407               | -87.0      | 2.2551     | -87.2      | 1.7885 | -87.6  | 1.2219 | -88.2  |
| .4500         | 1.1338              | 2.3854               | -84.8      | 2.2017     | -85.2      | 1.7467 | -86.3  | 1.1991 | -87.5  |
| .5000         | .9184               | 2.0969               | -80.2      | 1.9464     | -81.2      | 1.5743 | -83.7  | 1.1144 | -86.1  |
| .5500         | .7590               | 1.9977               | -80.0      | 1.8613     | -81.1      | 1.2460 | -78.3  | .9575  | -83.8  |
| .6000         | .6378               | 1.8639               | -79.9      | 1.7434     | -80.8      | .7725  | -64.4  | .7280  | -79.3  |
| .6500         | .5434               | 1.6957               | -79.6      | 1.5930     | -80.4      | .3693  | -1.9   | .4447  | -68.8  |
| .7000         | .4686               | 1.4931               | -79.2      | 1.4100     | -79.9      | .3463  | -.2    | .1829  | -26.5  |
| .7500         | .4082               | 1.2560               | -78.6      | 1.1946     | -79.0      | .3188  | 2.1    | .2620  | 62.2   |
| .8000         | .3587               | .9848                | -77.6      | .9472      | -77.5      | .2873  | 5.5    | .4563  | 88.0   |
| .8500         | .3178               | .6798                | -75.4      | .6686      | -74.4      | .2527  | 10.4   | .5378  | 107.7  |
| .9000         | .2834               | .3438                | -68.5      | .3637      | -65.4      | .2165  | 17.7   | .4955  | 108.4  |
| .9500         | .2544               | .0926                | 34.4       | .1207      | 7.2        | .1820  | 29.1   | .4471  | 109.5  |
| 1.0000        | .2296               | .0607                | 92.4       | .0852      | 74.7       | .1560  | 46.7   | .3927  | 111.0  |
| 1.0500        | .2082               | .0257                | 167.7      | .0378      | 133.5      | .1495  | 70.4   | .3324  | 113.2  |
| 1.1000        | .1897               | .0219                | -111.7     | .0248      | -133.3     | .0639  | 121.3  | .2668  | 116.8  |
| 1.1500        | .1736               | .0094                | -44.8      | .0158      | -78.8      | .0326  | -146.5 | .1971  | 123.6  |
| 1.2000        | .1594               | .0099                | 54.5       | .0092      | 29.9       | .0253  | -91.2  | .1281  | 138.9  |
| 1.2500        | .1469               | .0038                | 109.1      | .0077      | 79.7       | .0098  | -3.9   | .0831  | -178.6 |
| 1.3000        | .1359               | .0044                | -127.9     | .0036      | -154.1     | .0114  | 69.2   | .0643  | -106.8 |
| 1.3500        | .1260               | .0015                | -31.1      | .0032      | -101.0     | .0038  | 144.7  | .0298  | -61.4  |
| 1.4000        | .1171               | .0027                | 51.1       | .0028      | 30.9       | .0054  | -120.2 | .0167  | 39.5   |
| 1.4500        | .1092               | .0016                | -178.1     | .0014      | 92.0       | .0021  | -34.7  | .0143  | 89.6   |
| 1.5000        | .1020               | .0013                | -119.3     | .0021      | -150.7     | .0031  | 49.1   | .0061  | 177.5  |
| 1.5500        | .0956               | .0015                | 8.4        | .0010      | -37.7      | .0014  | 158.4  | .0072  | -112.3 |
| 1.6000        | .0897               | .0008                | 121.1      | .0012      | 36.7       | .0017  | -133.9 | .0032  | -41.7  |
| 1.6500        | .0843               | .0009                | -151.4     | .0011      | 164.4      | .0013  | -12.8  | .0035  | 45.5   |
| 1.7000        | .0794               | .0009                | -26.5      | .0008      | -87.7      | .0009  | 61.0   | .0017  | 118.0  |
| 1.7500        | .0750               | .0009                | 109.7      | .0008      | 11.9       | .0011  | 171.4  | .0020  | -152.0 |
| 1.8000        | .0709               | .0008                | -144.8     | .0010      | 137.5      | .0008  | -80.5  | .0011  | -72.5  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SURGE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E                   |                           | A N G L E                 |                            | 105.00 DEG.<br>AMPL. PHASE |        |       |        |
|---------------|---------------------|---------------------------|---------------------------|---------------------------|----------------------------|----------------------------|--------|-------|--------|
|               |                     | 60.00 DEG.<br>AMPL. PHASE | 75.00 DEG.<br>AMPL. PHASE | 90.00 DEG.<br>AMPL. PHASE | 105.00 DEG.<br>AMPL. PHASE |                            |        |       |        |
| .2000         | 5.7398              | .6178                     | -89.0                     | .2791                     | -89.0                      | .0000                      | -8.4   | .2126 | 91.0   |
| .2500         | 3.6735              | .6481                     | -89.0                     | .2831                     | -89.0                      | .0000                      | -16.0  | .2013 | 91.0   |
| .3000         | 2.5510              | .6735                     | -88.9                     | .2853                     | -89.0                      | .0000                      | -23.8  | .1894 | 91.0   |
| .3500         | 1.8742              | .6910                     | -88.8                     | .2855                     | -88.9                      | .0001                      | -31.8  | .1768 | 91.0   |
| .4000         | 1.4349              | .6969                     | -88.6                     | .2831                     | -88.9                      | .0001                      | -40.1  | .1634 | 90.9   |
| .4500         | 1.1338              | .6872                     | -88.3                     | .2778                     | -88.8                      | .0001                      | -49.0  | .1494 | 90.9   |
| .5000         | .9184               | .6578                     | -87.8                     | .2692                     | -88.6                      | .0001                      | -58.5  | .1348 | 91.0   |
| .5500         | .7590               | .6057                     | -87.1                     | .2570                     | -88.5                      | .0002                      | -69.2  | .1197 | 91.1   |
| .6000         | .6378               | .5294                     | -85.9                     | .2411                     | -88.3                      | .0002                      | -81.6  | .1046 | 91.4   |
| .6500         | .5434               | .4305                     | -83.9                     | .2212                     | -87.9                      | .0003                      | -96.0  | .0901 | 91.9   |
| .7000         | .4686               | .3141                     | -80.4                     | .1978                     | -87.6                      | .0004                      | -114.8 | .0767 | 91.7   |
| .7500         | .4082               | .1902                     | -73.2                     | .1712                     | -87.0                      | .0005                      | -138.5 | .0627 | 90.4   |
| .8000         | .3587               | .0774                     | -48.7                     | .1422                     | -86.4                      | .0005                      | -169.1 | .0485 | 89.0   |
| .8500         | .3178               | .0608                     | 50.4                      | .1119                     | -85.4                      | .0005                      | 154.8  | .0354 | 87.8   |
| .9000         | .2834               | .1191                     | 81.5                      | .0814                     | -84.2                      | .0004                      | 120.3  | .0239 | 86.4   |
| .9500         | .2544               | .1437                     | 93.8                      | .0523                     | -82.1                      | .0003                      | 94.3   | .0143 | 84.3   |
| 1.0000        | .2296               | .1253                     | 106.5                     | .0262                     | -77.8                      | .0002                      | 76.6   | .0067 | 80.3   |
| 1.0500        | .2082               | .0752                     | 132.1                     | .0051                     | -47.2                      | .0002                      | 64.7   | .0013 | 54.9   |
| 1.1000        | .1897               | .0528                     | -146.0                    | .0127                     | 84.7                       | .0001                      | 56.4   | .0026 | -84.0  |
| 1.1500        | .1736               | .1062                     | -95.9                     | .0229                     | 92.7                       | .0001                      | 51.7   | .0044 | -91.8  |
| 1.2000        | .1594               | .1445                     | -73.0                     | .0270                     | 96.3                       | .0001                      | 48.6   | .0049 | -95.3  |
| 1.2500        | .1469               | .1370                     | -45.9                     | .0255                     | 99.2                       | .0000                      | 45.9   | .0043 | -98.3  |
| 1.3000        | .1359               | .1166                     | 12.3                      | .0196                     | 102.4                      | .0000                      | 45.4   | .0030 | -101.6 |
| 1.3500        | .1260               | .1065                     | 16.0                      | .0110                     | 106.9                      | .0000                      | 46.5   | .0016 | -106.3 |
| 1.4000        | .1171               | .0962                     | 21.0                      | .0018                     | 132.3                      | .0000                      | 48.5   | .0003 | -130.9 |
| 1.4500        | .1092               | .0861                     | 27.7                      | .0066                     | -78.3                      | .0000                      | 53.3   | .0008 | 80.1   |
| 1.5000        | .1020               | .0768                     | 36.7                      | .0120                     | -71.2                      | .0000                      | 61.8   | .0013 | 72.3   |
| 1.5500        | .0956               | .0696                     | 48.6                      | .0138                     | -65.9                      | .0000                      | 75.3   | .0014 | 66.6   |
| 1.6000        | .0897               | .0658                     | 63.5                      | .0122                     | -59.6                      | .0000                      | 96.1   | .0011 | 59.9   |
| 1.6500        | .0843               | .0671                     | 80.0                      | .0079                     | -49.5                      | .0000                      | 122.1  | .0006 | 49.2   |
| 1.7000        | .0794               | .0740                     | 95.5                      | .0028                     | -14.6                      | .0000                      | 145.2  | .0002 | 13.1   |
| 1.7500        | .0750               | .0311                     | 143.3                     | .0037                     | 95.6                       | .0000                      | 160.7  | .0003 | -93.7  |
| 1.8000        | .0709               | .0171                     | -136.0                    | .0068                     | 118.3                      | .0000                      | 171.9  | .0004 | -117.6 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SURGE DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E     |             | A N G L E   |             | WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E     |             | A N G L E   |             |
|---------------|---------------------|-------------|-------------|-------------|-------------|---------------|---------------------|-------------|-------------|-------------|-------------|
|               |                     | 120.00 DEG. | AMPL. PHASE | 135.00 DEG. | AMPL. PHASE |               |                     | 150.00 DEG. | AMPL. PHASE | 165.00 DEG. | AMPL. PHASE |
| .2000         | 5.7398              | .3643       | 91.0        | .4661       | 91.0        | .5293         | 91.0                | .5633       | 91.0        |             |             |
| .2500         | 3.6735              | .3340       | 91.0        | .4152       | 91.0        | .4608         | 90.9                | .4832       | 90.9        |             |             |
| .3000         | 2.5510              | .3028       | 90.9        | .3634       | 90.9        | .3915         | 90.8                | .4024       | 90.7        |             |             |
| .3500         | 1.8742              | .2705       | 90.9        | .3101       | 90.7        | .3208         | 90.5                | .3205       | 90.3        |             |             |
| .4000         | 1.4349              | .2368       | 90.8        | .2554       | 90.4        | .2496         | 90.0                | .2394       | 89.6        |             |             |
| .4500         | 1.1338              | .2020       | 90.6        | .2006       | 90.0        | .1807         | 89.1                | .1631       | 88.3        |             |             |
| .5000         | .9184               | .1668       | 90.5        | .1481       | 89.4        | .1188         | 87.5                | .0981       | 85.4        |             |             |
| .5500         | .7590               | .1326       | 90.5        | .1014       | 88.0        | .0680         | 82.4                | .0473       | 75.7        |             |             |
| .6000         | .6378               | .1012       | 90.0        | .0609       | 82.9        | .0285         | 67.7                | .0143       | 41.1        |             |             |
| .6500         | .5434               | .0718       | 87.4        | .0281       | 71.7        | .0084         | 4.3                 | .0104       | -54.8       |             |             |
| .7000         | .4686               | .0446       | 83.1        | .0083       | 29.3        | .0109         | -70.4               | .0118       | -89.4       |             |             |
| .7500         | .4082               | .0227       | 75.7        | .0086       | -61.3       | .0105         | -95.9               | .0081       | -119.3      |             |             |
| .8000         | .3587               | .0077       | 51.4        | .0102       | -86.9       | .0067         | -125.5              | .0048       | -166.5      |             |             |
| .8500         | .3178               | .0049       | -49.5       | .0077       | -106.2      | .0038         | -176.3              | .0032       | 140.4       |             |             |
| .9000         | .2834               | .0081       | -80.6       | .0042       | -139.3      | .0028         | 129.2               | .0017       | 85.8        |             |             |
| .9500         | .2544               | .0079       | -92.8       | .0026       | 157.6       | .0017         | 78.5                | .0010       | -7.1        |             |             |
| 1.0000        | .2296               | .0055       | -105.3      | .0024       | 106.9       | .0010         | -4.2                | .0012       | -75.4       |             |             |
| 1.0500        | .2082               | .0026       | -130.4      | .0017       | 66.5        | .0012         | -71.1               | .0008       | -134.0      |             |             |
| 1.1000        | .1897               | .0014       | 147.9       | .0010       | -.5         | .0008         | -122.0              | .0007       | 132.9       |             |             |
| 1.1500        | .1736               | .0021       | 96.9        | .0011       | -66.5       | .0006         | 146.1               | .0006       | 77.9        |             |             |
| 1.2000        | .1594               | .0021       | 73.9        | .0008       | -108.3      | .0006         | 90.4                | .0004       | -30.2       |             |             |
| 1.2500        | .1469               | .0014       | 47.0        | .0005       | 178.0       | .0003         | 3.5                 | .0004       | -80.7       |             |             |
| 1.3000        | .1359               | .0007       | -10.9       | .0006       | 106.0       | .0004         | -69.8               | .0002       | 153.5       |             |             |
| 1.3500        | .1260               | .0008       | -74.6       | .0004       | 60.5        | .0002         | -145.5              | .0002       | 100.0       |             |             |
| 1.4000        | .1171               | .0008       | -108.3      | .0003       | -40.0       | .0003         | 119.6               | .0002       | -31.7       |             |             |
| 1.4500        | .1092               | .0004       | -149.3      | .0003       | -90.5       | .0001         | 33.7                | .0001       | -92.7       |             |             |
| 1.5000        | .1020               | .0003       | 128.7       | .0002       | -178.2      | .0002         | -49.7               | .0002       | 150.2       |             |             |
| 1.5500        | .0956               | .0004       | 80.9        | .0002       | 111.7       | .0001         | -158.8              | .0001       | 37.4        |             |             |
| 1.6000        | .0897               | .0003       | 40.8        | .0001       | 41.0        | .0001         | 133.5               | .0001       | -36.9       |             |             |
| 1.6500        | .0843               | .0002       | -41.2       | .0002       | -45.9       | .0001         | 12.5                | .0001       | -164.5      |             |             |
| 1.7000        | .0794               | .0002       | -96.6       | .0001       | -118.3      | .0001         | -61.2               | .0001       | 87.8        |             |             |
| 1.7500        | .0750               | .0001       | -144.7      | .0001       | 151.7       | .0001         | -171.7              | .0001       | -11.8       |             |             |
| 1.8000        | .0709               | .0001       | 134.9       | .0001       | 72.4        | .0001         | 80.6                | .0002       | -137.3      |             |             |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SURGE DISPLACEMENT ( FEET / FEET )

## W A V E   A N G L E

| WAVE FREQ. | WAVE/SHIP LENGTH | AMPL. | PHASE  |
|------------|------------------|-------|--------|
| .2000      | 5.7398           | .5740 | 91.0   |
| .2500      | 3.6735           | .4898 | 90.9   |
| .3000      | 2.5510           | .4050 | 90.7   |
| .3500      | 1.8742           | .3194 | 90.3   |
| .4000      | 1.4349           | .2350 | 89.4   |
| .4500      | 1.1338           | .1566 | 87.9   |
| .5000      | .9184            | .0909 | 84.5   |
| .5500      | .7590            | .0408 | 72.5   |
| .6000      | .6378            | .0114 | 24.4   |
| .6500      | .5434            | .0114 | -64.7  |
| .7000      | .4686            | .0114 | -95.6  |
| .7500      | .4082            | .0073 | -129.6 |
| .8000      | .3587            | .0044 | 179.6  |
| .8500      | .3178            | .0028 | 128.4  |
| .9000      | .2834            | .0013 | 63.6   |
| .9500      | .2544            | .0011 | -34.6  |
| 1.0000     | .2296            | .0011 | -93.2  |
| 1.0500     | .2082            | .0007 | -167.9 |
| 1.1000     | .1897            | .0007 | 111.1  |
| 1.1500     | .1736            | .0004 | 44.1   |
| 1.2000     | .1594            | .0005 | -55.1  |
| 1.2500     | .1469            | .0002 | -110.7 |
| 1.3000     | .1359            | .0003 | 127.0  |
| 1.3500     | .1260            | .0001 | 29.9   |
| 1.4000     | .1171            | .0002 | -51.6  |
| 1.4500     | .1092            | .0002 | 177.7  |
| 1.5000     | .1020            | .0001 | 118.9  |
| 1.5500     | .0956            | .0002 | -8.7   |
| 1.6000     | .0897            | .0001 | -121.3 |
| 1.6500     | .0843            | .0001 | 150.4  |
| 1.7000     | .0794            | .0001 | 26.6   |
| 1.7500     | .0750            | .0001 | -109.6 |
| 1.8000     | .0709            | .0001 | 145.0  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM SURGE DISPLACEMENT ( FEET )

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 2.0704E-01          | .69049           | 451.9    |
| 4.879                | 4.8117E-01          | .65936           | 448.0    |
| 7.334                | 8.7877E-01          | .60779           | 439.1    |
| 10.497               | 1.2582E+00          | .60770           | 439.1    |
| 13.867               | 1.8529E+00          | .57773           | 431.7    |
| 17.894               | 2.2978E+00          | .58877           | 434.6    |
| 23.554               | 3.3771E+00          | .55792           | 425.5    |
| 28.835               | 4.4452E+00          | .53711           | 417.4    |
| 37.139               | 6.4174E+00          | .50326           | 399.3    |
| 47.602               | 8.3765E+00          | .49768           | 395.4    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN<br>24.0 HRS | 48.0 HRS   | 72.0 HRS   |
|----------------------|--------------------|------------|----------------------------------|------------|------------|
| 2.380                | .8727              | 1.4882E+00 | 1.6113E+00                       | 1.6864E+00 | 1.7272E+00 |
| 4.879                | .8847              | 3.5148E+00 | 3.8053E+00                       | 3.9825E+00 | 4.0788E+00 |
| 7.334                | .9029              | 6.5452E+00 | 7.0856E+00                       | 7.4150E+00 | 7.5942E+00 |
| 10.497               | .9030              | 9.3713E+00 | 1.0145E+01                       | 1.0617E+01 | 1.0873E+01 |
| 13.867               | .9128              | 1.3903E+01 | 1.5051E+01                       | 1.5750E+01 | 1.6131E+01 |
| 17.894               | .9092              | 1.7201E+01 | 1.8621E+01                       | 1.9486E+01 | 1.9957E+01 |
| 23.554               | .9189              | 2.5415E+01 | 2.7515E+01                       | 2.8795E+01 | 2.9491E+01 |
| 28.835               | .9251              | 3.3493E+01 | 3.6264E+01                       | 3.7953E+01 | 3.8872E+01 |
| 37.139               | .9345              | 4.8137E+01 | 5.2138E+01                       | 5.4579E+01 | 5.5902E+01 |
| 47.602               | .9360              | 6.2712E+01 | 6.7931E+01                       | 7.1115E+01 | 7.2839E+01 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM SURGE DISPLACEMENT ( FEET )

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 6.4517E+00        | 1.4970E-02                   | 1.82                   | 1.4970E+06        | 9.8503E+07 |
| 1.2903E+01        | 1.8717E-03                   | 2.73                   | 1.8717E+05        | 1.3098E+06 |
| 1.9355E+01        | 3.0128E-04                   | 3.52                   | 3.0128E+04        | 1.5705E+05 |
| 2.5807E+01        | 4.3624E-05                   | 4.36                   | 4.3624E+03        | 2.5765E+04 |
| 3.2258E+01        | 6.3506E-06                   | 5.20                   | 6.3506E+02        | 3.7274E+03 |
| 3.8710E+01        | 1.1855E-06                   | 5.93                   | 1.1855E+02        | 5.1651E+02 |
| 4.5162E+01        | 3.0723E-07                   | 6.51                   | 3.0723E+01        | 8.7832E+01 |
| 5.1613E+01        | 8.9281E-08                   | 7.05                   | 8.9281E+00        | 2.1795E+01 |
| 5.8065E+01        | 2.5279E-08                   | 7.60                   | 2.5279E+00        | 6.4002E+00 |
| 6.4517E+01        | 6.6721E-09                   | 8.18                   | 6.6721E-01        | 1.8607E+00 |
| 7.0968E+01        | 1.6079E-09                   | 8.79                   | 1.6079E-01        | 5.0642E-01 |
| 7.7420E+01        | 3.4895E-10                   | 9.46                   | 3.4895E-02        | 1.2589E-01 |
| 8.3872E+01        | 6.7634E-11                   | 10.17                  | 6.7634E-03        | 2.8132E-02 |
| 9.0323E+01        | 1.1655E-11                   | 10.93                  | 1.1655E-03        | 5.5978E-03 |
| 9.6775E+01        | 1.7819E-12                   | 11.75                  | 1.7819E-04        | 9.8734E-04 |
| 1.0323E+02        | 2.4138E-13                   | 12.62                  | 2.4138E-05        | 1.5405E-04 |
| 1.0968E+02        | 2.8957E-14                   | 13.54                  | 2.8957E-06        | 2.1243E-05 |
| 1.1613E+02        | 3.0754E-15                   | 14.51                  | 3.0754E-07        | 2.5882E-06 |
| 1.2258E+02        | 2.8911E-16                   | 15.54                  | 2.8911E-08        | 2.7863E-07 |
| 1.2903E+02        | 2.4060E-17                   | 16.62                  | 2.4060E-09        | 2.6505E-08 |
| 1.3548E+02        | 1.7726E-18                   | 17.75                  | 1.7726E-10        | 2.2287E-09 |
| 1.4194E+02        | 1.1564E-19                   | 18.94                  | 1.1564E-11        | 1.6570E-10 |
| 1.4839E+02        | 6.6814E-21                   | 20.18                  | 6.6814E-13        | 1.0896E-11 |
| 1.5484E+02        | 3.4190E-22                   | 21.47                  | 3.4190E-14        | 6.3395E-13 |
| 1.6129E+02        | 1.5497E-23                   | 22.81                  | 1.5497E-15        | 3.2641E-14 |
| 1.6774E+02        | 6.2211E-25                   | 24.21                  | 6.2211E-17        | 1.4875E-15 |
| 1.7419E+02        | 2.2117E-26                   | 25.66                  | 2.2117E-18        | 6.0000E-17 |
| 1.8065E+02        | 6.9624E-28                   | 27.16                  | 6.9624E-20        | 2.1421E-18 |
| 1.8710E+02        | 1.9401E-29                   | 28.71                  | 1.9401E-21        | 6.7684E-20 |
| 1.9355E+02        | 4.7846E-31                   | 30.32                  | 4.7846E-23        | 1.8923E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 2.3037E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 3.0738E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 3.9523E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 5.1021E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 6.2557E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 7.2974E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 8.2334E+01 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SWAY DISPLACEMENT ( FEET / FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | 15.00 DEG. |        | 30.00 DEG. |        | 45.00 DEG. |        | 60.00 DEG. |        |
|---------------|---------------------|------------|--------|------------|--------|------------|--------|------------|--------|
|               |                     | AMPL.      | PHASE  | AMPL.      | PHASE  | AMPL.      | PHASE  | AMPL.      | PHASE  |
| .2000         | 5.7398              | .3572      | 88.7   | .6612      | 89.0   | .8765      | 89.3   | .9916      | 89.8   |
| .2500         | 3.6735              | .3632      | 89.4   | .6694      | 89.6   | .8816      | 89.9   | .9889      | 90.5   |
| .3000         | 2.5510              | .3516      | 90.9   | .6496      | 91.0   | .8566      | 91.5   | .9909      | 93.2   |
| .3500         | 1.8742              | .3153      | 94.6   | .5905      | 94.3   | .8187      | 96.5   | .9961      | 92.8   |
| .4000         | 1.4349              | .2516      | 103.6  | .4914      | 102.1  | .8042      | 100.6  | .9465      | 93.5   |
| .4500         | 1.1338              | .1767      | 127.8  | .3707      | 119.0  | .7199      | 104.2  | .8718      | 95.1   |
| .5000         | .9184               | .1702      | 179.5  | .2874      | 154.3  | .5882      | 112.1  | .7697      | 97.8   |
| .5500         | .7590               | .1632      | 179.6  | .3409      | -163.3 | .4466      | 128.0  | .6427      | 102.0  |
| .6000         | .6378               | .1537      | 179.7  | .4795      | -139.3 | .3526      | 156.5  | .4976      | 108.8  |
| .6500         | .5434               | .1415      | 179.9  | .5680      | -124.1 | .3578      | -169.9 | .3487      | 121.2  |
| .7000         | .4686               | .1266      | -179.8 | .5350      | -123.8 | .4175      | -144.0 | .2241      | 146.0  |
| .7500         | .4082               | .1091      | -179.4 | .4950      | -123.3 | .3988      | -116.8 | .1740      | -169.7 |
| .8000         | .3587               | .0889      | -178.7 | .4480      | -122.7 | .2628      | -76.5  | .2018      | -131.3 |
| .8500         | .3178               | .0662      | -177.3 | .3941      | -121.8 | .3124      | 4.1    | .2312      | -108.8 |
| .9000         | .2834               | .0408      | -174.0 | .3334      | -120.5 | .2916      | 3.3    | .2232      | -91.0  |
| .9500         | .2544               | .0137      | -156.1 | .2660      | -118.3 | .2678      | 2.1    | .1761      | -69.3  |
| 1.0000        | .2296               | .0209      | -105.5 | .1924      | -114.1 | .2410      | .6     | .1195      | -29.6  |
| 1.0500        | .2082               | .0087      | -87.1  | .1147      | -103.4 | .2114      | -1.5   | .1213      | 31.5   |
| 1.1000        | .1897               | .0045      | 50.0   | .0400      | -87.1  | .1793      | -4.8   | .1684      | 71.3   |
| 1.1500        | .1736               | .0048      | 73.9   | .0104      | 25.1   | .1450      | -9.9   | .1872      | 99.5   |
| 1.2000        | .1594               | .0015      | 170.9  | .0145      | 72.0   | .1101      | -18.9  | .1677      | 136.0  |
| 1.2500        | .1469               | .0034      | -120.6 | .0053      | 117.8  | .0783      | -37.3  | .2280      | -158.5 |
| 1.3000        | .1359               | .0016      | -15.1  | .0064      | -134.4 | .0443      | 61.9   | .3983      | -111.8 |
| 1.3500        | .1260               | .0028      | 64.1   | .0055      | -82.2  | .0313      | 97.9   | .3693      | -111.8 |
| 1.4000        | .1171               | .0021      | -170.8 | .0058      | 31.2   | .0120      | 169.9  | .3377      | -111.9 |
| 1.4500        | .1092               | .0019      | -91.9  | .0046      | 102.9  | .0114      | -116.0 | .3036      | -112.0 |
| 1.5000        | .1020               | .0017      | 24.0   | .0054      | -148.2 | .0090      | -64.6  | .2668      | -112.1 |
| 1.5500        | .0956               | .0010      | 124.3  | .0037      | -56.0  | .0077      | 15.9   | .2275      | -112.3 |
| 1.6000        | .0897               | .0010      | -136.4 | .0036      | 41.4   | .0096      | 87.1   | .1856      | -112.6 |
| 1.6500        | .0843               | .0007      | -25.2  | .0024      | 146.6  | .0082      | 175.3  | .1412      | -113.1 |
| 1.7000        | .0794               | .0005      | 75.2   | .0020      | -121.0 | .0086      | -105.2 | .0942      | -114.1 |
| 1.7500        | .0750               | .0004      | -167.3 | .0015      | -12.7  | .0067      | -10.3  | .0516      | -39.2  |
| 1.8000        | .0709               | .0003      | -46.2  | .0010      | 84.6   | .0052      | 75.9   | .0332      | -15.8  |

SL-7 = NORMAL FULL LOAD DEPARTURE

SPEED = 25,000 KNOTS

REGULAR WAVE SWAY DISPLACEMENT ( FEET / FEET )

| WAVE   | WAVE/SHIP | 75.00  | DEG.   | 90.00 | DEG.  | 105.00 | DEG.   | 120.00 | DEG.   |
|--------|-----------|--------|--------|-------|-------|--------|--------|--------|--------|
| FREQ.  | LENGTH    | AMPL.  | PHASE  | AMPL. | PHASE | AMPL.  | PHASE  | AMPL.  | PHASE  |
| .2000  | 5.7398    | 1.0142 | 90.3   | .9617 | 90.8  | .8555  | 91.3   | .7159  | 91.9   |
| .2500  | 3.6735    | 1.0070 | 91.5   | .9667 | 91.3  | .8407  | 90.5   | .6813  | 90.4   |
| .3000  | 2.5510    | 1.0227 | 91.2   | .9384 | 90.6  | .8005  | 90.4   | .6355  | 90.2   |
| .3500  | 1.8742    | .9980  | 91.2   | .9110 | 90.7  | .7620  | 90.3   | .5856  | 89.6   |
| .4000  | 1.4349    | .9670  | 91.7   | .8817 | 90.9  | .7196  | 89.9   | .5276  | 88.4   |
| .4500  | 1.1338    | .9259  | 92.5   | .8493 | 91.1  | .6712  | 89.4   | .4597  | 86.4   |
| .5000  | .9184     | .8750  | 93.5   | .8129 | 91.4  | .6165  | 88.5   | .3818  | 83.6   |
| .5500  | .7590     | .8118  | 94.9   | .7730 | 91.6  | .5547  | 87.3   | .2968  | 79.8   |
| .6000  | .6378     | .7370  | 96.6   | .7289 | 91.9  | .4870  | 85.8   | .2106  | 75.0   |
| .6500  | .5434     | .6511  | 98.8   | .6825 | 92.1  | .4156  | 84.2   | .1310  | 67.9   |
| .7000  | .4686     | .5559  | 101.6  | .6327 | 92.2  | .3421  | 82.4   | .0662  | 53.9   |
| .7500  | .4082     | .4544  | 105.3  | .5826 | 92.2  | .2694  | 80.4   | .0269  | 10.3   |
| .8000  | .3587     | .3502  | 110.5  | .5313 | 92.2  | .2009  | 78.2   | .0277  | -59.1  |
| .8500  | .3178     | .2481  | 118.3  | .4798 | 92.2  | .1393  | 75.4   | .0347  | -82.5  |
| .9000  | .2834     | .1568  | 132.5  | .4284 | 92.2  | .0867  | 71.4   | .0331  | -93.5  |
| .9500  | .2544     | .0911  | 164.0  | .3779 | 92.2  | .0448  | 63.8   | .0249  | -102.9 |
| 1.0000 | .2296     | .0787  | -143.1 | .3283 | 92.1  | .0151  | 36.4   | .0148  | -115.7 |
| 1.0500 | .2082     | .1010  | -110.2 | .2809 | 91.9  | .0136  | -65.1  | .0062  | -144.6 |
| 1.1000 | .1897     | .1201  | -92.9  | .2360 | 91.7  | .0244  | -89.3  | .0036  | 132.4  |
| 1.1500 | .1736     | .1222  | -80.4  | .1942 | 91.5  | .0292  | -97.3  | .0051  | 85.9   |
| 1.2000 | .1594     | .1076  | -68.2  | .1560 | 91.2  | .0284  | -102.6 | .0049  | 61.1   |
| 1.2500 | .1469     | .0814  | -52.2  | .1216 | 90.8  | .0237  | -107.9 | .0034  | 34.6   |
| 1.3000 | .1359     | .0531  | -24.3  | .0915 | 90.3  | .0170  | -114.2 | .0019  | -12.8  |
| 1.3500 | .1260     | .0401  | 27.3   | .0657 | 89.5  | .0097  | -124.1 | .0016  | -76.5  |
| 1.4000 | .1171     | .0501  | 73.2   | .0445 | 88.5  | .0036  | -153.3 | .0016  | -120.4 |
| 1.4500 | .1092     | .0619  | 99.3   | .0274 | 86.7  | .0030  | 101.4  | .0011  | -161.8 |
| 1.5000 | .1020     | .0643  | 119.3  | .0143 | 82.9  | .0056  | 72.1   | .0007  | 138.3  |
| 1.5500 | .0956     | .0571  | 140.7  | .0050 | 69.1  | .0065  | 59.2   | .0009  | 69.2   |
| 1.6000 | .0897     | .0450  | 169.3  | .0024 | -46.4 | .0058  | 48.0   | .0005  | -16.4  |
| 1.6500 | .0843     | .0360  | -150.5 | .0057 | -75.3 | .0041  | 33.8   | .0004  | -41.0  |
| 1.7000 | .0794     | .0348  | -106.1 | .0074 | -80.6 | .0023  | 8.4    | .0004  | -104.7 |
| 1.7500 | .0750     | .0364  | -68.1  | .0075 | -82.9 | .0013  | -54.9  | .0003  | -168.4 |
| 1.8000 | .0709     | .0359  | -33.5  | .0067 | -84.3 | .0017  | -111.7 | .0003  | 142.3  |

AD-A104 951

HOFFMAN MARITIME CONSULTANTS INC GLEN HEAD NY

F/G 20/4

USER MANUAL FOR PROGRAM SCOMOT SECOND PART OF U.S.C.G. SHIP MOT--ETC(U)

FEB 81 T E ZIELINSKI

DOT-CG-958905-A

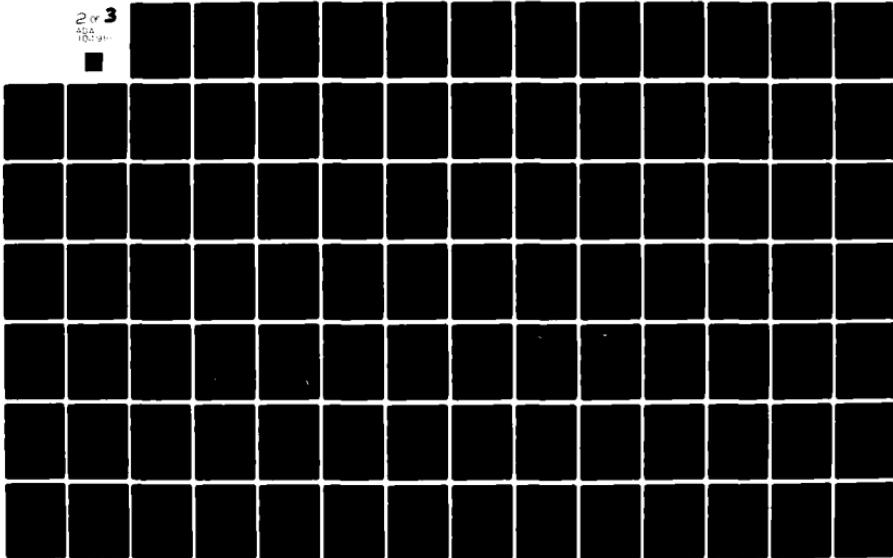
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USCG-M-11-80

NL

2 or 3  
ASA  
100-910-



SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE SWAY DISPLACEMENT ( FEET / FEET )

| WAVE   | WAVE/SHIP | 135.00 | DEG.   | 150.00 | DEG.   | 165.00 | DEG.   |
|--------|-----------|--------|--------|--------|--------|--------|--------|
| FREQ.  | LENGTH    | AMPL.  | PHASE  | AMPL.  | PHASE  | AMPL.  | PHASE  |
| .2000  | 5.7398    | .5556  | 91.9   | .3768  | 91.4   | .1891  | 91.0   |
| .2500  | 3.6735    | .5103  | 90.3   | .3373  | 90.2   | .1673  | 90.2   |
| .3000  | 2.5510    | .4643  | 89.8   | .2996  | 89.4   | .1461  | 89.1   |
| .3500  | 1.8742    | .4110  | 88.5   | .2553  | 87.4   | .1210  | 86.5   |
| .4000  | 1.4349    | .3482  | 86.1   | .2028  | 83.6   | .0915  | 81.5   |
| .4500  | 1.1338    | .2751  | 82.1   | .1439  | 77.1   | .0596  | 72.7   |
| .5000  | .9184     | .1957  | 76.1   | .0851  | 66.1   | .0304  | 55.3   |
| .5500  | .7590     | .1185  | 66.6   | .0384  | 40.8   | .0129  | 5.8    |
| .6000  | .6378     | .0560  | 46.4   | .0210  | -25.7  | .0124  | -56.6  |
| .6500  | .5434     | .0265  | -12.5  | .0240  | -69.5  | .0116  | -81.3  |
| .7000  | .4686     | .0309  | -65.5  | .0202  | -87.2  | .0070  | -98.3  |
| .7500  | .4082     | .0309  | -84.6  | .0114  | -104.2 | .0025  | -135.4 |
| .8000  | .3587     | .0224  | -97.5  | .0042  | -145.5 | .0017  | 138.7  |
| .8500  | .3178     | .0117  | -115.7 | .0031  | 134.0  | .0015  | 99.6   |
| .9000  | .2834     | .0046  | -165.0 | .0028  | 95.4   | .0007  | 49.6   |
| .9500  | .2544     | .0041  | 121.3  | .0015  | 49.0   | .0006  | -42.6  |
| 1.0000 | .2296     | .0038  | 85.1   | .0012  | -35.3  | .0006  | -88.9  |
| 1.0500 | .2082     | .0024  | 44.1   | .0012  | -85.2  | .0003  | -148.1 |
| 1.1000 | .1897     | .0016  | -21.0  | .0007  | -136.2 | .0003  | 126.3  |
| 1.1500 | .1736     | .0016  | -78.6  | .0005  | 139.5  | .0002  | 70.9   |
| 1.2000 | .1594     | .0011  | -121.7 | .0005  | 82.3   | .0001  | -22.9  |
| 1.2500 | .1469     | .0007  | 170.7  | .0003  | 1.8    | .0001  | -92.1  |
| 1.3000 | .1359     | .0006  | 100.7  | .0002  | -72.4  | .0076  | 138.8  |
| 1.3500 | .1260     | .0005  | 41.7   | .0001  | 176.1  | .0001  | 98.8   |
| 1.4000 | .1171     | .0004  | -37.0  | .0002  | 99.4   | .0001  | -51.9  |
| 1.4500 | .1092     | .0003  | -99.2  | .0002  | 10.8   | .0001  | -134.1 |
| 1.5000 | .1020     | .0002  | 156.7  | .0002  | -83.4  | .0001  | 133.9  |
| 1.5500 | .0956     | .0003  | 102.5  | .0002  | -168.5 | .0001  | 44.3   |
| 1.6000 | .0897     | .0002  | 11.9   | .0001  | 99.7   | .0001  | -51.4  |
| 1.6500 | .0843     | .0002  | -69.8  | .0001  | 27.0   | .0001  | -110.4 |
| 1.7000 | .0794     | .0002  | -148.2 | .0001  | -88.4  | .0001  | 102.8  |
| 1.7500 | .0750     | .0001  | 129.7  | .0000  | -103.0 | .0002  | -146.0 |
| 1.8000 | .0709     | .0001  | 48.4   | .0002  | 102.7  | .0009  | 173.9  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM SWAY DISPLACEMENT ( FEET )

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 1.5987E-01          | .58381           | 653.2    |
| 4.879                | 3.5923E-01          | .57464           | 632.9    |
| 7.334                | 6.2631E-01          | .55991           | 596.9    |
| 10.497               | 8.9666E-01          | .55988           | 596.9    |
| 13.867               | 1.2941E+00          | .55194           | 573.2    |
| 17.894               | 1.6157E+00          | .55478           | 582.3    |
| 23.554               | 2.3358E+00          | .54721           | 555.7    |
| 28.835               | 3.0563E+00          | .54296           | 535.3    |
| 37.139               | 4.4271E+00          | .53863           | 494.8    |
| 47.602               | 5.7945E+00          | .53841           | 486.8    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .9108              | 7.3387E-01 | 7.8583E-01           | 8.1735E-01 | 8.3527E-01 |
| 4.879                | .9137              | 1.6531E+00 | 1.7707E+00           | 1.8419E+00 | 1.8826E+00 |
| 7.334                | .9183              | 2.8850E+00 | 3.0920E+00           | 3.2168E+00 | 3.2888E+00 |
| 10.497               | .9183              | 4.1303E+00 | 4.4267E+00           | 4.6054E+00 | 4.7085E+00 |
| 13.867               | .9207              | 5.9471E+00 | 6.3761E+00           | 6.6341E+00 | 6.7839E+00 |
| 17.894               | .9198              | 7.4337E+00 | 7.9689E+00           | 8.2910E+00 | 8.4776E+00 |
| 23.554               | .9221              | 1.0701E+01 | 1.1476E+01           | 1.1941E+01 | 1.2212E+01 |
| 28.835               | .9234              | 1.3931E+01 | 1.4944E+01           | 1.5550E+01 | 1.5905E+01 |
| 37.139               | .9246              | 1.9914E+01 | 2.1375E+01           | 2.2246E+01 | 2.2755E+01 |
| 47.602               | .9247              | 2.5989E+01 | 2.7898E+01           | 2.9035E+01 | 2.9700E+01 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM SWAY DISPLACEMENT ( FEET )

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 2.4892E+00        | 3.5568E-02                   | 1.45                   | 3.5568E+06        | 9.6443E+07 |
| 4.9785E+00        | 4.3714E-03                   | 2.36                   | 4.3714E+05        | 3.1196E+06 |
| 7.4677E+00        | 6.8651E-04                   | 3.16                   | 6.8651E+04        | 3.6849E+05 |
| 9.9570E+00        | 9.7511E-05                   | 4.01                   | 9.7511E+03        | 5.8900E+04 |
| 1.2446E+01        | 1.3997E-05                   | 4.85                   | 1.3997E+03        | 8.3514E+03 |
| 1.4935E+01        | 2.5898E-06                   | 5.59                   | 2.5898E+02        | 1.1407E+03 |
| 1.7425E+01        | 6.6573E-07                   | 6.18                   | 6.6573E+01        | 1.9240E+02 |
| 1.9914E+01        | 1.9252E-07                   | 6.72                   | 1.9252E+01        | 4.7321E+01 |
| 2.2403E+01        | 5.4384E-08                   | 7.26                   | 5.4384E+00        | 1.3813E+01 |
| 2.4892E+01        | 1.4340E-08                   | 7.84                   | 1.4340E+00        | 4.0044E+00 |
| 2.7382E+01        | 3.4545E-09                   | 8.46                   | 3.4545E-01        | 1.0885E+00 |
| 2.9871E+01        | 7.4971E-10                   | 9.13                   | 7.4971E-02        | 2.7048E-01 |
| 3.2360E+01        | 1.4535E-10                   | 9.84                   | 1.4535E-02        | 6.0437E-02 |
| 3.4849E+01        | 2.5059E-11                   | 10.60                  | 2.5059E-03        | 1.2029E-02 |
| 3.7339E+01        | 3.8335E-12                   | 11.42                  | 3.8335E-04        | 2.1225E-03 |
| 3.9828E+01        | 5.1978E-13                   | 12.28                  | 5.1978E-05        | 3.3137E-04 |
| 4.2317E+01        | 6.2422E-14                   | 13.20                  | 6.2422E-06        | 4.5736E-05 |
| 4.4806E+01        | 6.6370E-15                   | 14.18                  | 6.6370E-07        | 5.5785E-06 |
| 4.7296E+01        | 6.2460E-16                   | 15.20                  | 6.2460E-08        | 6.0124E-07 |
| 4.9785E+01        | 5.2019E-17                   | 16.28                  | 5.2019E-09        | 5.7259E-08 |
| 5.2274E+01        | 3.8337E-18                   | 17.42                  | 3.8337E-10        | 4.8185E-09 |
| 5.4763E+01        | 2.5002E-19                   | 18.60                  | 2.5002E-11        | 3.5837E-10 |
| 5.7253E+01        | 1.4430E-20                   | 19.84                  | 1.4430E-12        | 2.3559E-11 |
| 5.9742E+01        | 7.3703E-22                   | 21.13                  | 7.3703E-14        | 1.3693E-12 |
| 6.2231E+01        | 3.3318E-23                   | 22.48                  | 3.3318E-15        | 7.0371E-14 |
| 6.4720E+01        | 1.3331E-24                   | 23.88                  | 1.3331E-16        | 3.1985E-15 |
| 6.7210E+01        | 4.7208E-26                   | 25.33                  | 4.7208E-18        | 1.2859E-16 |
| 6.9699E+01        | 1.4795E-27                   | 26.83                  | 1.4795E-19        | 4.5729E-18 |
| 7.2188E+01        | 4.1034E-29                   | 28.39                  | 4.1034E-21        | 1.4385E-19 |
| 7.4677E+01        | 1.0069E-30                   | 30.00                  | 1.0069E-22        | 4.0027E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 9.9248E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 1.2942E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 1.6679E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 2.1204E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 2.5523E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 2.9402E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 3.2890E+01 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE YAW DISPLACEMENT (DEGREE/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E    |             | A N G L E  |             |            |             |
|---------------|---------------------|------------|-------------|------------|-------------|------------|-------------|
|               |                     | 15.00 DEG. | AMPL. PHASE | 30.00 DEG. | AMPL. PHASE | 45.00 DEG. | AMPL. PHASE |
| .2000         | 5.7398              | .0131      | -9.1        | .0224      | -9.7        | .0255      | -10.9       |
| .2500         | 3.6735              | .0271      | -13.0       | .0457      | -13.3       | .0508      | -14.6       |
| .3000         | 2.5510              | .0468      | -16.3       | .0782      | -16.9       | .0849      | -20.5       |
| .3500         | 1.8742              | .0714      | -19.5       | .1187      | -21.2       | .1123      | -29.8       |
| .4000         | 1.4349              | .0984      | -22.5       | .1621      | -25.6       | .1245      | -26.0       |
| .4500         | 1.1338              | .1224      | -24.9       | .2018      | -28.8       | .1556      | -20.1       |
| .5000         | .9184               | .1360      | -26.5       | .2295      | -30.0       | .1843      | -18.6       |
| .5500         | .7590               | .1304      | -26.5       | .2311      | -29.5       | .1963      | -18.2       |
| .6000         | .6378               | .1226      | -26.4       | .1946      | -27.4       | .1824      | -17.8       |
| .6500         | .5434               | .1127      | -26.4       | .1177      | -18.9       | .1372      | -17.2       |
| .7000         | .4686               | .1007      | -26.3       | .1084      | -18.9       | .0720      | -20.9       |
| .7500         | .4082               | .0865      | -26.1       | .0971      | -19.0       | .0207      | 28.5        |
| .8000         | .3587               | .0701      | -25.8       | .0839      | -19.1       | .0907      | 126.7       |
| .8500         | .3178               | .0516      | -25.3       | .0686      | -19.2       | .1680      | 140.3       |
| .9000         | .2834               | .0310      | -24.1       | .0514      | -19.4       | .1563      | 141.1       |
| .9500         | .2544               | .0083      | -15.4       | .0322      | -19.9       | .1430      | 142.2       |
| 1.0000        | .2296               | .0039      | 115.8       | .0111      | -22.5       | .1279      | 143.7       |
| 1.0500        | .2082               | .0050      | 163.2       | .0122      | 165.0       | .1113      | 145.8       |
| 1.1000        | .1897               | .0010      | 178.1       | .0163      | 162.6       | .0933      | 149.1       |
| 1.1500        | .1736               | .0017      | -30.2       | .0055      | -174.4      | .0741      | 154.4       |
| 1.2000        | .1594               | .0014      | -33.0       | .0035      | -38.8       | .0545      | 164.4       |
| 1.2500        | .1469               | .0007      | 131.4       | .0039      | -25.0       | .0372      | -173.7      |
| 1.3000        | .1359               | .0013      | 141.6       | .0006      | 25.4        | .0128      | -109.6      |
| 1.3500        | .1260               | .0007      | -63.6       | .0026      | 138.7       | .0110      | -24.4       |
| 1.4000        | .1171               | .0008      | -27.2       | .0011      | 172.7       | .0057      | 10.3        |
| 1.4500        | .1092               | .0008      | 108.8       | .0024      | -51.0       | .0028      | 89.8        |
| 1.5000        | .1020               | .0004      | -173.0      | .0012      | 19.7        | .0035      | 156.8       |
| 1.5500        | .0956               | .0005      | -59.3       | .0018      | 124.1       | .0028      | -158.1      |
| 1.6000        | .0897               | .0003      | 50.4        | .0010      | -135.0      | .0027      | -60.5       |
| 1.6500        | .0843               | .0003      | 146.3       | .0011      | -44.6       | .0028      | -10.4       |
| 1.7000        | .0794               | .0002      | -95.5       | .0007      | 66.3        | .0028      | 89.0        |
| 1.7500        | .0750               | .0001      | 11.3        | .0006      | 158.2       | .0023      | 162.2       |
| 1.8000        | .0709               | .0001      | 126.3       | .0005      | -90.3       | .0019      | -98.8       |
|               |                     |            |             |            |             | .0085      | -128.9      |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE YAW DISPLACEMENT (DEGREE/ FEET )

| WAVE FREQ. | WAVE/SHIP LENGTH | AMPL. | PHASE  | W A V E 75.00 DEG. | AMPL. | PHASE  | W A V E 90.00 DEG. | AMPL. | PHASE  | W A V E 105.00 DEG. | AMPL. | PHASE  | W A V E 120.00 DEG. |
|------------|------------------|-------|--------|--------------------|-------|--------|--------------------|-------|--------|---------------------|-------|--------|---------------------|
| .2000      | 5.7398           | .0130 | -23.9  | .0052              | .0052 | -88.6  | .0125              | .0125 | -156.4 | .0205               | .0205 | -170.6 |                     |
| .2500      | 3.6735           | .0207 | -42.0  | .0086              | .0086 | -178.9 | .0176              | .0176 | 168.4  | .0243               | .0243 | 174.9  |                     |
| .3000      | 2.5510           | .0231 | -7.9   | .0004              | .0004 | 173.1  | .0219              | .0219 | -179.9 | .0341               | .0341 | -178.3 |                     |
| .3500      | 1.8742           | .0408 | -8.3   | .0027              | .0027 | -64.9  | .0295              | .0295 | -175.7 | .0447               | .0447 | -175.8 |                     |
| .4000      | 1.4349           | .0571 | -9.6   | .0049              | .0049 | -66.0  | .0376              | .0376 | -173.8 | .0543               | .0543 | -174.5 |                     |
| .4500      | 1.1338           | .0738 | -10.4  | .0068              | .0068 | -66.6  | .0454              | .0454 | -173.0 | .0620               | .0620 | -173.9 |                     |
| .5000      | .9184            | .0905 | -10.9  | .0084              | .0084 | -66.5  | .0524              | .0524 | -172.7 | .0669               | .0669 | -173.9 |                     |
| .5500      | .7590            | .1065 | -11.3  | .0100              | .0100 | -65.7  | .0585              | .0585 | -173.1 | .0684               | .0684 | -174.3 |                     |
| .6000      | .6378            | .1209 | -11.5  | .0110              | .0110 | -64.1  | .0630              | .0630 | -173.8 | .0660               | .0660 | -174.6 |                     |
| .6500      | .5434            | .1323 | -11.6  | .0119              | .0119 | -62.0  | .0665              | .0665 | -174.7 | .0592               | .0592 | -175.1 |                     |
| .7000      | .4686            | .1398 | -11.5  | .0123              | .0123 | -59.7  | .0680              | .0680 | -175.4 | .0482               | .0482 | -175.9 |                     |
| .7500      | .4082            | .1423 | -11.4  | .0122              | .0122 | -56.3  | .0673              | .0673 | -176.1 | .0346               | .0346 | -177.5 |                     |
| .8000      | .3587            | .1389 | -10.9  | .0119              | .0119 | -52.7  | .0638              | .0638 | -176.8 | .0207               | .0207 | -179.4 |                     |
| .8500      | .3178            | .1296 | -10.1  | .0113              | .0113 | -49.0  | .0580              | .0580 | -177.5 | .0087               | .0087 | -172.3 |                     |
| .9000      | .2834            | .1144 | -8.9   | .0107              | .0107 | -45.1  | .0502              | .0502 | -178.6 | .0015               | .0015 | 79.3   |                     |
| .9500      | .2544            | .0943 | -7.2   | .0103              | .0103 | -41.4  | .0410              | .0410 | -179.9 | .0053               | .0053 | 10.1   |                     |
| 1.0000     | .2296            | .0708 | -4.5   | .0096              | .0096 | -37.9  | .0313              | .0313 | 178.4  | .0067               | .0067 | -.1    |                     |
| 1.0500     | .2082            | .0455 | .4     | .0090              | .0090 | -34.5  | .0218              | .0218 | 175.9  | .0056               | .0056 | -9.9   |                     |
| 1.1000     | .1897            | .0215 | 12.3   | .0084              | .0084 | -31.4  | .0133              | .0133 | 172.0  | .0035               | .0035 | -25.2  |                     |
| 1.1500     | .1736            | .0067 | 94.8   | .0077              | .0077 | -28.5  | .0062              | .0062 | 164.1  | .0015               | .0015 | -61.8  |                     |
| 1.2000     | .1594            | .0185 | 159.9  | .0071              | .0071 | -25.7  | .0012              | .0012 | 112.3  | .0012               | .0012 | -143.8 |                     |
| 1.2500     | .1469            | .0280 | 172.5  | .0064              | .0064 | -22.9  | .0031              | .0031 | 6.8    | .0015               | .0015 | 174.8  |                     |
| 1.3000     | .1359            | .0312 | -178.9 | .0057              | .0057 | -20.0  | .0049              | .0049 | -5.8   | .0013               | .0013 | 148.5  |                     |
| 1.3500     | .1260            | .0284 | -169.5 | .0050              | .0050 | -17.0  | .0053              | .0053 | -13.6  | .0008               | .0008 | 113.3  |                     |
| 1.4000     | .1171            | .0213 | -155.7 | .0044              | .0044 | -14.0  | .0047              | .0047 | -21.6  | .0005               | .0005 | 49.5   |                     |
| 1.4500     | .1092            | .0128 | -128.3 | .0037              | .0037 | -10.9  | .0034              | .0034 | -31.7  | .0005               | .0005 | -9.4   |                     |
| 1.5000     | .1020            | .0093 | -67.9  | .0031              | .0031 | -7.9   | .0020              | .0020 | -48.9  | .0004               | .0004 | -52.4  |                     |
| 1.5500     | .0956            | .0129 | -20.5  | .0026              | .0026 | -5.0   | .0009              | .0009 | -92.2  | .0001               | .0001 | -93.2  |                     |
| 1.6000     | .0897            | .0159 | 3.5    | .0022              | .0022 | -2.8   | .0010              | .0010 | -165.7 | .0003               | .0003 | -144.9 |                     |
| 1.6500     | .0843            | .0155 | 23.7   | .0017              | .0017 | -1.6   | .0013              | .0013 | 162.8  | .0002               | .0002 | 131.6  |                     |
| 1.7000     | .0794            | .0123 | 49.7   | .0014              | .0014 | -2.0   | .0014              | .0014 | 144.6  | .0002               | .0002 | 72.6   |                     |
| 1.7500     | .0750            | .0093 | 91.6   | .0011              | .0011 | -5.0   | .0011              | .0011 | 126.5  | .0002               | .0002 | 13.4   |                     |
| 1.8000     | .0709            | .0093 | 141.5  | .0009              | .0009 | -11.5  | .0007              | .0007 | 101.0  | .0001               | .0001 | -60.2  |                     |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE YAW DISPLACEMENT (DEGREE/ FEET )

| WAVE   | WAVE/SHIP | 135.00 DEG.  | 150.00 DEG.  | 165.00 DEG.  |
|--------|-----------|--------------|--------------|--------------|
| FREQ.  | LENGTH    | AMPL. PHASE  | AMPL. PHASE  | AMPL. PHASE  |
| .2000  | 5.7398    | .0226 178.9  | .0175 172.1  | .0091 170.0  |
| .2500  | 3.6735    | .0255 178.1  | .0208 179.8  | .0115 -179.4 |
| .3000  | 2.5510    | .0356 -177.1 | .0284 -176.2 | .0155 -175.7 |
| .3500  | 1.8742    | .0449 -175.0 | .0346 -174.3 | .0185 -173.9 |
| .4000  | 1.4349    | .0519 -173.9 | .0380 -173.4 | .0196 -173.1 |
| .4500  | 1.1338    | .0553 -173.6 | .0378 -173.2 | .0185 -173.0 |
| .5000  | .9184     | .0542 -173.7 | .0337 -173.2 | .0151 -172.9 |
| .5500  | .7590     | .0487 -173.7 | .0255 -173.5 | .0099 -173.9 |
| .6000  | .6378     | .0384 -174.3 | .0150 -175.3 | .0041 -178.2 |
| .6500  | .5434     | .0249 -175.9 | .0050 176.7  | .0006 57.4   |
| .7000  | .4686     | .0115 179.4  | .0021 27.7   | .0023 12.6   |
| .7500  | .4082     | .0016 133.5  | .0046 9.7    | .0022 3.4    |
| .8000  | .3587     | .0049 14.1   | .0038 -.1    | .0010 -17.1  |
| .8500  | .3178     | .0061 3.9    | .0018 -23.0  | .0004 -101.6 |
| .9000  | .2834     | .0045 -7.6   | .0008 -104.2 | .0005 -159.0 |
| .9500  | .2544     | .0021 -34.2  | .0009 -160.7 | .0003 157.8  |
| 1.0000 | .2296     | .0011 -111.0 | .0007 158.6  | .0002 76.8   |
| 1.0500 | .2082     | .0013 -166.7 | .0004 88.3   | .0002 12.9   |
| 1.1000 | .1897     | .0010 159.2  | .0004 19.3   | .0001 -41.9  |
| 1.1500 | .1736     | .0006 106.2  | .0003 -29.6  | .0001 -136.6 |
| 1.2000 | .1594     | .0005 32.2   | .0002 -117.5 | .0001 166.7  |
| 1.2500 | .1469     | .0004 -15.6  | .0002 179.0  | .0001 61.8   |
| 1.3000 | .1359     | .0002 -77.1  | .0001 87.3   | .0008 147.5  |
| 1.3500 | .1260     | .0002 -157.6 | .0001 14.5   | .0000 -164.8 |
| 1.4000 | .1171     | .0002 136.4  | .0000 -97.2  | .0000 139.3  |
| 1.4500 | .1092     | .0001 36.7   | .0001 176.1  | .0000 41.4   |
| 1.5000 | .1020     | .0001 -9.1   | .0001 92.7   | .0000 -52.3  |
| 1.5500 | .0956     | .0001 -116.6 | .0001 8.9    | .0000 -139.1 |
| 1.6000 | .0897     | .0001 -174.6 | .0001 -75.9  | .0000 135.1  |
| 1.6500 | .0843     | .0001 108.9  | .0001 -179.3 | .0000 5.9    |
| 1.7000 | .0794     | .0001 28.2   | .0001 124.1  | .0000 27.8   |
| 1.7500 | .0750     | .0001 -53.6  | .0001 -4.3   | .0001 -151.1 |
| 1.8000 | .0709     | .0000 -138.4 | .0000 107.1  | .0005 170.7  |

SHIP MOTION PROGRAM 77.1

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SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM YAW DISPLACEMENT (DEGREE)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 4.1460E-02          | .65113           | 616.0    |
| 4.879                | 9.1159E-02          | .64261           | 600.6    |
| 7.334                | 1.5022E-01          | .62977           | 574.0    |
| 10.497               | 2.1504E-01          | .62975           | 574.0    |
| 13.867               | 2.9478E-01          | .62269           | 557.6    |
| 17.894               | 3.7586E-01          | .62527           | 563.7    |
| 23.554               | 5.0864E-01          | .61816           | 546.1    |
| 28.835               | 6.2681E-01          | .61359           | 533.1    |
| 37.139               | 7.9018E-01          | .60694           | 508.9    |
| 47.602               | 1.0034E+00          | .60602           | 504.3    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8877              | 1.9489E-01 | 2.0828E-01           | 2.1649E-01 | 2.2098E-01 |
| 4.879                | .8908              | 4.3413E-01 | 4.6413E-01           | 4.8247E-01 | 4.9259E-01 |
| 7.334                | .8954              | 7.3321E-01 | 7.8542E-01           | 8.1714E-01 | 8.3496E-01 |
| 10.497               | .8954              | 1.0496E+00 | 1.1244E+00           | 1.1698E+00 | 1.1953E+00 |
| 13.867               | .8978              | 1.4615E+00 | 1.5676E+00           | 1.6310E+00 | 1.6682E+00 |
| 17.894               | .8970              | 1.8527E+00 | 1.9862E+00           | 2.0665E+00 | 2.1130E+00 |
| 23.554               | .8994              | 2.5478E+00 | 2.7351E+00           | 2.8462E+00 | 2.9113E+00 |
| 28.835               | .9010              | 3.1726E+00 | 3.4087E+00           | 3.5478E+00 | 3.6292E+00 |
| 37.139               | .9032              | 4.0598E+00 | 4.3679E+00           | 4.5476E+00 | 4.6527E+00 |
| 47.602               | .9035              | 5.1659E+00 | 5.5592E+00           | 5.7883E+00 | 5.9223E+00 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM YAW DISPLACEMENT (DEGREE)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 5.0516E-01        | 5.0416E-02                   | 1.30                   | 5.0416E+06        | 9.4958E+07 |
| 1.0105E+00        | 6.7805E-03                   | 2.17                   | 6.7805E+05        | 4.3636E+06 |
| 1.5155E+00        | 1.2883E-03                   | 2.89                   | 1.2883E+05        | 5.4922E+05 |
| 2.0206E+00        | 2.3058E-04                   | 3.64                   | 2.3058E+04        | 1.0577E+05 |
| 2.5258E+00        | 3.5645E-05                   | 4.45                   | 3.5645E+03        | 1.9494E+04 |
| 3.0310E+00        | 5.1557E-06                   | 5.29                   | 5.1557E+02        | 3.0490E+03 |
| 3.5361E+00        | 8.2391E-07                   | 6.08                   | 8.2391E+01        | 4.3317E+02 |
| 4.0413E+00        | 1.7021E-07                   | 6.77                   | 1.7021E+01        | 6.5370E+01 |
| 4.5464E+00        | 4.2128E-08                   | 7.38                   | 4.2128E+00        | 1.2808E+01 |
| 5.0516E+00        | 1.0585E-08                   | 7.98                   | 1.0585E+00        | 3.1544E+00 |
| 5.5567E+00        | 2.4854E-09                   | 8.60                   | 2.4854E-01        | 8.0993E-01 |
| 6.0619E+00        | 5.2972E-10                   | 9.28                   | 5.2972E-02        | 1.9557E-01 |
| 6.5671E+00        | 1.0125E-10                   | 9.99                   | 1.0125E-02        | 4.2848E-02 |
| 7.0722E+00        | 1.7250E-11                   | 10.76                  | 1.7250E-03        | 8.3999E-03 |
| 7.5774E+00        | 2.6113E-12                   | 11.58                  | 2.6113E-04        | 1.4638E-03 |
| 8.0825E+00        | 3.5070E-13                   | 12.46                  | 3.5070E-05        | 2.2606E-04 |
| 8.5877E+00        | 4.1747E-14                   | 13.38                  | 4.1747E-06        | 3.0895E-05 |
| 9.0929E+00        | 4.4024E-15                   | 14.36                  | 4.4024E-07        | 3.7344E-06 |
| 9.5980E+00        | 4.1113E-16                   | 15.39                  | 4.1113E-08        | 3.9913E-07 |
| 1.0103E+01        | 3.3990E-17                   | 16.47                  | 3.3990E-09        | 3.7714E-08 |
| 1.0608E+01        | 2.4871E-18                   | 17.60                  | 2.4871E-10        | 3.1503E-09 |
| 1.1113E+01        | 1.6104E-19                   | 18.79                  | 1.6104E-11        | 2.3261E-10 |
| 1.1619E+01        | 9.2253E-21                   | 20.04                  | 9.2253E-13        | 1.5181E-11 |
| 1.2124E+01        | 4.6750E-22                   | 21.33                  | 4.6750E-14        | 8.7578E-13 |
| 1.2629E+01        | 2.0955E-23                   | 22.68                  | 2.0955E-15        | 4.4655E-14 |
| 1.3134E+01        | 8.3073E-25                   | 24.08                  | 8.3073E-17        | 2.0124E-15 |
| 1.3639E+01        | 2.9126E-26                   | 25.54                  | 2.9126E-18        | 8.0160E-17 |
| 1.4144E+01        | 9.0307E-28                   | 27.04                  | 9.0307E-20        | 2.8223E-18 |
| 1.4650E+01        | 2.4762E-29                   | 28.61                  | 2.4762E-21        | 8.7831E-20 |
| 1.5155E+01        | 6.0043E-31                   | 30.22                  | 6.0043E-23        | 2.4161E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 2.2467E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 2.8579E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 3.4828E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 4.2337E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 5.0714E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 5.8543E+00 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 10 CYCLES = 6.5706E+00 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE ROLL DISPLACEMENT (DEGREE/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E |        | A N G L E |        | AMPL.<br>AMPL. | PHASE<br>PHASE | WAVE<br>15.00 DEG. | WAVE<br>30.00 DEG. | WAVE<br>45.00 DEG. | WAVE<br>60.00 DEG. |
|---------------|---------------------|---------|--------|-----------|--------|----------------|----------------|--------------------|--------------------|--------------------|--------------------|
|               |                     | AMPL.   | PHASE  | AMPL.     | PHASE  |                |                |                    |                    |                    |                    |
| .2000         | 5.7398              | .0450   | -58.3  | .0852     | -61.7  | .1172          | -68.2          | .1417              | -78.5              |                    |                    |
| .2500         | 3.6735              | .1041   | -60.3  | .2044     | -64.2  | .3026          | -72.4          | .4178              | -89.5              |                    |                    |
| .3000         | 2.5510              | .2131   | -65.3  | .4533     | -71.0  | .7985          | -88.0          | 1.1685             | -144.6             |                    |                    |
| .3500         | 1.8742              | .3751   | -71.7  | .9005     | -81.8  | 1.8212         | -126.4         | .9504              | 163.3              |                    |                    |
| .4000         | 1.4349              | .5467   | -77.5  | 1.5012    | -93.5  | 2.3032         | -169.1         | .7924              | 149.6              |                    |                    |
| .4500         | 1.1338              | .6453   | -81.6  | 2.0259    | -100.8 | 2.3562         | 169.0          | .7664              | 143.2              |                    |                    |
| .5000         | .9134               | .6168   | -85.1  | 2.1613    | -102.0 | 2.5146         | 157.5          | .7871              | 138.2              |                    |                    |
| .5500         | .7590               | .5942   | -85.2  | 1.8196    | -100.6 | 2.7877         | 150.5          | .8234              | 133.1              |                    |                    |
| .6000         | .6378               | .5630   | -85.4  | 1.1923    | -101.8 | 3.1370         | 147.2          | .8569              | 127.7              |                    |                    |
| .6500         | .5434               | .5231   | -85.7  | .5721     | -112.1 | 3.4876         | 149.7          | .8719              | 121.9              |                    |                    |
| .7000         | .4686               | .4746   | -86.1  | .5469     | -110.6 | 3.3482         | 165.1          | .8527              | 115.5              |                    |                    |
| .7500         | .4082               | .4174   | -86.7  | .5169     | -108.6 | 1.5236         | 179.9          | .7848              | 108.2              |                    |                    |
| .8000         | .3587               | .3518   | -87.6  | .4825     | -105.9 | .8734          | 122.1          | .6572              | 99.1               |                    |                    |
| .8500         | .3178               | .2776   | -89.2  | .4445     | -102.4 | 1.0503         | 102.8          | .4716              | 84.7               |                    |                    |
| .9000         | .2834               | .1953   | -92.4  | .4041     | -97.6  | .9762          | 103.0          | .2803              | 48.8               |                    |                    |
| .9500         | .2544               | .1062   | -101.6 | .3631     | -91.0  | .8912          | 103.2          | .3261              | -18.9              |                    |                    |
| 1.0000        | .2296               | .1470   | 42.1   | .3249     | -81.9  | .7951          | 103.5          | .6012              | -46.7              |                    |                    |
| 1.0500        | .2082               | .0056   | 91.9   | .2948     | -69.7  | .6880          | 103.9          | .8844              | -55.4              |                    |                    |
| 1.1000        | .1897               | .0158   | -111.5 | .0804     | 62.7   | .5700          | 104.5          | 1.0819             | -56.7              |                    |                    |
| 1.1500        | .1736               | .0080   | -128.3 | .0537     | -112.0 | .4411          | 105.6          | 1.1063             | -50.9              |                    |                    |
| 1.2000        | .1594               | .0044   | 89.5   | .0322     | -118.8 | .3015          | 107.7          | .6739              | -26.4              |                    |                    |
| 1.2500        | .1469               | .0049   | 60.4   | .0064     | 119.7  | .1524          | 114.6          | .6954              | -122.7             |                    |                    |
| 1.3000        | .1359               | .0023   | -109.0 | .0144     | 65.0   | .4194          | -134.5         | .7374              | -94.6              |                    |                    |
| 1.3500        | .1260               | .0027   | -122.6 | .0028     | 16.8   | .0557          | -129.2         | .6871              | -93.9              |                    |                    |
| 1.4000        | .1171               | .0013   | 52.0   | .0080     | -122.3 | .0341          | 78.3           | .6324              | -93.1              |                    |                    |
| 1.4500        | .1092               | .0008   | 48.4   | .0014     | -126.0 | .0295          | 57.4           | .5734              | -92.1              |                    |                    |
| 1.5000        | .1020               | .0007   | -139.5 | .0039     | 49.4   | .0025          | -44.0          | .5102              | -90.7              |                    |                    |
| 1.5500        | .0956               | .0002   | 43.5   | .0004     | 145.6  | .0147          | -125.5         | .4430              | -88.8              |                    |                    |
| 1.6000        | .0897               | .0003   | 41.1   | .0016     | -137.4 | .0038          | -130.3         | .3721              | -85.9              |                    |                    |
| 1.6500        | .0843               | .0004   | -159.7 | .0009     | 17.3   | .0072          | 41.2           | .2984              | -81.5              |                    |                    |
| 1.7000        | .0794               | .0002   | -44.1  | .0006     | 54.6   | .0034          | 74.7           | .2237              | -73.6              |                    |                    |
| 1.7500        | .0750               | .0002   | 23.8   | .0008     | -172.1 | .0040          | -153.1         | .1434              | -3.4               |                    |                    |
| 1.8000        | .0709               | .0003   | 143.9  | .0005     | -60.5  | .0018          | -99.0          | .0434              | -99.4              |                    |                    |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE ROLL DISPLACEMENT (DEGREE/ FEET )

| WAVE FREQ. | WAVE/SHIP LENGTH | 75.00 DEG.   | W A V E      | A N G L E    | 90.00 DEG.   | 105.00 DEG. | 120.00 DEG. |
|------------|------------------|--------------|--------------|--------------|--------------|-------------|-------------|
|            |                  | AMPL. PHASE  | AMPL. PHASE  | AMPL. PHASE  | AMPL. PHASE  | AMPL. PHASE | AMPL. PHASE |
| .2000      | 5.7398           | .1644 -94.3  | .1984 -115.5 | .2579 -140.8 | .3368 -170.2 |             |             |
| .2500      | 3.6735           | .5913 -129.7 | .5524 154.7  | .3281 102.5  | .2250 77.6   |             |             |
| .3000      | 2.5510           | .5319 148.4  | .2407 107.3  | .1688 75.2   | .1427 58.8   |             |             |
| .3500      | 1.8742           | .3427 134.3  | .1579 98.1   | .1286 63.4   | .1231 50.7   |             |             |
| .4000      | 1.4349           | .2874 132.3  | .1211 93.9   | .1131 55.1   | .1177 47.0   |             |             |
| .4500      | 1.1338           | .2690 132.6  | .0983 91.2   | .1066 49.1   | .1178 46.3   |             |             |
| .5000      | .9184            | .2657 133.0  | .0817 89.2   | .1046 45.2   | .1166 47.4   |             |             |
| .5500      | .7590            | .2693 132.8  | .0683 87.7   | .1036 42.9   | .1149 50.1   |             |             |
| .6000      | .6378            | .2754 131.8  | .0581 86.7   | .1039 41.8   | .1087 52.9   |             |             |
| .6500      | .5434            | .2819 129.8  | .0487 86.1   | .1020 42.7   | .0980 57.7   |             |             |
| .7000      | .4686            | .2868 127.0  | .0404 85.7   | .0983 43.2   | .0839 63.6   |             |             |
| .7500      | .4082            | .2874 123.5  | .0335 86.5   | .0931 45.5   | .0673 70.7   |             |             |
| .8000      | .3587            | .2846 119.3  | .0265 87.1   | .0867 48.1   | .0496 79.6   |             |             |
| .8500      | .3178            | .2766 114.6  | .0191 89.0   | .0790 51.5   | .0320 92.0   |             |             |
| .9000      | .2834            | .2620 109.3  | .0126 90.1   | .0697 55.6   | .0176 113.7  |             |             |
| .9500      | .2544            | .2405 103.7  | .0062 93.5   | .0597 60.1   | .0096 163.2  |             |             |
| 1.0000     | .2296            | .2125 97.5   | .0009 148.2  | .0492 65.4   | .0107 -143.3 |             |             |
| 1.0500     | .2082            | .1809 90.8   | .0049 -102.1 | .0391 71.5   | .0126 -121.7 |             |             |
| 1.1000     | .1897            | .1419 82.5   | .0095 -97.4  | .0295 78.9   | .0117 -112.7 |             |             |
| 1.1500     | .1736            | .1007 71.0   | .0133 -95.6  | .0209 88.0   | .0085 -109.9 |             |             |
| 1.2000     | .1594            | .0624 50.5   | .0162 -94.7  | .0137 100.3  | .0043 -114.8 |             |             |
| 1.2500     | .1469            | .0401 5.2    | .0183 -94.3  | .0082 119.4  | .0009 -165.7 |             |             |
| 1.3000     | .1359            | .0484 -44.2  | .0195 -93.9  | .0047 154.1  | .0019 94.1   |             |             |
| 1.3500     | .1260            | .0656 -66.8  | .0198 -93.5  | .0039 -157.6 | .0024 79.7   |             |             |
| 1.4000     | .1171            | .0747 -77.8  | .0196 -93.3  | .0044 -125.7 | .0016 67.2   |             |             |
| 1.4500     | .1092            | .0714 -85.0  | .0186 -93.1  | .0045 -109.1 | .0005 19.6   |             |             |
| 1.5000     | .1020            | .0566 -91.9  | .0172 -92.9  | .0040 -98.1  | .0008 -86.9  |             |             |
| 1.5500     | .0956            | .0340 -103.9 | .0154 -92.8  | .0030 -88.8  | .0008 -104.2 |             |             |
| 1.6000     | .0897            | .0139 -154.8 | .0134 -92.7  | .0018 -76.8  | .0004 -141.4 |             |             |
| 1.6500     | .0843            | .0243 130.7  | .0113 -92.5  | .0007 -42.2  | .0003 100.4  |             |             |
| 1.7000     | .0794            | .0385 117.6  | .0092 -92.4  | .0007 40.1   | .0005 79.4   |             |             |
| 1.7500     | .0750            | .0420 115.5  | .0073 -92.3  | .0011 63.2   | .0002 55.9   |             |             |
| 1.8000     | .0709            | .0332 117.3  | .0056 -92.0  | .0011 68.6   | .0002 -81.5  |             |             |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE ROLL DISPLACEMENT (DEGREE/ FEET )

| WAVE FREQ. | WAVE/SHIP LENGTH | 135.00 DEG.<br>AMPL. PHASE | 150.00 DEG.<br>AMPL. PHASE | 165.00 DEG.<br>AMPL. PHASE |
|------------|------------------|----------------------------|----------------------------|----------------------------|
| .2000      | 5.7398           | .3622 156.6                | .2721 128.8                | .1351 113.4                |
| .2500      | 3.6735           | .1615 65.6                 | .1066 59.9                 | .0533 57.4                 |
| .3000      | 2.5510           | .1155 52.4                 | .0813 50.6                 | .0419 50.2                 |
| .3500      | 1.8742           | .1050 48.5                 | .0754 49.2                 | .0391 50.4                 |
| .4000      | 1.4349           | .1031 48.5                 | .0742 51.6                 | .0377 53.7                 |
| .4500      | 1.1338           | .1011 50.9                 | .0708 55.7                 | .0356 59.1                 |
| .5000      | .9184            | .0985 54.8                 | .0640 62.4                 | .0301 65.5                 |
| .5500      | .7590            | .0880 59.5                 | .0519 68.1                 | .0226 75.6                 |
| .6000      | .6378            | .0735 66.5                 | .0371 79.8                 | .0143 91.7                 |
| .6500      | .5434            | .0555 75.8                 | .0223 97.7                 | .0072 123.8                |
| .7000      | .4686            | .0367 88.8                 | .0112 136.4                | .0050 -172.3               |
| .7500      | .4082            | .0200 112.2                | .0093 -160.5               | .0059 -133.5               |
| .8000      | .3587            | .0111 164.9                | .0110 -129.1               | .0055 -120.2               |
| .8500      | .3178            | .0124 -142.6               | .0098 -118.5               | .0035 -121.8               |
| .9000      | .2834            | .0138 -122.2               | .0062 -121.3               | .0015 -149.0               |
| .9500      | .2544            | .0116 -115.8               | .0027 -149.3               | .0010 137.0                |
| 1.0000     | .2296            | .0071 -119.7               | .0018 135.0                | .0009 91.1                 |
| 1.0500     | .2082            | .0028 -150.0               | .0017 92.1                 | .0005 38.1                 |
| 1.1000     | .1897            | .0020 126.8                | .0009 49.1                 | .0004 -50.7                |
| 1.1500     | .1736            | .0024 90.6                 | .0007 -43.4                | .0004 -85.6                |
| 1.2000     | .1594            | .0015 62.2                 | .0008 -81.8                | .0001 164.4                |
| 1.2500     | .1469            | .0007 -23.9                | .0002 -147.0               | .0002 113.2                |
| 1.3000     | .1359            | .0011 -79.3                | .0004 117.4                | .0029 -41.1                |
| 1.3500     | .1260            | .0006 -106.1               | .0002 100.1                | .0002 -44.3                |
| 1.4000     | .1171            | .0004 133.3                | .0003 -49.3                | .0000 160.8                |
| 1.4500     | .1092            | .0005 110.3                | .0001 -61.1                | .0000 156.0                |
| 1.5000     | .1020            | .0001 32.8                 | .0001 134.4                | .0000 -28.1                |
| 1.5500     | .0956            | .0003 -63.2                | .0000 -83.5                | .0000 131.2                |
| 1.6000     | .0897            | .0001 -61.9                | .0001 -29.5                | .0000 -145.0               |
| 1.6500     | .0843            | .0002 113.8                | .0001 165.6                | .0000 -.9                  |
| 1.7000     | .0794            | .0000 71.1                 | .0000 -2.8                 | .0000 -130.1               |
| 1.7500     | .0750            | .0001 -44.0                | .0002 3.6                  | .0000 33.7                 |
| 1.8000     | .0709            | .0000 -147.3               | .0001 -116.6               | .0003 3.0                  |

SHIP MOTION PROGRAM 77.1

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12.29.26

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SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM ROLL DISPLACEMENT (DEGREE)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 3.3608E-01          | .56804           | 490.5    |
| 4.879                | 7.4557E-01          | .54677           | 482.3    |
| 7.334                | 1.2370E+00          | .51731           | 467.0    |
| 10.497               | 1.7708E+00          | .51726           | 467.0    |
| 13.867               | 2.4370E+00          | .50252           | 456.3    |
| 17.894               | 3.1021E+00          | .50779           | 460.5    |
| 23.554               | 4.2224E+00          | .49353           | 448.2    |
| 28.835               | 5.2379E+00          | .48474           | 438.2    |
| 37.139               | 6.7259E+00          | .47242           | 416.3    |
| 47.602               | 8.5779E+00          | .47076           | 411.6    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .9158              | 2.0543E+00 | 2.2057E+00           | 2.2963E+00 | 2.3490E+00 |
| 4.879                | .9222              | 4.6172E+00 | 4.9593E+00           | 5.1630E+00 | 5.2822E+00 |
| 7.334                | .9307              | 7.7955E+00 | 8.3789E+00           | 8.7238E+00 | 8.9256E+00 |
| 10.497               | .9307              | 1.1159E+01 | 1.1994E+01           | 1.2488E+01 | 1.2777E+01 |
| 13.867               | .9347              | 1.5485E+01 | 1.6651E+01           | 1.7338E+01 | 1.7740E+01 |
| 17.894               | .9333              | 1.9654E+01 | 2.1131E+01           | 2.2002E+01 | 2.2512E+01 |
| 23.554               | .9371              | 2.6948E+01 | 2.8987E+01           | 3.0184E+01 | 3.0884E+01 |
| 28.835               | .9394              | 3.3538E+01 | 3.6088E+01           | 3.7581E+01 | 3.8454E+01 |
| 37.139               | .9426              | 4.3046E+01 | 4.6345E+01           | 4.8269E+01 | 4.9394E+01 |
| 47.602               | .9430              | 5.4825E+01 | 5.9032E+01           | 6.1485E+01 | 6.2919E+01 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM ROLL DISPLACEMENT (DEGREE)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 5.3472E+00        | 4.6279E-02                   | 1.33                   | 4.6279E+06        | 9.5372E+07 |
| 1.0694E+01        | 6.6024E-03                   | 2.18                   | 6.6024E+05        | 3.9677E+06 |
| 1.6041E+01        | 1.3209E-03                   | 2.88                   | 1.3209E+05        | 5.2815E+05 |
| 2.1389E+01        | 2.4930E-04                   | 3.60                   | 2.4930E+04        | 1.0716E+05 |
| 2.6736E+01        | 4.0361E-05                   | 4.39                   | 4.0361E+03        | 2.0894E+04 |
| 3.2087E+01        | 6.0499E-06                   | 5.22                   | 6.0499E+02        | 3.4312E+03 |
| 3.7430E+01        | 9.9004E-07                   | 6.00                   | 9.9004E+01        | 5.0598E+02 |
| 4.2777E+01        | 2.0791E-07                   | 6.68                   | 2.0791E+01        | 7.8213E+01 |
| 4.8124E+01        | 5.2403E-08                   | 7.28                   | 5.2403E+00        | 1.5551E+01 |
| 5.3472E+01        | 1.3430E-08                   | 7.87                   | 1.3430E+00        | 3.8973E+00 |
| 5.8819E+01        | 3.2131E-09                   | 8.49                   | 3.2131E-01        | 1.0217E+00 |
| 6.4166E+01        | 6.9616E-10                   | 9.16                   | 6.9616E-02        | 2.5169E-01 |
| 6.9513E+01        | 1.3493E-10                   | 9.87                   | 1.3493E-02        | 5.6123E-02 |
| 7.4860E+01        | 2.3257E-11                   | 10.63                  | 2.3257E-03        | 1.1167E-02 |
| 8.0207E+01        | 3.5549E-12                   | 11.45                  | 3.5549E-04        | 1.9702E-03 |
| 8.5554E+01        | 4.8126E-13                   | 12.32                  | 4.8126E-05        | 3.0737E-04 |
| 9.0902E+01        | 5.7668E-14                   | 13.24                  | 5.7668E-06        | 4.2359E-05 |
| 9.6249E+01        | 6.1146E-15                   | 14.21                  | 6.1146E-07        | 5.1553E-06 |
| 1.0160E+02        | 5.7359E-16                   | 15.24                  | 5.7359E-08        | 5.5410E-07 |
| 1.0694E+02        | 4.7596E-17                   | 16.32                  | 4.7596E-09        | 5.2599E-08 |
| 1.1229E+02        | 3.4932E-18                   | 17.46                  | 3.4932E-10        | 4.4102E-09 |
| 1.1764E+02        | 2.2673E-19                   | 18.64                  | 2.2673E-11        | 3.2664E-10 |
| 1.2298E+02        | 1.3013E-20                   | 19.89                  | 1.3013E-12        | 2.1371E-11 |
| 1.2833E+02        | 6.6031E-22                   | 21.18                  | 6.6031E-14        | 1.2352E-12 |
| 1.3368E+02        | 2.9621E-23                   | 22.53                  | 2.9621E-15        | 6.3069E-14 |
| 1.3903E+02        | 1.1746E-24                   | 23.93                  | 1.1746E-16        | 2.8447E-15 |
| 1.4437E+02        | 4.1166E-26                   | 25.39                  | 4.1166E-18        | 1.1334E-16 |
| 1.4972E+02        | 1.2751E-27                   | 26.89                  | 1.2751E-19        | 3.9891E-18 |
| 1.5507E+02        | 3.4899E-29                   | 28.46                  | 3.4899E-21        | 1.2402E-19 |
| 1.6041E+02        | 8.4402E-31                   | 30.07                  | 8.4402E-23        | 3.4055E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 2.4071E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 3.0667E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 3.7401E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 4.5617E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 5.4574E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 6.2900E+01 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 7.0424E+01 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |        | 15.00 DEGREES |        | 30.00 DEGREES |        |
|---------------|---------------------|---------------------|--------|---------------|--------|---------------|--------|
|               |                     | AMPLITUDE           | PHASE  | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  |
| .2000         | 5.7398              | 1.6286E+03          | 35.0   | 1.4909E+03    | 35.4   | 1.1084E+03    | 37.4   |
| .2500         | 3.6735              | 4.3331E+03          | 31.7   | 4.0202E+03    | 31.7   | 3.1377E+03    | 32.0   |
| .3000         | 2.5510              | 8.9005E+03          | 31.4   | 8.3342E+03    | 31.3   | 6.7175E+03    | 31.1   |
| .3500         | 1.8742              | 1.5277E+04          | 32.7   | 1.4451E+04    | 32.4   | 1.1996E+04    | 31.8   |
| .4000         | 1.4349              | 2.2668E+04          | 35.1   | 2.1706E+04    | 34.8   | 1.8620E+04    | 33.7   |
| .4500         | 1.1338              | 2.9464E+04          | 38.9   | 2.8622E+04    | 38.2   | 2.5641E+04    | 36.5   |
| .5000         | .9184               | 3.3641E+04          | 44.4   | 3.3328E+04    | 43.3   | 3.1563E+04    | 40.6   |
| .5500         | .7530               | 3.2003E+04          | 44.3   | 3.1727E+04    | 43.2   | 3.4746E+04    | 46.1   |
| .6000         | .6378               | 2.9795E+04          | 44.1   | 2.9511E+04    | 43.2   | 3.3957E+04    | 53.4   |
| .6500         | .5434               | 2.7019E+04          | 43.7   | 2.6682E+04    | 43.1   | 2.9818E+04    | 63.4   |
| .7000         | .4686               | 2.3675E+04          | 43.3   | 2.3238E+04    | 42.9   | 2.7643E+04    | 63.3   |
| .7500         | .4082               | 1.9765E+04          | 42.5   | 1.9181E+04    | 42.7   | 2.5005E+04    | 63.0   |
| .8000         | .3587               | 1.5294E+04          | 41.1   | 1.4510E+04    | 42.2   | 2.1905E+04    | 62.7   |
| .8500         | .3178               | 1.0275E+04          | 38.1   | 9.2281E+03    | 41.2   | 1.8342E+04    | 62.1   |
| .9000         | .2834               | 4.7997E+03          | 27.3   | 3.3481E+03    | 36.1   | 1.4320E+04    | 61.2   |
| .9500         | .2544               | 2.3524E+03          | -88.7  | 3.2332E+03    | -127.6 | 9.8443E+03    | 59.3   |
| 1.0000        | .2296               | 1.6169E+03          | 15.4   | 1.6100E+03    | -20.7  | 4.9444E+03    | 53.1   |
| 1.0500        | .2082               | 1.7918E+03          | 123.6  | 1.5045E+03    | 87.6   | 1.2114E+03    | -53.7  |
| 1.1000        | .1897               | 2.2253E+03          | -173.6 | 2.2348E+03    | 162.7  | 1.3030E+03    | 68.1   |
| 1.1500        | .1736               | 1.5209E+03          | -101.2 | 1.7430E+03    | -138.3 | 2.0823E+03    | 141.6  |
| 1.2000        | .1594               | 1.3388E+03          | -30.8  | 1.3581E+03    | -57.4  | 1.8356E+03    | -168.4 |
| 1.2500        | .1469               | 3.7459E+02          | 36.1   | 8.1259E+02    | 2.0    | 1.1259E+03    | -92.5  |
| 1.3000        | .1359               | 5.2706E+02          | 175.5  | 3.3471E+02    | 137.6  | 9.2288E+02    | -20.9  |
| 1.3500        | .1260               | 6.1577E+02          | -137.3 | 5.9250E+02    | -164.0 | 4.2754E+02    | 58.9   |
| 1.4000        | .1171               | 5.3045E+02          | -80.0  | 4.9148E+02    | -109.3 | 4.3565E+02    | 164.1  |
| 1.4500        | .1092               | 4.8606E+02          | 14.1   | 4.6564E+02    | -42.6  | 4.4363E+02    | -155.8 |
| 1.5000        | .1020               | 5.0441E+02          | 94.9   | 4.7959E+02    | 51.5   | 2.9629E+02    | -95.1  |
| 1.5500        | .0956               | 3.4204E+02          | 178.1  | 5.0380E+02    | 128.2  | 4.2283E+02    | -24.4  |
| 1.6000        | .0897               | 7.5162E+02          | -47.4  | 3.5565E+02    | -114.0 | 3.8523E+02    | 59.9   |
| 1.6500        | .0843               | 8.6618E+02          | 15.4   | 8.5295E+02    | -27.0  | 5.1164E+02    | 139.1  |
| 1.7000        | .0794               | 5.0015E+02          | 125.6  | 7.1994E+02    | 55.8   | 4.3650E+02    | -119.7 |
| 1.7500        | .0750               | 1.2066E+03          | -85.1  | 6.1779E+02    | -175.2 | 7.0734E+02    | -34.9  |
| 1.8000        | .0709               | 1.5611E+03          | -14.5  | 1.4272E+03    | -62.8  | 7.2242E+02    | 66.2   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |               |                   |
|---------------|---------------------|---------------------|---------------|-------------------|
|               |                     | 45.00 DEGREES       | 60.00 DEGREES | 75.00 DEGREES     |
| .2000         | 5.7398              | 5.7362E+02          | 45.6          | 1.7605E+02 127.8  |
| .2500         | 3.6735              | 1.8649E+03          | 33.7          | 5.1434E+02 48.4   |
| .3000         | 2.5510              | 4.2945E+03          | 31.0          | 1.5834E+03 33.5   |
| .3500         | 1.8742              | 8.0773E+03          | 30.8          | 3.4457E+03 30.1   |
| .4000         | 1.4349              | 1.3204E+04          | 32.0          | 6.2208E+03 29.7   |
| .4500         | 1.1338              | 1.9309E+04          | 34.0          | 9.9203E+03 30.6   |
| .5000         | .9184               | 2.5616E+04          | 36.9          | 1.4383E+04 32.3   |
| .5500         | .7590               | 3.1006E+04          | 40.7          | 1.9272E+04 34.7   |
| .6000         | .6378               | 3.4277E+04          | 45.7          | 2.4055E+04 37.6   |
| .6500         | .5434               | 3.4518E+04          | 51.8          | 2.8067E+04 41.3   |
| .7000         | .4686               | 3.1516E+04          | 59.3          | 3.0618E+04 45.6   |
| .7500         | .4082               | 2.5937E+04          | 68.1          | 3.1141E+04 50.6   |
| .8000         | .3587               | 1.9122E+04          | 77.4          | 2.9342E+04 56.4   |
| .8500         | .3178               | 1.2654E+04          | 84.1          | 2.5323E+04 62.9   |
| .9000         | .2834               | 1.1741E+04          | 84.2          | 1.9609E+04 69.8   |
| .9500         | .2544               | 1.0692E+04          | 84.3          | 1.3098E+04 76.4   |
| 1.0000        | .2296               | 9.5078E+03          | 84.5          | 6.9255E+03 79.6   |
| 1.0500        | .2082               | 8.1878E+03          | 84.8          | 2.4897E+03 59.4   |
| 1.1000        | .1897               | 6.7323E+03          | 85.3          | 2.2327E+03 -5.1   |
| 1.1500        | .1736               | 5.1418E+03          | 86.1          | 2.7957E+03 -3.3   |
| 1.2000        | .1594               | 3.4179E+03          | 87.8          | 2.2824E+03 29.6   |
| 1.2500        | .1469               | 1.5695E+03          | 93.8          | 2.0068E+03 92.0   |
| 1.3000        | .1359               | 1.9334E+03          | 143.2         | 2.5498E+03 146.6  |
| 1.3500        | .1260               | 1.2738E+03          | -167.2        | 2.2008E+03 147.4  |
| 1.4000        | .1171               | 7.6648E+02          | -86.0         | 1.8216E+03 148.6  |
| 1.4500        | .1092               | 6.3862E+02          | -16.2         | 1.4129E+03 150.7  |
| 1.5000        | .1020               | 3.8982E+02          | 50.1          | 9.7722E+02 154.9  |
| 1.5500        | .0956               | 2.5832E+02          | 131.1         | 5.2666E+02 165.9  |
| 1.6000        | .0897               | 2.7550E+02          | 173.6         | 2.2860E+02 -120.8 |
| 1.6500        | .0843               | 2.0245E+02          | -164.9        | 6.1176E+02 -60.3  |
| 1.7000        | .0794               | 2.2499E+02          | -74.3         | 1.1592E+03 -49.8  |
| 1.7500        | .0750               | 3.7270E+02          | -23.9         | 6.4000E+02 16.6   |
| 1.8000        | .0709               | 3.5530E+02          | 68.9          | 3.5900E+02 120.4  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                |                |        |            |        |
|---------------|---------------------|---------------------|----------------|----------------|--------|------------|--------|
|               |                     | 90.00 DEGREES       | 105.00 DEGREES | 120.00 DEGREES |        |            |        |
| .2000         | 5.7398              | 7.3297E+02          | -168.4         | 6.4879E+02     | -172.6 | 3.2965E+02 | 160.2  |
| .2500         | 3.6735              | 1.1711E+03          | -165.4         | 9.2607E+02     | -173.6 | 4.2097E+02 | 96.9   |
| .3000         | 2.5510              | 1.7280E+03          | -163.2         | 1.1602E+03     | -178.0 | 1.3201E+03 | 56.2   |
| .3500         | 1.8742              | 2.4019E+03          | -161.7         | 1.2809E+03     | 172.1  | 3.2995E+03 | 44.5   |
| .4000         | 1.4349              | 3.1769E+03          | -160.8         | 1.2799E+03     | 150.8  | 6.6148E+03 | 38.8   |
| .4500         | 1.1338              | 4.0235E+03          | -160.4         | 1.4511E+03     | 111.5  | 1.1469E+04 | 34.4   |
| .5000         | .9184               | 4.8996E+03          | -160.2         | 2.4038E+03     | 74.7   | 1.7889E+04 | 29.4   |
| .5500         | .7590               | 5.7508E+03          | -160.2         | 4.4302E+03     | 49.4   | 2.5085E+04 | 22.2   |
| .6000         | .6378               | 6.5134E+03          | -160.0         | 7.3656E+03     | 32.9   | 2.9450E+04 | 10.3   |
| .6500         | .5434               | 7.1158E+03          | -159.1         | 1.0538E+04     | 12.2   | 2.6219E+04 | 7.5    |
| .7000         | .4686               | 7.5230E+03          | -157.4         | 1.0968E+04     | -11.1  | 2.5251E+04 | 14.8   |
| .7500         | .4082               | 7.8318E+03          | -153.1         | 7.9515E+03     | -16.1  | 2.4530E+04 | 17.8   |
| .8000         | .3587               | 8.4186E+03          | -145.8         | 6.8572E+03     | 2.3    | 2.1014E+04 | 18.0   |
| .8500         | .3178               | 9.8368E+03          | -142.3         | 7.7749E+03     | 16.6   | 1.4632E+04 | 15.8   |
| .9000         | .2834               | 1.1208E+04          | -144.6         | 8.8052E+03     | 21.6   | 6.5220E+03 | 13.0   |
| .9500         | .2544               | 1.1449E+04          | -148.7         | 9.0537E+03     | 21.4   | 1.4479E+03 | -166.0 |
| 1.0000        | .2296               | 1.0968E+04          | -151.1         | 8.3836E+03     | 20.4   | 7.3934E+03 | -172.6 |
| 1.0500        | .2082               | 1.0153E+04          | -152.3         | 6.8008E+03     | 18.0   | 1.0149E+04 | -177.1 |
| 1.1000        | .1897               | 9.0462E+03          | -152.3         | 4.6804E+03     | 15.1   | 9.3643E+03 | 177.6  |
| 1.1500        | .1736               | 7.8555E+03          | -151.0         | 2.3344E+03     | 10.5   | 5.9450E+03 | 171.9  |
| 1.2000        | .1594               | 6.5879E+03          | -148.9         | 1.5050E+02     | -59.1  | 1.4806E+03 | 163.3  |
| 1.2500        | .1469               | 5.2668E+03          | -145.3         | 1.7613E+03     | -168.0 | 2.1105E+03 | -19.9  |
| 1.3000        | .1359               | 4.0916E+03          | -139.6         | 2.9114E+03     | -174.5 | 3.5160E+03 | -30.8  |
| 1.3500        | .1260               | 3.0574E+03          | -130.5         | 3.2319E+03     | 179.6  | 2.6833E+03 | -47.1  |
| 1.4000        | .1171               | 2.2212E+03          | -116.2         | 2.8364E+03     | 171.3  | 9.8501E+02 | -102.9 |
| 1.4500        | .1092               | 1.7137E+03          | -95.6          | 1.9109E+03     | 159.3  | 1.5356E+03 | 158.9  |
| 1.5000        | .1020               | 1.5019E+03          | -73.0          | 8.9470E+02     | 124.4  | 1.8049E+03 | 127.6  |
| 1.5500        | .0956               | 1.4571E+03          | -54.7          | 8.6783E+02     | 38.8   | 1.0544E+03 | 84.4   |
| 1.6000        | .0897               | 1.4230E+03          | -42.6          | 1.4478E+03     | 6.4    | 8.2179E+02 | -9.8   |
| 1.6500        | .0843               | 1.3381E+03          | -35.1          | 1.6334E+03     | -9.4   | 1.0124E+03 | -68.2  |
| 1.7000        | .0794               | 1.1679E+03          | -30.7          | 1.3393E+03     | -24.8  | 7.9589E+02 | -129.7 |
| 1.7500        | .0750               | 9.3566E+02          | -28.7          | 7.5231E+02     | -52.4  | 7.5867E+02 | 151.6  |
| 1.8000        | .0709               | 6.6908E+02          | -28.8          | 4.8358E+02     | -135.0 | 7.8228E+02 | 86.5   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                |                                     |
|---------------|---------------------|---------------------|----------------|-------------------------------------|
|               |                     | 135.00 DEGREES      | 150.00 DEGREES | 165.00 DEGREES                      |
| .2000         | 5.7398              | 4.2701E+02          | 64.0           | 9.6233E+02 43.0 1.3850E+03 38.2     |
| .2500         | 3.6735              | 1.6652E+03          | 42.2           | 3.1283E+03 35.3 4.2144E+03 33.1     |
| .3000         | 2.5510              | 4.3191E+03          | 36.4           | 7.3872E+03 32.3 9.6091E+03 30.8     |
| .3500         | 1.8742              | 8.9059E+03          | 33.4           | 1.4333E+04 30.2 1.8126E+04 28.7     |
| .4000         | 1.4349              | 1.5736E+04          | 30.7           | 2.3983E+04 27.6 2.9413E+04 26.1     |
| .4500         | 1.1338              | 2.4655E+04          | 27.4           | 3.5264E+04 24.0 4.1526E+04 22.1     |
| .5000         | .9184               | 3.4443E+04          | 22.5           | 4.4825E+04 17.2 4.8690E+04 14.4     |
| .5500         | .7590               | 4.0175E+04          | 12.7           | 4.2821E+04 11.0 4.2640E+04 12.8     |
| .6000         | .6378               | 3.5965E+04          | 11.3           | 3.7506E+04 15.4 3.5565E+04 16.1     |
| .6500         | .5434               | 3.3139E+04          | 16.2           | 2.9554E+04 16.1 2.3072E+04 15.0     |
| .7000         | .4686               | 2.7536E+04          | 16.9           | 1.6262E+04 14.0 6.7734E+03 11.2     |
| .7500         | .4082               | 1.7227E+04          | 14.9           | 1.6098E+03 10.7 6.6466E+03 -173.1   |
| .8000         | .3587               | 4.9434E+03          | 11.8           | 9.0390E+03 -174.3 1.1968E+04 -179.6 |
| .8500         | .3178               | 5.6859E+03          | -171.5         | 1.2030E+04 179.4 8.6665E+03 171.2   |
| .9000         | .2834               | 1.1375E+04          | -176.6         | 7.8893E+03 171.0 1.2731E+03 135.6   |
| .9500         | .2544               | 1.1009E+04          | 177.6          | 8.1269E+02 137.7 4.3735E+03 -18.8   |
| 1.0000        | .2296               | 6.0203E+03          | 170.6          | 4.2424E+03 -22.2 4.4003E+03 -40.9   |
| 1.0500        | .2082               | 1.8612E+02          | -2.5           | 4.3563E+03 -41.9 1.7746E+03 -103.1  |
| 1.1000        | .1897               | 4.0386E+03          | -26.8          | 1.8727E+03 -95.5 1.8186E+03 165.4   |
| 1.1500        | .1736               | 4.0460E+03          | -43.2          | 1.8477E+03 171.4 8.9996E+02 79.3    |
| 1.2000        | .1594               | 1.8358E+03          | -87.3          | 1.0595E+03 110.7 1.5766E+03 -10.5   |
| 1.2500        | .1469               | 1.7249E+03          | 175.7          | 1.2753E+03 -2.3 7.6639E+02 -50.3    |
| 1.3000        | .1359               | 1.5436E+03          | 131.0          | 1.0752E+03 -45.0 5.3726E+02 146.0   |
| 1.3500        | .1260               | 7.8780E+02          | 38.2           | 3.6475E+02 -166.5 5.2664E+02 80.3   |
| 1.4000        | .1171               | 1.1358E+03          | -36.2          | 5.9331E+02 103.6 9.9009E+02 -69.2   |
| 1.4500        | .1092               | 6.6847E+02          | -93.6          | 3.3900E+02 2.4 8.1896E+01 -73.5     |
| 1.5000        | .1020               | 5.3473E+02          | 148.6          | 2.5148E+02 -104.2 2.4578E+02 16.3   |
| 1.5500        | .0956               | 5.9794E+02          | 77.7           | 1.5009E+02 83.3 2.9315E+02 -88.7    |
| 1.6000        | .0897               | 2.6021E+02          | -22.8          | 2.7894E+02 7.7 1.3164E+02 97.4      |
| 1.6500        | .0843               | 4.7791E+02          | -122.7         | 4.0404E+02 -114.9 7.7866E+02 24.3   |
| 1.7000        | .0794               | 3.2158E+02          | 138.9          | 2.0916E+02 114.7 4.9673E+02 -65.4   |
| 1.7500        | .0750               | 4.9932E+02          | 43.6           | 4.8951E+02 -47.8 5.3462E+02 97.4    |
| 1.8000        | .0709               | 3.9821E+02          | -65.4          | 4.8689E+02 -91.7 8.7218E+02 32.4    |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

## W A V E   A N G L E

| WAVE   | WAVE/SHIP | 180.00 DEGREES    |
|--------|-----------|-------------------|
| FREQ.  | LENGTH    | AMPLITUDE PHASE   |
| .2000  | 5.7398    | 1.5421E+03 37.1   |
| .2500  | 3.6735    | 4.6130E+03 32.5   |
| .3000  | 2.5510    | 1.0415E+04 30.3   |
| .3500  | 1.8742    | 1.9473E+04 28.3   |
| .4000  | 1.4349    | 3.1310E+04 25.7   |
| .4500  | 1.1338    | 4.3507E+04 21.5   |
| .5000  | .9184     | 4.9387E+04 13.6   |
| .5500  | .7590     | 4.2405E+04 13.4   |
| .6000  | .6378     | 3.4305E+04 16.0   |
| .6500  | .5434     | 2.0294E+04 14.4   |
| .7000  | .4686     | 3.5973E+03 9.5    |
| .7500  | .4082     | 3.6547E+03 -174.6 |
| .8000  | .3587     | 1.1785E+04 178.2  |
| .8500  | .3178     | 6.7185E+03 166.8  |
| .9000  | .2834     | 1.2292E+03 19.4   |
| .9500  | .2544     | 5.0016E+03 -24.0  |
| 1.0000 | .2296     | 3.5357E+03 -51.5  |
| 1.0500 | .2082     | 1.6107E+03 -144.3 |
| 1.1000 | .1897     | 1.5552E+03 144.9  |
| 1.1500 | .1736     | 1.1408E+03 27.3   |
| 1.2000 | .1594     | 1.5227E+03 -23.1  |
| 1.2500 | .1469     | 2.4818E+02 -106.9 |
| 1.3000 | .1359     | 6.8009E+02 119.1  |
| 1.3500 | .1260     | 4.0608E+02 43.9   |
| 1.4000 | .1171     | 1.6290E+02 -36.6  |
| 1.4500 | .1092     | 1.3757E+02 16.8   |
| 1.5000 | .1020     | 2.2941E+02 -32.7  |
| 1.5500 | .0956     | 2.2988E+02 -107.4 |
| 1.6000 | .0897     | 5.7077E+02 25.1   |
| 1.6500 | .0843     | 2.0163E+03 -69.9  |
| 1.7000 | .0794     | 1.2611E+02 111.3  |
| 1.7500 | .0750     | 1.1169E+03 54.9   |
| 1.8000 | .0709     | 4.2645E+02 -24.3  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

SHORT TERM VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 1.0796E+04          | .67782           | 785.7    |
| 4.879                | 2.4155E+04          | .66291           | 760.2    |
| 7.334                | 4.0494E+04          | .64047           | 722.7    |
| 10.497               | 5.7966E+04          | .64043           | 722.5    |
| 13.867               | 7.9721E+04          | .62887           | 702.0    |
| 17.894               | 1.0159E+05          | .63300           | 709.6    |
| 23.554               | 1.3741E+05          | .62190           | 688.5    |
| 28.835               | 1.6854E+05          | .61525           | 674.0    |
| 37.139               | 2.0843E+05          | .60628           | 649.0    |
| 47.602               | 2.6330E+05          | .60508           | 644.6    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | HIGHEST OCCURANCE IN |            |            |            |
|----------------------|--------------------|----------------------|------------|------------|------------|
|                      |                    | 8.0 HRS              | 24.0 HRS   | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8777              | 4.0813E+04           | 4.3501E+04 | 4.5169E+04 | 4.6080E+04 |
| 4.879                | .8833              | 9.5249E+04           | 1.0187E+05 | 1.0588E+05 | 1.0821E+05 |
| 7.334                | .8916              | 1.7126E+05           | 1.8380E+05 | 1.9126E+05 | 1.9562E+05 |
| 10.497               | .8916              | 2.4518E+05           | 2.6314E+05 | 2.7382E+05 | 2.8006E+05 |
| 13.867               | .8957              | 3.4941E+05           | 3.7545E+05 | 3.9083E+05 | 3.9982E+05 |
| 17.894               | .8942              | 4.3970E+05           | 4.7228E+05 | 4.9157E+05 | 5.0285E+05 |
| 23.554               | .8981              | 6.1491E+05           | 6.6117E+05 | 6.8835E+05 | 7.0426E+05 |
| 28.835               | .9004              | 7.6900E+05           | 8.2732E+05 | 8.6147E+05 | 8.8144E+05 |
| 37.139               | .9034              | 9.7601E+05           | 1.0508E+06 | 1.0945E+06 | 1.1200E+06 |
| 47.602               | .9038              | 1.2373E+06           | 1.3322E+06 | 1.3877E+06 | 1.4201E+06 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM VERTICAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 1.2135E+05        | 5.5747E-02                   | 1.25                   | 5.5747E+06        | 9.4425E+07 |
| 2.4270E+05        | 6.8449E-03                   | 2.15                   | 6.8449E+05        | 4.8902E+06 |
| 3.6404E+05        | 1.1575E-03                   | 2.94                   | 1.1575E+05        | 5.6875E+05 |
| 4.8539E+05        | 1.9487E-04                   | 3.71                   | 1.9487E+04        | 9.6262E+04 |
| 6.0674E+05        | 3.0055E-05                   | 4.52                   | 3.0055E+03        | 1.6482E+04 |
| 7.2809E+05        | 4.4252E-06                   | 5.35                   | 4.4252E+02        | 2.5629E+03 |
| 8.4944E+05        | 6.9825E-07                   | 6.16                   | 6.9825E+01        | 3.7270E+02 |
| 9.7079E+05        | 1.3648E-07                   | 6.86                   | 1.3648E+01        | 5.6178E+01 |
| 1.0921E+06        | 3.2345E-08                   | 7.49                   | 3.2345E+00        | 1.0413E+01 |
| 1.2135E+06        | 8.0071E-09                   | 8.10                   | 8.0071E-01        | 2.4338E+00 |
| 1.3348E+06        | 1.8799E-09                   | 8.73                   | 1.8799E-01        | 6.1272E-01 |
| 1.4562E+06        | 4.0291E-10                   | 9.39                   | 4.0291E-02        | 1.4770E-01 |
| 1.5775E+06        | 7.7611E-11                   | 10.11                  | 7.7611E-03        | 3.2530E-02 |
| 1.6989E+06        | 1.3334E-11                   | 10.88                  | 1.3334E-03        | 6.4277E-03 |
| 1.8202E+06        | 2.0355E-12                   | 11.69                  | 2.0355E-04        | 1.1299E-03 |
| 1.9416E+06        | 2.7554E-13                   | 12.56                  | 2.7554E-05        | 1.7600E-04 |
| 2.0629E+06        | 3.3041E-14                   | 13.48                  | 3.3041E-06        | 2.4250E-05 |
| 2.1843E+06        | 3.5077E-15                   | 14.45                  | 3.5077E-07        | 2.9533E-06 |
| 2.3056E+06        | 3.2958E-16                   | 15.48                  | 3.2958E-08        | 3.1782E-07 |
| 2.4270E+06        | 2.7399E-17                   | 16.56                  | 2.7399E-09        | 3.0218E-08 |
| 2.5483E+06        | 2.0151E-18                   | 17.70                  | 2.0151E-10        | 2.5384E-09 |
| 2.6697E+06        | 1.3111E-19                   | 18.88                  | 1.3111E-11        | 1.8840E-10 |
| 2.7910E+06        | 7.5470E-21                   | 20.12                  | 7.5470E-13        | 1.2357E-11 |
| 2.9124E+05        | 3.8434E-22                   | 21.42                  | 3.8434E-14        | 7.1627E-13 |
| 3.0337E+06        | 1.7319E-23                   | 22.76                  | 1.7319E-15        | 3.6703E-14 |
| 3.1551E+06        | 6.9057E-25                   | 24.16                  | 6.9057E-17        | 1.6628E-15 |
| 3.2764E+06        | 2.4368E-26                   | 25.61                  | 2.4368E-18        | 6.6620E-17 |
| 3.3977E+06        | 7.6096E-28                   | 27.12                  | 7.6096E-20        | 2.3607E-18 |
| 3.5191E+06        | 2.1030E-29                   | 28.68                  | 2.1030E-21        | 7.3993E-20 |
| 3.6404E+06        | 5.1431E-31                   | 30.29                  | 5.1431E-23        | 2.0516E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 5.2870E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 6.7645E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 8.2583E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 1.0700E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 1.1942E+06 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 1.3846E+06 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 1.5589E+06 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |               |               |
|---------------|---------------------|---------------------|---------------|---------------|
|               |                     | 15.00 DEGREES       | 30.00 DEGREES | 45.00 DEGREES |
| .2000         | 5.7398              | 3.5708E+02          | 94.4          | 6.4982E+02    |
| .2500         | 3.6735              | 6.3559E+02          | 95.0          | 1.1492E+03    |
| .3000         | 2.5510              | 1.0853E+03          | 93.7          | 1.9671E+03    |
| .3500         | 1.8742              | 1.7670E+03          | 90.7          | 3.2547E+03    |
| .4000         | 1.4349              | 2.6878E+03          | 87.0          | 5.0668E+03    |
| .4500         | 1.1338              | 3.7465E+03          | 82.9          | 7.2611E+03    |
| .5000         | .9184               | 4.7234E+03          | 78.8          | 9.4552E+03    |
| .5500         | .7590               | 4.5576E+03          | 78.4          | 1.1103E+04    |
| .6000         | .6378               | 4.3286E+03          | 77.8          | 1.1674E+04    |
| .6500         | .5434               | 4.0368E+03          | 77.0          | 1.0773E+04    |
| .7000         | .4686               | 3.6830E+03          | 75.8          | 1.0103E+04    |
| .7500         | .4082               | 3.2687E+03          | 74.0          | 9.2910E+03    |
| .8000         | .3587               | 2.7966E+03          | 71.4          | 8.3361E+03    |
| .8500         | .3178               | 2.2728E+03          | 67.1          | 7.2389E+03    |
| .9000         | .2834               | 1.7129E+03          | 59.2          | 5.9999E+03    |
| .9500         | .2544               | 1.1697E+03          | 42.2          | 4.6200E+03    |
| 1.0000        | .2296               | 6.6934E+02          | 40.6          | 3.1022E+03    |
| 1.0500        | .2082               | 3.2559E+02          | -2.7          | 1.4643E+03    |
| 1.1000        | .1897               | 3.8694E+02          | -55.9         | 4.3163E+02    |
| 1.1500        | .1736               | 2.4059E+02          | -26.9         | 7.2695E+02    |
| 1.2000        | .1594               | 4.8022E+02          | 52.8          | 5.8434E+02    |
| 1.2500        | .1469               | 5.0111E+02          | 56.3          | 6.7127E+02    |
| 1.3000        | .1359               | 3.5207E+02          | -94.1         | 9.8078E+02    |
| 1.3500        | .1260               | 5.3255E+02          | -96.9         | 1.3895E+02    |
| 1.4000        | .1171               | 4.7979E+02          | 43.8          | 1.1265E+03    |
| 1.4500        | .1092               | 3.3983E+02          | 91.0          | 4.5004E+02    |
| 1.5000        | .1020               | 5.0795E+02          | -130.4        | 1.1688E+03    |
| 1.5500        | .0956               | 3.4693E+02          | -43.7         | 5.8801E+02    |
| 1.6000        | .0897               | 4.0111E+02          | 50.3          | 9.9978E+02    |
| 1.6500        | .0843               | 3.3622E+02          | 174.8         | 7.2843E+02    |
| 1.7000        | .0794               | 3.3309E+02          | -94.6         | 7.4671E+02    |
| 1.7500        | .0750               | 3.0817E+02          | 17.4          | 6.8745E+02    |
| 1.8000        | .0709               | 2.4798E+02          | 142.9         | 5.9346E+02    |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | 60.00 DEGREES |        | 75.00 DEGREES |        | 90.00 DEGREES |        |
|---------------|---------------------|---------------|--------|---------------|--------|---------------|--------|
|               |                     | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  |
| .2000         | 5.7398              | 9.0055E+02    | 91.6   | 8.6823E+02    | 88.5   | 7.7563E+02    | 83.3   |
| .2500         | 3.6735              | 1.5695E+03    | 90.3   | 1.4713E+03    | 80.7   | 9.6106E+02    | 70.7   |
| .3000         | 2.5510              | 2.4552E+03    | 78.1   | 1.6770E+03    | 80.9   | 1.3735E+03    | 83.9   |
| .3500         | 1.8742              | 3.0554E+03    | 80.3   | 2.4424E+03    | 84.6   | 1.9031E+03    | 84.3   |
| .4000         | 1.4349              | 4.5733E+03    | 82.3   | 3.4364E+03    | 84.1   | 2.4460E+03    | 84.1   |
| .4500         | 1.1338              | 6.7834E+03    | 81.1   | 4.7172E+03    | 82.4   | 2.9829E+03    | 84.0   |
| .5000         | .9184               | 9.7652E+03    | 78.9   | 6.3769E+03    | 80.0   | 3.4726E+03    | 84.3   |
| .5500         | .7590               | 1.3513E+04    | 76.5   | 8.4968E+03    | 77.2   | 3.8615E+03    | 85.0   |
| .6000         | .6378               | 1.7826E+04    | 74.0   | 1.1110E+04    | 74.1   | 4.0838E+03    | 86.6   |
| .6500         | .5434               | 2.2240E+04    | 71.8   | 1.4251E+04    | 70.9   | 4.0827E+03    | 88.8   |
| .7000         | .4686               | 2.6040E+04    | 70.0   | 1.7801E+04    | 67.7   | 3.9303E+03    | 92.2   |
| .7500         | .4082               | 2.8373E+04    | 68.6   | 2.1625E+04    | 64.7   | 3.4718E+03    | 97.9   |
| .8000         | .3587               | 2.8474E+04    | 67.8   | 2.5414E+04    | 61.9   | 2.8473E+03    | 107.4  |
| .8500         | .3178               | 2.5945E+04    | 67.6   | 2.8781E+04    | 59.5   | 2.1281E+03    | 126.1  |
| .9000         | .2834               | 2.0986E+04    | 68.2   | 3.1310E+04    | 57.5   | 1.7714E+03    | 160.2  |
| .9500         | .2544               | 1.4445E+04    | 69.6   | 3.2553E+04    | 56.1   | 2.1502E+03    | -162.1 |
| 1.0000        | .2296               | 7.6268E+03    | 71.1   | 3.2155E+04    | 55.2   | 3.0699E+03    | -142.0 |
| 1.0500        | .2082               | 1.9208E+03    | 65.2   | 2.9770E+04    | 54.8   | 4.1766E+03    | -130.8 |
| 1.1000        | .1897               | 1.8886E+03    | -79.9  | 2.5689E+04    | 55.2   | 5.3051E+03    | -123.9 |
| 1.1500        | .1736               | 3.2761E+03    | -77.3  | 2.0120E+04    | 56.7   | 6.3845E+03    | -119.3 |
| 1.2000        | .1594               | 2.9447E+03    | -62.7  | 1.3613E+04    | 59.9   | 7.3470E+03    | -115.8 |
| 1.2500        | .1469               | 2.0286E+03    | -11.4  | 6.9519E+03    | 67.8   | 8.1514E+03    | -113.1 |
| 1.3000        | .1359               | 2.1378E+03    | 55.5   | 1.6119E+03    | 123.9  | 8.7609E+03    | -110.8 |
| 1.3500        | .1260               | 1.9491E+03    | 58.1   | 4.3603E+03    | -137.4 | 9.1372E+03    | -108.9 |
| 1.4000        | .1171               | 1.7492E+03    | 61.5   | 7.1483E+03    | -124.3 | 9.3252E+03    | -107.2 |
| 1.4500        | .1092               | 1.5421E+03    | 66.3   | 7.9435E+03    | -115.7 | 9.2229E+03    | -105.7 |
| 1.5000        | .1020               | 1.3349E+03    | 72.9   | 6.8850E+03    | -105.8 | 8.8707E+03    | -104.4 |
| 1.5500        | .0956               | 1.1405E+03    | 82.6   | 4.5732E+03    | -89.8  | 8.2865E+03    | -103.3 |
| 1.6000        | .0897               | 9.8321E+02    | 96.7   | 2.2330E+03    | -46.8  | 7.4953E+03    | -102.4 |
| 1.6500        | .0843               | 9.0207E+02    | 115.8  | 2.5378E+03    | 32.5   | 6.5549E+03    | -101.6 |
| 1.7000        | .0794               | 9.3699E+02    | 137.0  | 3.8942E+03    | 64.3   | 5.5176E+03    | -100.9 |
| 1.7500        | .0750               | 9.2142E+02    | 167.5  | 4.2058E+03    | 84.1   | 4.4477E+03    | -100.4 |
| 1.8000        | .0709               | 4.2305E+02    | -179.8 | 3.4209E+03    | 107.6  | 3.4035E+03    | -100.0 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                |                                     |
|---------------|---------------------|---------------------|----------------|-------------------------------------|
|               |                     | 105.00 DEGREES      | 120.00 DEGREES | 135.00 DEGREES                      |
| .2000         | 5.7398              | 6.5717E+02          | 74.5           | 5.1858E+02 61.0 3.4018E+02 45.3     |
| .2500         | 3.6735              | 7.2594E+02          | 79.3           | 6.5212E+02 81.7 5.8075E+02 82.5     |
| .3000         | 2.5510              | 1.2244E+03          | 83.5           | 1.2323E+03 84.2 1.2622E+03 86.0     |
| .3500         | 1.8742              | 1.8057E+03          | 84.5           | 2.1705E+03 86.6 2.5488E+03 88.3     |
| .4000         | 1.4349              | 2.5712E+03          | 86.1           | 3.7496E+03 88.0 4.8092E+03 88.1     |
| .4500         | 1.1338              | 3.6016E+03          | 87.9           | 6.1625E+03 87.5 8.1199E+03 85.5     |
| .5000         | .9184               | 4.9292E+03          | 89.1           | 9.3946E+03 85.2 1.2112E+04 82.1     |
| .5500         | .7590               | 6.5140E+03          | 89.2           | 1.3221E+04 82.2 1.6222E+04 79.0     |
| .6000         | .6376               | 8.3715E+03          | 88.3           | 1.7463E+04 79.3 1.9402E+04 77.9     |
| .6500         | .5434               | 1.0339E+04          | 86.1           | 2.1495E+04 77.9 2.0623E+04 78.8     |
| .7000         | .4686               | 1.2626E+04          | 83.7           | 2.4665E+04 78.1 1.9199E+04 81.1     |
| .7500         | .4082               | 1.5136E+04          | 82.2           | 2.6197E+04 79.6 1.5102E+04 84.3     |
| .8000         | .3587               | 1.7704E+04          | 81.4           | 2.5514E+04 81.6 9.3500E+03 88.1     |
| .8500         | .3178               | 2.0192E+04          | 81.7           | 2.2347E+04 84.1 3.4703E+03 96.4     |
| .9000         | .2834               | 2.2304E+04          | 82.4           | 1.7187E+04 86.2 1.2541E+03 -130.0   |
| .9500         | .2544               | 2.3655E+04          | 83.5           | 1.0757E+04 88.3 3.1472E+03 -115.5   |
| 1.0000        | .2296               | 2.4026E+04          | 84.7           | 4.3104E+03 92.1 3.0538E+03 -131.4   |
| 1.0500        | .2082               | 2.3306E+04          | 85.5           | 1.0644E+03 -123.7 2.3195E+03 -170.9 |
| 1.1000        | .1897               | 2.1304E+04          | 85.9           | 4.0687E+03 -107.3 2.1855E+03 139.9  |
| 1.1500        | .1736               | 1.8135E+04          | 85.6           | 4.8133E+03 -114.0 1.9780E+03 101.8  |
| 1.2000        | .1594               | 1.4049E+04          | 84.3           | 3.7724E+03 -130.1 1.1451E+03 63.1   |
| 1.2500        | .1469               | 9.4471E+03          | 80.8           | 2.1902E+03 -168.7 6.8244E+02 -40.9  |
| 1.3000        | .1359               | 4.8658E+03          | 71.6           | 2.0395E+03 121.1 1.1200E+03 -103.3  |
| 1.3500        | .1260               | 1.3836E+03          | 16.1           | 2.5813E+03 81.0 9.4116E+02 -153.6   |
| 1.4000        | .1171               | 3.0043E+03          | -74.5          | 2.2830E+03 50.8 8.4686E+02 136.2    |
| 1.4500        | .1092               | 4.3869E+03          | -90.2          | 1.4568E+03 4.2 7.7715E+02 84.1      |
| 1.5000        | .1020               | 5.5114E+03          | -99.9          | 1.2946E+03 -67.3 5.6706E+02 -30.1   |
| 1.5500        | .0956               | 4.9305E+03          | -110.7         | 2.1686E+03 -118.1 7.9393E+02 -82.9  |
| 1.6000        | .0897               | 3.5715E+03          | -125.9         | 1.1102E+03 155.5 6.4399E+02 -171.5  |
| 1.6500        | .0843               | 2.0116E+03          | -158.0         | 9.9567E+02 122.4 5.6819E+02 108.0   |
| 1.7000        | .0794               | 1.5802E+03          | 132.8          | 9.9130E+02 63.2 6.3573E+02 28.6     |
| 1.7500        | .0750               | 2.3309E+03          | 88.5           | 9.3946E+02 4.7 3.7913E+02 -49.3     |
| 1.8000        | .0709               | 2.7448E+03          | 65.1           | 7.0268E+02 -44.1 5.9698E+02 -135.6  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE   | WAVE/SHIP | 150.00 DEGREES |        | W A V E    | A N G L E |
|--------|-----------|----------------|--------|------------|-----------|
| FREQ.  | LENGTH    | AMPLITUDE      | PHASE  | AMPLITUDE  | DEGREES   |
| .2000  | 5.7398    | 1.7605E+02     | 39.1   | 7.4054E+01 | 43.3      |
| .2500  | 3.6735    | 4.5850E+02     | 83.4   | 2.5850E+02 | 84.2      |
| .3000  | 2.5510    | 1.0959E+03     | 87.4   | 6.5226E+02 | 88.3      |
| .3500  | 1.8742    | 2.3865E+03     | 89.0   | 1.4583E+03 | 89.2      |
| .4000  | 1.4349    | 4.5832E+03     | 87.5   | 2.7838E+03 | 86.9      |
| .4500  | 1.1338    | 7.5406E+03     | 84.0   | 4.4541E+03 | 83.0      |
| .5000  | .9184     | 1.0679E+04     | 80.1   | 6.0363E+03 | 79.7      |
| .5500  | .7590     | 1.3122E+04     | 78.5   | 6.8930E+03 | 78.6      |
| .6000  | .6378     | 1.3818E+04     | 78.9   | 6.5106E+03 | 80.2      |
| .6500  | .5434     | 1.2186E+04     | 81.4   | 4.8658E+03 | 83.6      |
| .7000  | .4686     | 8.5050E+03     | 85.2   | 2.4934E+03 | 89.6      |
| .7500  | .4082     | 3.9929E+03     | 91.5   | 4.2284E+02 | 124.4     |
| .8000  | .3587     | 5.4617E+02     | 159.3  | 8.7897E+02 | -117.2    |
| .8500  | .3178     | 1.8706E+03     | -116.7 | 9.6922E+02 | -132.4    |
| .9000  | .2834     | 1.9756E+03     | -132.6 | 8.5607E+02 | 179.7     |
| .9500  | .2544     | 1.6688E+03     | -176.9 | 9.3782E+02 | 138.5     |
| 1.0000 | .2296     | 1.7512E+03     | 139.2  | 6.6189E+02 | 111.6     |
| 1.0500 | .2082     | 1.3458E+03     | 108.7  | 1.3275E+02 | 64.2      |
| 1.1000 | .1897     | 4.4962E+02     | 65.5   | 3.5185E+02 | -99.5     |
| 1.1500 | .1736     | 5.8110E+02     | -85.1  | 4.0500E+02 | -140.4    |
| 1.2000 | .1594     | 8.0380E+02     | -126.2 | 3.5276E+02 | 150.7     |
| 1.2500 | .1469     | 6.3533E+02     | 168.1  | 1.7184E+02 | 97.7      |
| 1.3000 | .1359     | 5.1174E+02     | 109.6  | 1.0078E+04 | 131.8     |
| 1.3500 | .1260     | 1.8821E+02     | -52.7  | 2.2607E+02 | -103.3    |
| 1.4000 | .1171     | 6.0245E+02     | -85.7  | 2.4753E+02 | 148.7     |
| 1.4500 | .1092     | 5.2927E+02     | -164.5 | 1.4857E+02 | 37.3      |
| 1.5000 | .1020     | 4.3663E+02     | 107.4  | 2.7978E+02 | -51.1     |
| 1.5500 | .0956     | 4.5736E+02     | 1.9    | 3.1662E+02 | -141.4    |
| 1.6000 | .0897     | 4.3497E+02     | -84.5  | 1.5410E+02 | 100.9     |
| 1.6500 | .0843     | 4.9677E+02     | -153.2 | 2.4424E+02 | 79.8      |
| 1.7000 | .0794     | 4.9689E+02     | 70.7   | 6.2713E+02 | -95.6     |
| 1.7500 | .0750     | 3.2714E+02     | 124.0  | 1.6042E+03 | 33.3      |
| 1.8000 | .0709     | 1.2262E+03     | -84.2  | 7.9441E+03 | -7.1      |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 7.4411E+03          | .67931           | 925.8    |
| 4.879                | 1.5243E+04          | .67369           | 901.4    |
| 7.334                | 2.2194E+04          | .66671           | 863.9    |
| 10.497               | 3.1763E+04          | .66670           | 863.9    |
| 13.867               | 4.0310E+04          | .66413           | 842.8    |
| 17.894               | 5.2912E+04          | .66434           | 850.6    |
| 23.554               | 6.5916E+04          | .66312           | 828.8    |
| 28.835               | 7.6497E+04          | .66276           | 813.7    |
| 37.139               | 8.6367E+04          | .66411           | 787.8    |
| 47.602               | 1.0744E+05          | .66464           | 783.2    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN<br>24.0 HRS | 48.0 HRS   | 72.0 HRS   |
|----------------------|--------------------|------------|----------------------------------|------------|------------|
| 2.380                | .8771              | 3.1268E+04 | 3.3352E+04                       | 3.4633E+04 | 3.5341E+04 |
| 4.879                | .8792              | 6.3127E+04 | 6.7331E+04                       | 6.9913E+04 | 7.1344E+04 |
| 7.334                | .8819              | 8.9880E+04 | 9.5847E+04                       | 9.9507E+04 | 1.0154E+05 |
| 10.497               | .8819              | 1.2863E+05 | 1.3716E+05                       | 1.4240E+05 | 1.4532E+05 |
| 13.867               | .8829              | 1.6125E+05 | 1.7193E+05                       | 1.7847E+05 | 1.8213E+05 |
| 17.894               | .8826              | 2.1260E+05 | 2.2669E+05                       | 2.3532E+05 | 2.4014E+05 |
| 23.554               | .8833              | 2.6151E+05 | 2.7880E+05                       | 2.8939E+05 | 2.9531E+05 |
| 28.835               | .8834              | 3.0090E+05 | 3.2075E+05                       | 3.3293E+05 | 3.3972E+05 |
| 37.139               | .8829              | 3.3481E+05 | 3.5679E+05                       | 3.7030E+05 | 3.7782E+05 |
| 47.602               | .8827              | 4.1543E+05 | 4.4267E+05                       | 4.5941E+05 | 4.6875E+05 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM LATERAL BENDING MOMENT AT STATION 10 ( FEET -L.TONS)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 3.7822E+04        | 1.8511E-01                   | .73                    | 1.8511E+07        | 8.1489E+07 |
| 7.5644E+04        | 3.1794E-02                   | 1.50                   | 3.1794E+06        | 1.5331E+07 |
| 1.1347E+05        | 7.1405E-03                   | 2.15                   | 7.1405E+05        | 2.4653E+06 |
| 1.5129E+05        | 1.6902E-03                   | 2.77                   | 1.6902E+05        | 5.4503E+05 |
| 1.8911E+05        | 3.6178E-04                   | 3.44                   | 3.6178E+04        | 1.3285E+05 |
| 2.2693E+05        | 6.7096E-05                   | 4.17                   | 6.7096E+03        | 2.9468E+04 |
| 2.6476E+05        | 1.0841E-05                   | 4.96                   | 1.0841E+03        | 5.6255E+03 |
| 3.0258E+05        | 1.5739E-06                   | 5.80                   | 1.5739E+02        | 9.2668E+02 |
| 3.4040E+05        | 2.2010E-07                   | 6.66                   | 2.2010E+01        | 1.3538E+02 |
| 3.7822E+05        | 3.3027E-08                   | 7.48                   | 3.3027E+00        | 1.8708E+01 |
| 4.1604E+05        | 5.6822E-09                   | 8.25                   | 5.6822E-01        | 2.7345E+00 |
| 4.5387E+05        | 1.0610E-09                   | 8.97                   | 1.0610E-01        | 4.6213E-01 |
| 4.9169E+05        | 1.9448E-10                   | 9.71                   | 1.9448E-02        | 8.6649E-02 |
| 5.2951E+05        | 3.2870E-11                   | 10.48                  | 3.2870E-03        | 1.6161E-02 |
| 5.6733E+05        | 4.9917E-12                   | 11.30                  | 4.9917E-04        | 2.7879E-03 |
| 6.0516E+05        | 6.7489E-13                   | 12.17                  | 6.7489E-05        | 4.3168E-04 |
| 6.4298E+05        | 8.0972E-14                   | 13.09                  | 8.0972E-06        | 5.9392E-05 |
| 6.8080E+05        | 8.6095E-15                   | 14.07                  | 8.6095E-07        | 7.2363E-06 |
| 7.1862E+05        | 8.1069E-16                   | 15.09                  | 8.1069E-08        | 7.7988E-07 |
| 7.5644E+05        | 6.7574E-17                   | 16.17                  | 6.7574E-09        | 7.4312E-08 |
| 7.9427E+05        | 4.9845E-18                   | 17.30                  | 4.9845E-10        | 6.2590E-09 |
| 8.3209E+05        | 3.2528E-19                   | 18.49                  | 3.2528E-11        | 4.6592E-10 |
| 8.6991E+05        | 1.8776E-20                   | 19.73                  | 1.8776E-12        | 3.0650E-11 |
| 9.0773E+05        | 9.5850E-22                   | 21.02                  | 9.5850E-14        | 1.7818E-12 |
| 9.4556E+05        | 4.3267E-23                   | 22.36                  | 4.3267E-15        | 9.1524E-14 |
| 9.8338E+05        | 1.7268E-24                   | 23.76                  | 1.7268E-16        | 4.1540E-15 |
| 1.0212E+06        | 6.0927E-26                   | 25.22                  | 6.0927E-18        | 1.6659E-16 |
| 1.0590E+06        | 1.9003E-27                   | 26.72                  | 1.9003E-19        | 5.9027E-18 |
| 1.0968E+06        | 5.2388E-29                   | 28.28                  | 5.2388E-21        | 1.8479E-19 |
| 1.1347E+06        | 1.2765E-30                   | 29.89                  | 1.2765E-22        | 5.1111E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 2.1798E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 2.6634E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 3.1130E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 3.5613E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 4.0390E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 4.5519E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 5.0584E+05 (AMPLITUDE)

NL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE FREQ. | WAVE/SHIP LENGTH | W A V E       |               |               | A N G L E |            |           |
|------------|------------------|---------------|---------------|---------------|-----------|------------|-----------|
|            |                  | 15.00 DEGREES | 30.00 DEGREES | 45.00 DEGREES | AMPLITUDE | PHASE      | AMPLITUDE |
| .2000      | 5.7398           | 8.0427E+01    | 138.0         | 1.4445E+02    | 134.3     | 1.8138E+02 | 126.2     |
| .2500      | 3.6735           | 2.0397E+02    | 126.9         | 3.8745E+02    | 122.5     | 5.4435E+02 | 112.4     |
| .3000      | 2.5510           | 4.4208E+02    | 116.9         | 9.1516E+02    | 110.6     | 1.5566E+03 | 91.5      |
| .3500      | 1.8742           | 8.0876E+02    | 107.8         | 1.8852E+03    | 97.4      | 3.6832E+03 | 50.7      |
| .4000      | 1.4349           | 1.2200E+03    | 100.3         | 3.2198E+03    | 84.7      | 4.7069E+03 | 8.1       |
| .4500      | 1.1338           | 1.5001E+03    | 94.5          | 4.4545E+03    | 76.9      | 4.8034E+03 | -12.5     |
| .5000      | .9184            | 1.5201E+03    | 88.6          | 4.9189E+03    | 75.0      | 5.1023E+03 | -21.9     |
| .5500      | .7590            | 1.4608E+03    | 88.6          | 4.3771E+03    | 74.6      | 5.6621E+03 | -26.6     |
| .6000      | .6378            | 1.3789E+03    | 88.6          | 3.1679E+03    | 70.0      | 6.4566E+03 | -28.1     |
| .6500      | .5434            | 1.2742E+03    | 88.6          | 1.9058E+03    | 55.5      | 7.4164E+03 | -24.9     |
| .7000      | .4686            | 1.1469E+03    | 88.6          | 1.7924E+03    | 56.5      | 7.6339E+03 | -10.1     |
| .7500      | .4082            | 9.9679E+02    | 88.5          | 1.6558E+03    | 58.0      | 4.1477E+03 | 6.1       |
| .8000      | .3587            | 8.2399E+02    | 88.5          | 1.4970E+03    | 60.1      | 2.1559E+03 | -36.8     |
| .8500      | .3178            | 6.2848E+02    | 88.3          | 1.3177E+03    | 63.2      | 2.3590E+03 | -66.4     |
| .9000      | .2834            | 4.1027E+02    | 88.0          | 1.1211E+03    | 67.8      | 2.1963E+03 | -66.2     |
| .9500      | .2544            | 1.6938E+02    | 86.9          | 9.1433E+02    | 75.2      | 2.0094E+03 | -65.9     |
| 1.0000     | .2296            | 3.1462E+02    | -127.7        | 7.1464E+02    | 88.1      | 1.7983E+03 | -65.5     |
| 1.0500     | .2082            | 5.3762E+01    | -43.6         | 5.6739E+02    | 111.3     | 1.5632E+03 | -65.0     |
| 1.1000     | .1897            | 1.9166E+01    | -11.8         | 1.8335E+02    | -86.1     | 1.3041E+03 | -64.1     |
| 1.1500     | .1736            | 3.0384E+01    | -170.0        | 8.6730E+01    | 34.8      | 1.0214E+03 | -62.7     |
| 1.2000     | .1594            | 3.4100E+01    | 167.9         | 3.3673E+01    | 152.3     | 7.1585E+02 | -59.8     |
| 1.2500     | .1469            | 2.1427E+01    | 11.5          | 7.3060E+01    | 170.5     | 3.9157E+02 | -51.7     |
| 1.3000     | .1359            | 2.9667E+01    | -57.1         | 1.1387E+01    | 80.5      | 8.0450E+02 | 46.8      |
| 1.3500     | .1250            | 3.4073E+01    | -170.3        | 7.5979E+01    | -21.8     | 8.2291E+01 | 122.8     |
| 1.4000     | .1171            | 3.5703E+01    | 129.6         | 3.9295E+01    | -112.2    | 7.5150E+01 | -168.9    |
| 1.4500     | .1092            | 9.0951E+00    | -31.2         | 7.1052E+01    | 155.3     | 3.1461E+01 | -20.5     |
| 1.5000     | .1020            | 1.6909E+01    | -124.4        | 3.4566E+01    | 92.2      | 8.8135E+01 | -27.6     |
| 1.5500     | .0956            | 1.5868E+01    | 107.7         | 3.7459E+01    | -58.9     | 3.5034E+01 | -94.4     |
| 1.6000     | .0897            | 1.6797E+01    | -11.3         | 2.0304E+01    | -164.0    | 7.4700E+01 | 152.5     |
| 1.6500     | .0843            | 2.7181E+00    | 46.1          | 2.7870E+01    | 96.6      | 3.5783E+01 | 94.7      |
| 1.7000     | .0794            | 1.5533E+01    | 97.6          | 2.5456E+01    | -50.0     | 5.1398E+01 | -35.5     |
| 1.7500     | .0750            | 2.0448E+01    | -96.9         | 2.4646E+00    | 24.2      | 2.8652E+01 | -82.7     |
| 1.8000     | .0709            | 1.6207E+01    | -13.3         | 2.6762E+01    | 90.2      | 3.9602E+01 | 119.0     |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |       | 75.00 DEGREES |        | 90.00 DEGREES |        |
|---------------|---------------------|---------------------|-------|---------------|--------|---------------|--------|
|               |                     | 60.00 DEGREES       | PHASE | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  |
| .2000         | 5.7398              | 1.9416E+02          | 110.3 | 2.1276E+02    | 81.9   | 2.9823E+02    | 43.6   |
| .2500         | 3.6775              | 7.1864E+02          | 90.1  | 1.0849E+03    | 41.0   | 1.2690E+03    | -37.0  |
| .3000         | 2.5510              | 2.2901E+03          | 29.1  | 1.2475E+03    | -45.5  | 7.9433E+02    | -81.1  |
| .3500         | 1.8742              | 1.9742E+03          | -26.2 | 9.4989E+02    | -64.2  | 7.1826E+02    | -87.5  |
| .4000         | 1.4349              | 1.6540E+03          | -40.6 | 8.8039E+02    | -70.0  | 7.3981E+02    | -89.1  |
| .4500         | 1.1338              | 1.5458E+03          | -45.1 | 8.5831E+02    | -72.7  | 7.9418E+02    | -89.3  |
| .5000         | .9184               | 1.4915E+03          | -45.5 | 8.3400E+02    | -73.8  | 8.6483E+02    | -89.1  |
| .5500         | .7590               | 1.4440E+03          | -43.0 | 7.8696E+02    | -73.5  | 9.4397E+02    | -88.6  |
| .6000         | .6378               | 1.3945E+03          | -37.8 | 7.0558E+02    | -71.4  | 1.0370E+03    | -88.3  |
| .6500         | .5434               | 1.3540E+03          | -30.1 | 5.8938E+02    | -65.6  | 1.1278E+03    | -88.2  |
| .7000         | .4686               | 1.3314E+03          | -21.0 | 4.6005E+02    | -51.3  | 1.2242E+03    | -88.4  |
| .7500         | .4082               | 1.3172E+03          | -11.6 | 3.8458E+02    | -20.7  | 1.2960E+03    | -89.1  |
| .8000         | .3587               | 1.2725E+03          | -2.7  | 4.7757E+02    | 13.3   | 1.3571E+03    | -90.0  |
| .8500         | .3178               | 1.1535E+03          | 7.2   | 7.0371E+02    | 31.2   | 1.4027E+03    | -91.0  |
| .9000         | .2834               | 9.5434E+02          | 22.5  | 9.6983E+02    | 38.1   | 1.4203E+03    | -92.4  |
| .9500         | .2544               | 7.9294E+02          | 53.0  | 1.2183E+03    | 40.2   | 1.4119E+03    | -93.8  |
| 1.0000        | .2296               | 9.5722E+02          | 92.1  | 1.4119E+03    | 39.8   | 1.3820E+03    | -95.2  |
| 1.0500        | .2082               | 1.4340E+03          | 114.7 | 1.5229E+03    | 37.9   | 1.3287E+03    | -96.8  |
| 1.1000        | .1897               | 1.9493E+03          | 126.2 | 1.5335E+03    | 34.7   | 1.2560E+03    | -98.5  |
| 1.1500        | .1736               | 2.2457E+03          | 137.0 | 1.4368E+03    | 30.2   | 1.1662E+03    | -100.4 |
| 1.2000        | .1594               | 1.6900E+03          | 162.7 | 1.2440E+03    | 24.0   | 1.0656E+03    | -102.3 |
| 1.2500        | .1469               | 1.2646E+03          | 66.1  | 9.8461E+02    | 14.9   | 9.5724E+02    | -104.3 |
| 1.3000        | .1359               | 1.6411E+03          | 89.2  | 7.0591E+02    | .4     | 8.4534E+02    | -106.4 |
| 1.3500        | .1260               | 1.5324E+03          | 89.7  | 4.7332E+02    | -25.4  | 7.3409E+02    | -108.5 |
| 1.4000        | .1171               | 1.4142E+03          | 90.2  | 3.7398E+02    | -65.7  | 6.3021E+02    | -111.0 |
| 1.4500        | .1092               | 1.2865E+03          | 91.0  | 3.9962E+02    | -101.2 | 5.3166E+02    | -113.4 |
| 1.5000        | .1020               | 1.1495E+03          | 92.0  | 4.3465E+02    | -123.5 | 4.4256E+02    | -115.8 |
| 1.5500        | .0956               | 1.0034E+03          | 93.4  | 4.1839E+02    | -131.9 | 3.6414E+02    | -118.1 |
| 1.6000        | .0897               | 8.4854E+02          | 95.3  | 3.4632E+02    | -156.0 | 2.9645E+02    | -120.2 |
| 1.6500        | .0843               | 6.8577E+02          | 98.4  | 2.4736E+02    | -177.3 | 2.3928E+02    | -122.0 |
| 1.7000        | .0794               | 5.1707E+02          | 103.7 | 1.6585E+02    | 147.1  | 1.9191E+02    | -123.4 |
| 1.7500        | .0750               | 2.3308E+02          | 175.4 | 1.5040E+02    | 99.3   | 1.5314E+02    | -124.4 |
| 1.8000        | .0709               | 6.6056E+01          | 55.0  | 1.7529E+02    | 66.9   | 1.2197E+02    | -124.7 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                |                   |
|---------------|---------------------|---------------------|----------------|-------------------|
|               |                     | 105.00 DEGREES      | 120.00 DEGREES | 135.00 DEGREES    |
| .2000         | 5.7398              | 4.7991E+02          | 21.8           | 7.1785E+02 -3.6   |
| .2500         | 3.6735              | 8.9787E+02          | -81.7          | 6.4700E+02 -98.4  |
| .3000         | 2.5510              | 6.3312E+02          | -96.8          | 5.0624E+02 -103.1 |
| .3500         | 1.8742              | 6.1474E+02          | -97.1          | 4.8461E+02 -101.0 |
| .4000         | 1.4349              | 6.4120E+02          | -95.2          | 4.5279E+02 -98.1  |
| .4500         | 1.1338              | 6.7024E+02          | -92.3          | 3.7453E+02 -95.0  |
| .5000         | .9184               | 6.8878E+02          | -88.9          | 2.0278E+02 -86.2  |
| .5500         | .7590               | 6.7353E+02          | -84.2          | 7.6713E+01 44.8   |
| .6000         | .6378               | 6.2696E+02          | -76.9          | 3.6409E+02 79.1   |
| .6500         | .5434               | 5.2937E+02          | -68.0          | 6.8621E+02 87.2   |
| .7000         | .4686               | 4.2494E+02          | -53.7          | 9.8101E+02 96.0   |
| .7500         | .4082               | 3.2851E+02          | -23.8          | 1.2101E+03 106.3  |
| .8000         | .3587               | 3.3169E+02          | 19.7           | 1.3621E+03 118.2  |
| .8500         | .3178               | 4.6840E+02          | 52.5           | 1.4318E+03 131.3  |
| .9000         | .2834               | 6.4400E+02          | 71.7           | 1.4127E+03 144.7  |
| .9500         | .2544               | 8.2025E+02          | 85.0           | 1.2801E+03 158.1  |
| 1.0000        | .2296               | 9.6167E+02          | 96.2           | 1.0250E+03 172.0  |
| 1.0500        | .2082               | 1.0610E+03          | 106.0          | 6.8368E+02 -170.1 |
| 1.1000        | .1897               | 1.1038E+03          | 115.9          | 3.7342E+02 -134.9 |
| 1.1500        | .1736               | 1.0900E+03          | 125.8          | 3.1701E+02 -71.9  |
| 1.2000        | .1594               | 1.0179E+03          | 136.2          | 4.0896E+02 -39.5  |
| 1.2500        | .1469               | 3.9611E+02          | 147.5          | 3.9069E+02 -27.8  |
| 1.3000        | .1359               | 7.4102E+02          | 160.7          | 2.4900E+02 -23.0  |
| 1.3500        | .1260               | 5.7460E+02          | 177.0          | 4.8300E+01 -24.2  |
| 1.4000        | .1171               | 4.2580E+02          | -161.4         | 1.2074E+02 163.8  |
| 1.4500        | .1092               | 3.1974E+02          | -132.9         | 1.8272E+02 164.2  |
| 1.5000        | .1020               | 2.6574E+02          | -100.0         | 1.2143E+02 165.7  |
| 1.5500        | .0956               | 2.4393E+02          | -69.3          | 3.2067E+01 56.5   |
| 1.6000        | .0897               | 2.2396E+02          | -42.4          | 8.2348E+01 -5.3   |
| 1.6500        | .0843               | 1.9821E+02          | -17.3          | 9.9835E+01 -6.0   |
| 1.7000        | .0794               | 1.6822E+02          | 8.6            | 1.8045E+01 73.3   |
| 1.7500        | .0750               | 1.3938E+02          | 36.5           | 7.4110E+01 164.8  |
| 1.8000        | .0709               | 1.1664E+02          | 67.0           | 5.8318E+01 172.3  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS/ FEET )

| WAVE   | WAVE/SHIP | 150.00 DEGREES | W A V E | A N G L E  |        |
|--------|-----------|----------------|---------|------------|--------|
| FREQ.  | LENGTH    | AMPLITUDE      | PHASE   | AMPLITUDE  | PHASE  |
| .2000  | 5.7398    | 6.3635E+02     | -56.9   | 3.1958E+02 | -70.5  |
| .2500  | 3.6735    | 2.9934E+02     | -108.3  | 1.4732E+02 | -109.7 |
| .3000  | 2.5510    | 2.4228E+02     | -107.9  | 1.1740E+02 | -109.3 |
| .3500  | 1.8742    | 1.8838E+02     | -109.2  | 8.1287E+01 | -114.7 |
| .4000  | 1.4349    | 9.1173E+01     | -131.7  | 3.5574E+01 | 174.2  |
| .4500  | 1.1338    | 1.4895E+02     | 112.1   | 1.3213E+02 | 107.7  |
| .5000  | .9184     | 3.9910E+02     | 102.5   | 2.6091E+02 | 104.6  |
| .5500  | .7590     | 6.1754E+02     | 105.0   | 3.6098E+02 | 109.2  |
| .6000  | .6378     | 7.5718E+02     | 112.9   | 4.0497E+02 | 121.0  |
| .6500  | .5434     | 8.0060E+02     | 127.2   | 3.9152E+02 | 139.2  |
| .7000  | .4686     | 7.6165E+02     | 145.4   | 3.3844E+02 | 160.3  |
| .7500  | .4082     | 6.4711E+02     | 165.3   | 2.4538E+02 | -175.9 |
| .8000  | .3587     | 4.4988E+02     | -172.0  | 1.3514E+02 | -137.4 |
| .8500  | .3178     | 2.4091E+02     | -131.3  | 1.1600E+02 | -71.0  |
| .9000  | .2834     | 2.2710E+02     | -66.1   | 1.4685E+02 | -48.1  |
| .9500  | .2544     | 2.8299E+02     | -45.7   | 1.3207E+02 | -57.9  |
| 1.0000 | .2296     | 2.4598E+02     | -54.2   | 1.0147E+02 | -92.0  |
| 1.0500 | .2082     | 1.7548E+02     | -89.3   | 8.8946E+01 | -128.8 |
| 1.1000 | .1897     | 1.5813E+02     | -131.4  | 5.1514E+01 | -139.7 |
| 1.1500 | .1736     | 1.0995E+02     | -148.1  | 2.6898E+01 | -24.0  |
| 1.2000 | .1594     | 2.7202E+01     | -45.1   | 4.8858E+01 | -7.4   |
| 1.2500 | .1469     | 9.3637E+01     | -2.2    | 2.4711E+01 | -77.3  |
| 1.3000 | .1359     | 4.2824E+01     | -28.2   | 6.8314E+02 | -46.1  |
| 1.3500 | .1260     | 6.8384E+01     | -140.2  | 1.5947E+01 | -20.2  |
| 1.4000 | .1171     | 3.9281E+01     | -107.9  | 2.9061E+01 | 65.2   |
| 1.4500 | .1092     | 4.3517E+01     | 45.9    | 2.6477E+00 | 13.7   |
| 1.5000 | .1020     | 3.1756E+01     | 71.2    | 1.8165E+01 | -36.3  |
| 1.5500 | .0956     | 2.7436E+01     | -92.0   | 9.1586E+00 | 110.3  |
| 1.6000 | .0897     | 1.6649E+01     | 5.2     | 1.3214E+01 | -138.4 |
| 1.6500 | .0843     | 1.3021E+01     | 140.3   | 1.2509E+01 | 53.2   |
| 1.7000 | .0794     | 2.2055E+01     | -95.7   | 1.2978E+01 | -154.6 |
| 1.7500 | .0750     | 1.0659E+02     | 10.4    | 3.9294E+01 | 3.0    |
| 1.8000 | .0709     | 1.7025E+01     | -129.3  | 1.5832E+02 | -3.6   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 8.8217E+02          | .74482           | 783.3    |
| 4.879                | 1.9093E+03          | .73675           | 753.6    |
| 7.334                | 3.0579E+03          | .72358           | 708.8    |
| 10.497               | 4.3771E+03          | .72356           | 708.7    |
| 13.867               | 5.9120E+03          | .71617           | 682.9    |
| 17.894               | 7.5769E+03          | .71885           | 692.5    |
| 23.554               | 1.0120E+04          | .71152           | 665.1    |
| 28.835               | 1.2397E+04          | .70706           | 644.7    |
| 37.139               | 1.5589E+04          | .70197           | 604.0    |
| 47.602               | 1.9811E+04          | .70163           | 595.6    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8501              | 4.3441E+03 | 4.6702E+03           | 4.8686E+03 | 4.9811E+03 |
| 4.879                | .8536              | 9.7757E+03 | 1.0517E+04           | 1.0966E+04 | 1.1221E+04 |
| 7.334                | .8592              | 1.6569E+04 | 1.7836E+04           | 1.8599E+04 | 1.9033E+04 |
| 10.497               | .8592              | 2.3719E+04 | 2.5533E+04           | 2.6625E+04 | 2.7246E+04 |
| 13.867               | .8623              | 3.2985E+04 | 3.5515E+04           | 3.7031E+04 | 3.7896E+04 |
| 17.894               | .8612              | 4.1836E+04 | 4.5042E+04           | 4.6966E+04 | 4.8062E+04 |
| 23.554               | .8642              | 5.7464E+04 | 6.1879E+04           | 6.4515E+04 | 6.6023E+04 |
| 28.835               | .8660              | 7.1554E+04 | 7.7059E+04           | 8.0336E+04 | 8.2214E+04 |
| 37.139               | .8681              | 9.1724E+04 | 9.8792E+04           | 1.0298E+05 | 1.0539E+05 |
| 47.602               | .8682              | 1.1576E+05 | 1.2575E+05           | 1.3108E+05 | 1.3415E+05 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM TORSIONAL MOMENT AT STATION 10 ( FEET -L.TONS)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 1.1533E+04        | 3.6876E-02                   | 1.43                   | 3.6876E+06        | 9.6312E+07 |
| 2.3065E+04        | 4.8012E-03                   | 2.32                   | 4.8012E+05        | 3.2075E+06 |
| 3.4598E+04        | 8.8152E-04                   | 3.05                   | 8.8152E+04        | 3.9197E+05 |
| 4.6130E+04        | 1.5535E-04                   | 3.81                   | 1.5535E+04        | 7.2618E+04 |
| 5.7663E+04        | 2.4345E-05                   | 4.61                   | 2.4345E+03        | 1.3100E+04 |
| 6.9196E+04        | 3.6358E-06                   | 5.44                   | 3.6358E+02        | 2.0709E+03 |
| 8.0728E+04        | 6.0064E-07                   | 6.22                   | 6.0064E+01        | 3.0352E+02 |
| 9.2261E+04        | 1.2545E-07                   | 6.90                   | 1.2545E+01        | 4.7518E+01 |
| 1.0379E+05        | 3.0959E-08                   | 7.51                   | 3.0959E+00        | 9.4495E+00 |
| 1.1533E+05        | 7.7662E-09                   | 8.11                   | 7.7662E-01        | 2.3193E+00 |
| 1.2686E+05        | 1.8265E-09                   | 8.74                   | 1.8265E-01        | 5.9398E-01 |
| 1.3839E+05        | 3.9064E-10                   | 9.41                   | 3.9064E-02        | 1.4358E-01 |
| 1.4992E+05        | 7.5004E-11                   | 10.12                  | 7.5004E-03        | 3.1563E-02 |
| 1.6146E+05        | 1.2844E-11                   | 10.89                  | 1.2844E-03        | 6.2160E-03 |
| 1.7299E+05        | 1.9548E-12                   | 11.71                  | 1.9548E-04        | 1.0889E-03 |
| 1.8452E+05        | 2.6394E-13                   | 12.58                  | 2.6394E-05        | 1.6909E-04 |
| 1.9605E+05        | 3.1582E-14                   | 13.50                  | 3.1582E-06        | 2.3236E-05 |
| 2.0759E+05        | 3.3470E-15                   | 14.48                  | 3.3470E-07        | 2.8235E-06 |
| 2.1912E+05        | 3.1406E-16                   | 15.50                  | 3.1406E-08        | 3.0330E-07 |
| 2.3065E+05        | 2.6087E-17                   | 16.58                  | 2.6087E-09        | 2.8798E-08 |
| 2.4218E+05        | 1.9179E-18                   | 17.72                  | 1.9179E-10        | 2.4169E-09 |
| 2.5372E+05        | 1.2480E-19                   | 18.90                  | 1.2480E-11        | 1.7931E-10 |
| 2.6525E+05        | 7.1883E-21                   | 20.14                  | 7.1883E-13        | 1.1761E-11 |
| 2.7678E+05        | 3.6650E-22                   | 21.44                  | 3.6650E-14        | 6.8218E-13 |
| 2.8831E+05        | 1.6542E-23                   | 22.78                  | 1.6542E-15        | 3.4996E-14 |
| 2.9985E+05        | 6.6099E-25                   | 24.18                  | 6.6099E-17        | 1.5881E-15 |
| 3.1138E+05        | 2.3382E-26                   | 25.63                  | 2.3382E-18        | 6.3761E-17 |
| 3.2291E+05        | 7.3223E-28                   | 27.14                  | 7.3223E-20        | 2.2650E-18 |
| 3.3445E+05        | 2.0297E-29                   | 28.69                  | 2.0297E-21        | 7.1193E-20 |
| 3.4598E+05        | 4.9794E-31                   | 30.30                  | 4.9794E-23        | 1.9799E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 4.8871E+04 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 5 CYCLES = 6.3059E+04 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 6 CYCLES = 7.7463E+04 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 7 CYCLES = 9.4130E+04 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 8 CYCLES = 1.1322E+05 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\* 9 CYCLES = 1.3136E+05 (AMPLITUDE)

MAXIMUM VALUE IN 10\*\*10 CYCLES = 1.4791E+05 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                 | 15.00 DEGREES   |                 | 30.00 DEGREES   |                 |
|---------------|---------------------|---------------------|-----------------|-----------------|-----------------|-----------------|-----------------|
|               |                     | 0.00 DEGREES        | AMPLITUDE PHASE |
| .2000         | 5.7398              | 3.6104E+00          | -66.2           | 3.4308E+00      | -65.6           | 2.9381E+00      | -63.4           |
| .2500         | 3.6735              | 6.9318E+00          | -63.7           | 6.5041E+00      | -63.5           | 5.3468E+00      | -62.1           |
| .3000         | 2.5510              | 1.3413E+01          | -59.9           | 1.2468E+01      | -60.0           | 9.9378E+00      | -59.7           |
| .3500         | 1.8742              | 2.5257E+01          | -55.5           | 2.3414E+01      | -55.9           | 1.8504E+01      | -56.7           |
| .4000         | 1.4349              | 4.4597E+01          | -50.6           | 4.1450E+01      | -51.3           | 3.2777E+01      | -53.1           |
| .4500         | 1.1338              | 7.2351E+01          | -44.8           | 6.7520E+01      | -46.0           | 5.4204E+01      | -49.0           |
| .5000         | .9184               | 1.0722E+02          | -37.7           | 1.0076E+02      | -39.5           | 8.2734E+01      | -44.1           |
| .5500         | .7590               | 9.9196E+01          | -35.8           | 9.3240E+01      | -37.2           | 1.1620E+02      | -38.0           |
| .6000         | .6378               | 8.8592E+01          | -32.6           | 8.3159E+01      | -33.2           | 1.4955E+02      | -30.6           |
| .6500         | .5434               | 7.5751E+01          | -27.4           | 7.1062E+01      | -26.4           | 1.8090E+02      | -21.8           |
| .7000         | .4686               | 6.1478E+01          | -18.4           | 5.8245E+01      | -14.7           | 1.6620E+02      | -19.9           |
| .7500         | .4082               | 4.7940E+01          | -1.5            | 4.8000E+01      | 6.0             | 1.4869E+02      | -16.9           |
| .8000         | .3587               | 4.0940E+01          | 28.4            | 4.6997E+01      | 36.4            | 1.2875E+02      | -12.5           |
| .8500         | .3178               | 4.8475E+01          | 62.3            | 5.9963E+01      | 63.6            | 1.0716E+02      | -5.4            |
| .9000         | .2834               | 6.9368E+01          | 83.7            | 8.3770E+01      | 80.3            | 8.5765E+01      | 6.6             |
| .9500         | .2544               | 9.8032E+01          | 95.2            | 1.1442E+02      | 89.8            | 6.9206E+01      | 27.8            |
| 1.0000        | .2296               | 5.9143E+01          | 97.8            | 7.3369E+01      | 95.1            | 6.6699E+01      | 58.5            |
| 1.0500        | .2082               | 3.6241E+01          | 84.9            | 4.2827E+01      | 88.8            | 8.4062E+01      | 86.0            |
| 1.1000        | .1897               | 3.1523E+01          | 72.0            | 3.2805E+01      | 72.8            | 4.9085E+01      | 83.3            |
| 1.1500        | .1736               | 2.4889E+01          | 75.2            | 2.8471E+01      | 71.0            | 3.3966E+01      | 69.8            |
| 1.2000        | .1594               | 1.2124E+01          | 74.9            | 1.7522E+01      | 75.8            | 2.8699E+01      | 65.0            |
| 1.2500        | .1469               | 5.8502E+00          | 13.2            | 6.2114E+00      | 50.6            | 1.9889E+01      | 69.9            |
| 1.3000        | .1359               | 6.6277E+00          | 3.1             | 6.5241E+00      | 2.1             | 8.7861E+00      | 67.5            |
| 1.3500        | .1260               | 4.3753E+00          | 2.2             | 5.0164E+00      | 2.2             | 4.4439E+00      | 13.8            |
| 1.4000        | .1171               | 2.3317E+00          | -6.0            | 2.9349E+00      | 3.6             | 4.7875E+00      | 1.8             |
| 1.4500        | .1092               | 1.1697E+00          | -102.2          | 9.7563E-01      | -19.1           | 2.5712E+00      | 2.7             |
| 1.5000        | .1020               | 1.2154E+00          | -102.8          | 1.5453E+00      | -119.6          | 1.3517E+00      | 12.6            |
| 1.5500        | .0956               | 2.4930E+00          | 53.8            | 6.9857E-01      | -40.9           | 3.0900E-01      | 109.1           |
| 1.6000        | .0897               | 5.7123E+00          | 92.1            | 3.6366E+00      | 66.5            | 1.4866E+00      | -135.4          |
| 1.6500        | .0843               | 4.4017E+00          | 112.6           | 4.9717E+00      | 108.2           | 1.1511E+00      | -47.6           |
| 1.7000        | .0794               | 5.7800E+00          | 40.0            | 1.5785E+00      | 108.4           | 2.6064E+00      | 52.1            |
| 1.7500        | .0750               | 1.2167E+01          | 59.5            | 6.9160E+00      | 34.9            | 3.0329E+00      | 125.0           |
| 1.8000        | .0709               | 6.6192E+00          | 75.3            | 9.3818E+00      | 74.5            | 2.3647E+00      | -133.8          |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | 45.00 DEGREES |        | 60.00 DEGREES |        | 75.00 DEGREES |        |
|---------------|---------------------|---------------|--------|---------------|--------|---------------|--------|
|               |                     | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  |
| .2000         | 5.7398              | 2.2614E+00    | -57.9  | 1.5958E+00    | -44.9  | 1.1827E+00    | -19.2  |
| .2500         | 3.6735              | 3.8100E+00    | -57.5  | 2.4074E+00    | -43.2  | 1.7242E+00    | -12.1  |
| .3000         | 2.5510              | 6.6205E+00    | -56.8  | 3.5867E+00    | -43.0  | 2.3461E+00    | -4.9   |
| .3500         | 1.8742              | 1.1705E+01    | -55.8  | 5.5013E+00    | -44.5  | 3.0523E+00    | 1.6    |
| .4000         | 1.4349              | 2.0433E+01    | -54.3  | 8.7475E+00    | -47.0  | 3.8185E+00    | 6.7    |
| .4500         | 1.1338              | 3.4164E+01    | -52.1  | 1.4079E+01    | -49.1  | 4.6015E+00    | 9.7    |
| .5000         | .9184               | 5.3736E+01    | -49.2  | 2.2260E+01    | -50.1  | 5.3509E+00    | 10.4   |
| .5500         | .7590               | 7.8866E+01    | -45.5  | 3.3909E+01    | -50.0  | 6.0470E+00    | 8.0    |
| .6000         | .6378               | 1.0778E+02    | -40.9  | 4.9187E+01    | -48.7  | 6.7678E+00    | 2.2    |
| .6500         | .5434               | 1.3710E+02    | -35.4  | 6.7600E+01    | -46.4  | 7.7444E+00    | -6.7   |
| .7000         | .4686               | 1.6264E+02    | -29.0  | 8.7816E+01    | -43.3  | 9.3350E+00    | -17.0  |
| .7500         | .4082               | 1.8043E+02    | -22.1  | 1.0769E+02    | -39.5  | 1.1855E+01    | -25.0  |
| .8000         | .3587               | 1.8802E+02    | -15.1  | 1.2449E+02    | -35.0  | 1.5416E+01    | -32.0  |
| .8500         | .3178               | 1.8497E+02    | -8.7   | 1.3538E+02    | -30.1  | 1.9918E+01    | -34.9  |
| .9000         | .2834               | 1.7053E+02    | -7.9   | 1.3799E+02    | -24.9  | 2.5167E+01    | -35.4  |
| .9500         | .2544               | 1.5401E+02    | -6.7   | 1.3113E+02    | -20.1  | 3.0625E+01    | -34.1  |
| 1.0000        | .2296               | 1.3544E+02    | -5.0   | 1.1549E+02    | -16.3  | 3.5838E+01    | -31.5  |
| 1.0500        | .2082               | 1.1492E+02    | -2.5   | 9.4076E+01    | -14.9  | 4.0055E+01    | -28.1  |
| 1.1000        | .1897               | 9.2661E+01    | 1.5    | 7.2163E+01    | -18.0  | 4.2820E+01    | -23.9  |
| 1.1500        | .1736               | 6.9206E+01    | 8.8    | 5.6016E+01    | -26.4  | 4.3227E+01    | -19.2  |
| 1.2000        | .1594               | 4.6388E+01    | 24.9   | 4.7766E+01    | -35.2  | 4.0806E+01    | -13.9  |
| 1.2500        | .1469               | 3.2205E+01    | 64.8   | 4.2270E+01    | -36.2  | 3.5337E+01    | -7.8   |
| 1.3000        | .1359               | 2.3576E+01    | 53.0   | 3.3945E+01    | -26.5  | 2.6999E+01    | -.6    |
| 1.3500        | .1260               | 1.8035E+01    | 55.4   | 3.0152E+01    | -27.3  | 1.6642E+01    | 9.6    |
| 1.4000        | .1171               | 1.0180E+01    | 66.0   | 2.6032E+01    | -28.6  | 5.9535E+00    | 36.8   |
| 1.4500        | .1092               | 3.1958E+00    | 67.4   | 2.1596E+01    | -30.5  | 6.2303E+00    | 162.3  |
| 1.5000        | .1020               | 1.3526E+00    | -14.9  | 1.6865E+01    | -33.6  | 1.3646E+01    | -171.8 |
| 1.5500        | .0956               | 1.2590E+00    | -20.8  | 1.1905E+01    | -39.7  | 1.7681E+01    | -158.0 |
| 1.6000        | .0897               | 3.4880E-01    | -34.7  | 6.9872E+00    | -55.6  | 1.7507E+01    | -144.6 |
| 1.6500        | .0843               | 3.3914E-01    | 35.2   | 4.1213E+00    | -112.5 | 1.3585E+01    | -127.0 |
| 1.7000        | .0794               | 9.4914E-01    | 69.9   | 7.6275E+00    | -166.8 | 7.7974E+00    | -94.4  |
| 1.7500        | .0750               | 1.1699E+00    | 143.0  | 6.5218E+00    | -136.5 | 5.5952E+00    | -15.3  |
| 1.8000        | .0709               | 1.7351E+00    | -135.1 | 2.6484E+00    | -98.3  | 9.4117E+00    | 39.4   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE VERTICAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>PERIOD | WAVE/SHIP<br>LENGTH | 90.00 DEGREES |        | 105.00 DEGREES |        | 120.00 DEGREES |        |
|----------------|---------------------|---------------|--------|----------------|--------|----------------|--------|
|                |                     | AMPLITUDE     | PHASE  | AMPLITUDE      | PHASE  | AMPLITUDE      | PHASE  |
| .2000          | 5.7398              | 1.1645E+00    | 10.5   | 1.3225E+00     | 30.2   | 1.4699E+00     | 42.0   |
| .2500          | 3.6735              | 1.8392E+00    | 13.9   | 2.0348E+00     | 22.8   | 1.9800E+00     | 25.7   |
| .3000          | 2.5510              | 2.7023E+00    | 15.7   | 2.9219E+00     | 10.2   | 2.6249E+00     | -4.9   |
| .3500          | 1.8742              | 3.7276E+00    | 16.2   | 4.1606E+00     | -7.4   | 4.4332E+00     | -42.5  |
| .4000          | 1.4349              | 4.8589E+00    | 15.3   | 6.2115E+00     | -28.1  | 8.8676E+00     | -70.6  |
| .4500          | 1.1338              | 5.9947E+00    | 13.1   | 9.8288E+00     | -48.4  | 1.7418E+01     | -90.1  |
| .5000          | .9184               | 6.9897E+00    | 9.3    | 1.5989E+01     | -64.8  | 3.2831E+01     | -106.1 |
| .5500          | .7590               | 7.6460E+00    | 3.6    | 2.6258E+01     | -82.8  | 6.0863E+01     | -127.6 |
| .6000          | .6378               | 7.7092E+00    | -5.1   | 4.1744E+01     | -101.7 | 9.9207E+01     | -162.1 |
| .6500          | .5434               | 6.9646E+00    | -21.5  | 6.4866E+01     | -128.3 | 9.7562E+01     | 161.0  |
| .7000          | .4686               | 5.2520E+00    | -52.3  | 7.6103E+01     | -165.5 | 7.6675E+01     | 146.6  |
| .7500          | .4082               | 5.7535E+00    | -125.5 | 5.8992E+01     | 164.2  | 6.4774E+01     | 144.8  |
| .8000          | .3587               | 1.3015E+01    | -178.0 | 3.8498E+01     | 152.0  | 5.7368E+01     | 144.9  |
| .8500          | .3178               | 2.1776E+01    | 146.9  | 2.5288E+01     | 155.2  | 4.8683E+01     | 142.6  |
| .9000          | .2834               | 2.8019E+01    | 117.4  | 1.8156E+01     | 174.9  | 3.4608E+01     | 137.5  |
| .9500          | .2544               | 2.8469E+01    | 97.5   | 1.7160E+01     | -168.0 | 1.5806E+01     | 126.6  |
| 1.0000         | .2296               | 2.6251E+01    | 85.4   | 1.7103E+01     | -156.2 | 6.0749E+00     | -18.9  |
| 1.0500         | .2082               | 2.3388E+01    | 78.1   | 1.5713E+01     | -151.0 | 2.3854E+01     | -47.1  |
| 1.1000         | .1897               | 1.9810E+01    | 74.6   | 1.2988E+01     | -145.6 | 3.5329E+01     | -56.6  |
| 1.1500         | .1736               | 1.6071E+01    | 74.4   | 9.1997E+00     | -136.7 | 3.7274E+01     | -64.6  |
| 1.2000         | .1594               | 1.2774E+01    | 76.7   | 5.5726E+00     | -112.8 | 3.0163E+01     | -72.0  |
| 1.2500         | .1469               | 9.7328E+00    | 83.0   | 4.6754E+00     | -63.6  | 1.7293E+01     | -77.2  |
| 1.3000         | .1359               | 7.4027E+00    | 93.5   | 6.3643E+00     | -33.8  | 4.5910E+00     | -55.4  |
| 1.3500         | .1260               | 5.7766E+00    | 109.1  | 7.2636E+00     | -24.1  | 6.6971E+00     | 42.7   |
| 1.4000         | .1171               | 4.8536E+00    | 128.7  | 6.4920E+00     | -21.1  | 8.9960E+00     | 36.0   |
| 1.4500         | .1092               | 4.4994E+00    | 146.4  | 3.8896E+00     | -18.7  | 6.0840E+00     | 6.5    |
| 1.5000         | .1020               | 4.2832E+00    | 160.1  | 4.8932E-01     | 53.9   | 3.7980E+00     | -75.1  |
| 1.5500         | .0956               | 3.9516E+00    | 170.2  | 4.1803E+00     | 141.4  | 5.7750E+00     | -141.4 |
| 1.6000         | .0897               | 3.4222E+00    | 178.2  | 7.6734E+00     | 140.0  | 6.1261E+00     | 177.9  |
| 1.6500         | .0843               | 2.7322E+00    | -174.6 | 9.6836E+00     | 135.4  | 4.4969E+00     | 133.6  |
| 1.7000         | .0794               | 1.9250E+00    | -165.4 | 9.7742E+00     | 129.1  | 2.0760E+00     | 65.6   |
| 1.7500         | .0750               | 1.1499E+00    | -148.7 | 8.0393E+00     | 120.6  | 2.3574E+00     | -57.3  |
| 1.8000         | .0709               | 6.4954E-01    | -104.6 | 5.0618E+00     | 107.9  | 3.8586E+00     | -117.3 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE VERTICAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |        | 135.00 DEGREES |        | 150.00 DEGREES |        | 165.00 DEGREES |       |
|---------------|---------------------|---------------------|--------|----------------|--------|----------------|--------|----------------|-------|
|               |                     | AMPLITUDE           | PHASE  | AMPLITUDE      | PHASE  | AMPLITUDE      | PHASE  | AMPLITUDE      | PHASE |
| .2000         | 5.7398              | 1.5553E+00          | 51.1   | 1.6052E+00     | 59.1   | 1.6399E+00     | 64.9   |                |       |
| .2500         | 3.6735              | 1.6796E+00          | 30.3   | 1.3125E+00     | 42.0   | 1.0961E+00     | 59.3   |                |       |
| .3000         | 2.5510              | 1.8485E+00          | -27.7  | 1.1187E+00     | -77.6  | 1.4291E+00     | -133.1 |                |       |
| .3500         | 1.8742              | 4.7458E+00          | -82.9  | 5.9780E+00     | -120.9 | 7.8102E+00     | -142.2 |                |       |
| .4000         | 1.4343              | 1.2061E+01          | -107.5 | 1.6716E+01     | -136.4 | 2.1550E+01     | -152.1 |                |       |
| .4500         | 1.1338              | 2.6412E+01          | -123.4 | 3.8860E+01     | -149.1 | 5.0576E+01     | -162.5 |                |       |
| .5000         | .9184               | 5.5230E+01          | -141.9 | 8.7254E+01     | -167.9 | 1.1271E+02     | 176.0  |                |       |
| .5500         | .7590               | 1.0809E+02          | -173.0 | 1.3547E+02     | 154.8  | 1.4259E+02     | 142.0  |                |       |
| .6000         | .6378               | 1.1887E+02          | 150.5  | 1.2515E+02     | 135.9  | 1.3123E+02     | 131.5  |                |       |
| .6500         | .5434               | 1.0334E+02          | 138.2  | 1.1487E+02     | 131.4  | 1.1770E+02     | 127.9  |                |       |
| .7000         | .4686               | 9.3500E+01          | 135.2  | 9.8177E+01     | 127.3  | 8.9207E+01     | 122.8  |                |       |
| .7500         | .4082               | 8.1017E+01          | 131.4  | 6.6192E+01     | 121.3  | 4.4176E+01     | 116.2  |                |       |
| .8000         | .3587               | 5.7737E+01          | 125.4  | 2.3572E+01     | 110.5  | 3.0407E+00     | -66.2  |                |       |
| .8500         | .3178               | 2.5514E+01          | 113.5  | 1.6848E+01     | -62.2  | 3.3947E+01     | -79.1  |                |       |
| .9000         | .2834               | 1.0158E+01          | -35.1  | 3.9526E+01     | -75.2  | 3.8362E+01     | -87.1  |                |       |
| .9500         | .2544               | 3.4809E+01          | -62.1  | 3.9069E+01     | -82.4  | 2.2009E+01     | -85.3  |                |       |
| 1.0000        | .2296               | 4.4035E+01          | -71.4  | 2.2245E+01     | -77.9  | 1.2543E+01     | -19.8  |                |       |
| 1.0500        | .2082               | 3.6396E+01          | -76.9  | 1.3600E+01     | -19.4  | 2.2842E+01     | -2.9   |                |       |
| 1.1000        | .1897               | 1.9685E+01          | -69.3  | 2.2091E+01     | -1.0   | 2.4724E+01     | -19.3  |                |       |
| 1.1500        | .1736               | 1.2502E+01          | -14.2  | 2.3354E+01     | -15.9  | 1.8336E+01     | -30.2  |                |       |
| 1.2000        | .1594               | 1.8313E+01          | 4.6    | 1.7280E+01     | -31.0  | 1.2137E+01     | -5.1   |                |       |
| 1.2500        | .1469               | 1.8301E+01          | -9.7   | 9.7039E+00     | -16.0  | 1.4523E+01     | 17.4   |                |       |
| 1.3000        | .1359               | 1.2974E+01          | -33.1  | 1.0818E+01     | 18.5   | 1.2582E+01     | 12.5   |                |       |
| 1.3500        | .1260               | 5.7061E+00          | -47.7  | 1.0817E+01     | 14.3   | 6.9798E+00     | 19.9   |                |       |
| 1.4000        | .1171               | 3.2847E+00          | 29.5   | 5.7730E+00     | 8.4    | 7.9215E+00     | 59.2   |                |       |
| 1.4500        | .1092               | 5.8088E+00          | 28.6   | 3.3354E+00     | 52.9   | 4.2360E+00     | 33.1   |                |       |
| 1.5000        | .1020               | 4.1149E+00          | -4.5   | 3.6315E+00     | 37.5   | 1.5040E+00     | 77.9   |                |       |
| 1.5500        | .0956               | 1.2056E+00          | -101.3 | 1.4975E+00     | 1.2    | 1.5762E+00     | 80.9   |                |       |
| 1.6000        | .0897               | 1.7488E+00          | 136.7  | 1.5248E+00     | 141.8  | 2.7928E+00     | -76.1  |                |       |
| 1.6500        | .0843               | 1.6359E+00          | 44.0   | 1.5735E+00     | 64.0   | 3.8419E+00     | -128.3 |                |       |
| 1.7000        | .0794               | 2.1982E+00          | -52.2  | 2.2566E+00     | -52.8  | 1.0622E+00     | -49.3  |                |       |
| 1.7500        | .0750               | 2.1197E+00          | -146.4 | 6.6610E-01     | -120.4 | 6.7081E+00     | -58.5  |                |       |
| 1.8000        | .0709               | 2.3976E+00          | 120.8  | 1.8742E+00     | 85.5   | 5.7671E+00     | -91.7  |                |       |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE VERTICAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

## W A V E   A N G L E

| WAVE FREQ. | WAVE/SHIP LENGTH | AMPLITUDE  | PHASE  |
|------------|------------------|------------|--------|
| .2000      | 5.7398           | 1.6541E+00 | 67.0   |
| .2500      | 3.6735           | 1.0523E+00 | 68.0   |
| .3000      | 2.5510           | 1.7569E+00 | -146.1 |
| .3500      | 1.8742           | 8.6643E+00 | -148.4 |
| .4000      | 1.4349           | 2.3327E+01 | -156.6 |
| .4500      | 1.1338           | 5.5394E+01 | -166.6 |
| .5000      | .9184            | 1.2154E+02 | 170.6  |
| .5500      | .7590            | 1.4425E+02 | 139.0  |
| .6000      | .6378            | 1.3317E+02 | 130.4  |
| .6500      | .5434            | 1.1719E+02 | 126.7  |
| .7000      | .4686            | 8.4091E+01 | 121.4  |
| .7500      | .4082            | 3.5465E+01 | 115.0  |
| .8000      | .3587            | 1.1063E+01 | -76.9  |
| .8500      | .3178            | 3.6704E+01 | -83.5  |
| .9000      | .2834            | 3.4608E+01 | -90.5  |
| .9500      | .2544            | 1.5700E+01 | -79.0  |
| 1.0000     | .2296            | 1.5503E+01 | -5.1   |
| 1.0500     | .2082            | 2.4630E+01 | -7.9   |
| 1.1000     | .1897            | 2.3648E+01 | -25.5  |
| 1.1500     | .1736            | 1.5873E+01 | -26.1  |
| 1.2000     | .1594            | 1.3552E+01 | 8.5    |
| 1.2500     | .1469            | 1.5496E+01 | 16.4   |
| 1.3000     | .1359            | 1.1103E+01 | 12.0   |
| 1.3500     | .1260            | 6.7712E+00 | 31.3   |
| 1.4000     | .1171            | 5.9624E+00 | 37.5   |
| 1.4500     | .1092            | 3.1187E+00 | 40.9   |
| 1.5000     | .1020            | 2.0366E+00 | 93.0   |
| 1.5500     | .0956            | 1.3798E+00 | -17.3  |
| 1.6000     | .0897            | 3.7559E+00 | -95.8  |
| 1.6500     | .0843            | 3.4046E+00 | 15.0   |
| 1.7000     | .0794            | 6.2307E+00 | -51.9  |
| 1.7500     | .0750            | 9.4219E+00 | -78.4  |
| 1.8000     | .0709            | 5.7721E+00 | -42.8  |

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SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM VERTICAL SHEAR FORCE AT STATION 10 (L.TONS)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 4.6332E+01          | .73178           | 774.8    |
| 4.879                | 9.7848E+01          | .71360           | 760.0    |
| 7.334                | 1.4889E+02          | .68672           | 739.5    |
| 10.497               | 2.1310E+02          | .68668           | 739.5    |
| 13.867               | 2.7629E+02          | .67283           | 728.8    |
| 17.894               | 3.5993E+02          | .67779           | 732.7    |
| 23.554               | 4.5713E+02          | .66435           | 722.1    |
| 28.835               | 5.3600E+02          | .65601           | 715.2    |
| 37.139               | 6.1165E+02          | .64360           | 704.1    |
| 47.602               | 7.6152E+02          | .64169           | 702.2    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8557              | 1.8232E+02 | 1.9557E+02           | 2.0350E+02 | 2.0814E+02 |
| 4.879                | .8634              | 3.8221E+02 | 4.0965E+02           | 4.2609E+02 | 4.3570E+02 |
| 7.334                | .8742              | 5.8817E+02 | 6.2900E+02           | 6.5364E+02 | 6.6803E+02 |
| 10.497               | .8742              | 8.4185E+02 | 9.0027E+02           | 9.3555E+02 | 9.5614E+02 |
| 13.867               | .8796              | 1.1095E+03 | 1.1860E+03           | 1.2327E+03 | 1.2589E+03 |
| 17.894               | .8777              | 1.4361E+03 | 1.5352E+03           | 1.5954E+03 | 1.6298E+03 |
| 23.554               | .8828              | 1.8584E+03 | 1.9865E+03           | 2.0654E+03 | 2.1086E+03 |
| 28.835               | .8859              | 2.2065E+03 | 2.3595E+03           | 2.4530E+03 | 2.5055E+03 |
| 37.139               | .8904              | 2.5657E+03 | 2.7449E+03           | 2.8538E+03 | 2.9156E+03 |
| 47.602               | .8911              | 3.2035E+03 | 3.4274E+03           | 3.5635E+03 | 3.6407E+03 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM VERTICAL SHEAR FORCE AT STATION 10 (L.TONS)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 3.0084E+02        | 1.2452E-01                   | .90                    | 1.2452E+07        | 8.7548E+07 |
| 6.0167E+02        | 1.8666E-02                   | 1.73                   | 1.8666E+06        | 1.0586E+07 |
| 9.0251E+02        | 3.8069E-03                   | 2.42                   | 3.8069E+05        | 1.4859E+06 |
| 1.2033E+03        | 8.0080E-04                   | 3.10                   | 8.0080E+04        | 3.0061E+05 |
| 1.5042E+03        | 1.5210E-04                   | 3.82                   | 1.5210E+04        | 6.4870E+04 |
| 1.8050E+03        | 2.5239E-05                   | 4.60                   | 2.5239E+03        | 1.2686E+04 |
| 2.1058E+03        | 3.7491E-06                   | 5.43                   | 3.7491E+02        | 2.1490E+03 |
| 2.4067E+03        | 5.3878E-07                   | 6.27                   | 5.3878E+01        | 3.2103E+02 |
| 2.7075E+03        | 8.5499E-08                   | 7.07                   | 8.5499E+00        | 4.5328E+01 |
| 3.0084E+03        | 1.6230E-08                   | 7.79                   | 1.6230E+00        | 6.9270E+00 |
| 3.3092E+03        | 3.4020E-09                   | 8.47                   | 3.4020E-01        | 1.2828E+00 |
| 3.6100E+03        | 6.9783E-10                   | 9.16                   | 6.9783E-02        | 2.7042E-01 |
| 3.9109E+03        | 1.3132E-10                   | 9.88                   | 1.3132E-02        | 5.6651E-02 |
| 4.2117E+03        | 2.2141E-11                   | 10.65                  | 2.2141E-03        | 1.0917E-02 |
| 4.5125E+03        | 3.3184E-12                   | 11.48                  | 3.3184E-04        | 1.8823E-03 |
| 4.8134E+03        | 4.4076E-13                   | 12.36                  | 4.4076E-05        | 2.8776E-04 |
| 5.1142E+03        | 5.1820E-14                   | 13.29                  | 5.1820E-06        | 3.8894E-05 |
| 5.4150E+03        | 5.3902E-15                   | 14.27                  | 5.3902E-07        | 4.6430E-06 |
| 5.7159E+03        | 4.9595E-16                   | 15.30                  | 4.9595E-08        | 4.8942E-07 |
| 6.0167E+03        | 4.0364E-17                   | 16.39                  | 4.0364E-09        | 4.5558E-08 |
| 6.3175E+03        | 2.9062E-18                   | 17.54                  | 2.9062E-10        | 3.7458E-09 |
| 6.6184E+03        | 1.8512E-19                   | 18.73                  | 1.8512E-11        | 2.7211E-10 |
| 6.9192E+03        | 1.0434E-20                   | 19.98                  | 1.0434E-12        | 1.7469E-11 |
| 7.2201E+03        | 5.2050E-22                   | 21.28                  | 5.2050E-14        | 9.9139E-13 |
| 7.5209E+03        | 2.2981E-23                   | 22.64                  | 2.2981E-15        | 4.9751E-14 |
| 7.8217E+03        | 8.9824E-25                   | 24.05                  | 8.9824E-17        | 2.2083E-15 |
| 8.1226E+03        | 3.1083E-26                   | 25.51                  | 3.1083E-18        | 8.6716E-17 |
| 8.4234E+03        | 9.5238E-28                   | 27.02                  | 9.5238E-20        | 3.0131E-18 |
| 8.7242E+03        | 2.5839E-29                   | 28.59                  | 2.5839E-21        | 9.2655E-20 |
| 9.0251E+03        | 6.2073E-31                   | 30.21                  | 6.2073E-23        | 2.5218E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 1.5744E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 1.9511E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 2.3108E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 2.6819E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 3.1016E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 3.5417E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 3.9569E+03 (AMPLITUDE)

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |        |               |        |               |        |
|---------------|---------------------|---------------------|--------|---------------|--------|---------------|--------|
|               |                     | 15.00 DEGREES       |        | 30.00 DEGREES |        | 45.00 DEGREES |        |
|               |                     | AMPLITUDE           | PHASE  | AMPLITUDE     | PHASE  | AMPLITUDE     | PHASE  |
| .2000         | 5.7398              | 5.6962E-01          | -29.5  | 9.9126E-01    | -32.7  | 1.1880E+00    | -38.9  |
| .2500         | 3.6735              | 1.2426E+00          | -18.6  | 2.1044E+00    | -20.6  | 2.3924E+00    | -24.8  |
| .3000         | 2.5510              | 2.5369E+00          | -12.8  | 4.2735E+00    | -13.4  | 4.8922E+00    | -15.1  |
| .3500         | 1.8742              | 4.7871E+00          | -10.8  | 8.1446E+00    | -10.5  | 9.7779E+00    | -14.5  |
| .4000         | 1.4349              | 8.2765E+00          | -11.5  | 1.4294E+01    | -10.6  | 1.6062E+01    | -18.5  |
| .4500         | 1.1338              | 1.3097E+01          | -13.6  | 2.2906E+01    | -12.4  | 2.4604E+01    | -18.9  |
| .5000         | .9184               | 1.8958E+01          | -16.7  | 3.3564E+01    | -15.1  | 3.6704E+01    | -19.4  |
| .5500         | .7590               | 1.8660E+01          | -18.3  | 4.5354E+01    | -18.2  | 5.2141E+01    | -20.7  |
| .6000         | .6378               | 1.8276E+01          | -20.7  | 5.6446E+01    | -21.5  | 6.9671E+01    | -22.6  |
| .6500         | .5434               | 1.7833E+01          | -23.9  | 6.4167E+01    | -24.9  | 8.6932E+01    | -24.6  |
| .7000         | .4686               | 1.7374E+01          | -28.0  | 6.1137E+01    | -26.1  | 1.0049E+02    | -26.3  |
| .7500         | .4082               | 1.6952E+01          | -33.1  | 5.7505E+01    | -27.8  | 1.0516E+02    | -27.7  |
| .8000         | .3587               | 1.6639E+01          | -39.2  | 5.3310E+01    | -30.1  | 1.0046E+02    | -29.9  |
| .8500         | .3178               | 1.6521E+01          | -46.3  | 4.8615E+01    | -33.2  | 8.8019E+01    | -32.6  |
| .9000         | .2834               | 1.6689E+01          | -54.2  | 4.3523E+01    | -37.6  | 8.1986E+01    | -33.2  |
| .9500         | .2544               | 1.7232E+01          | -62.5  | 3.8219E+01    | -43.7  | 7.5069E+01    | -34.0  |
| 1.0000        | .2296               | 1.6726E+01          | -65.3  | 3.3045E+01    | -52.6  | 6.7278E+01    | -35.1  |
| 1.0500        | .2082               | 1.5063E+01          | -67.6  | 2.8641E+01    | -65.7  | 5.8634E+01    | -36.7  |
| 1.1000        | .1897               | 1.2775E+01          | -73.1  | 2.5342E+01    | -67.5  | 4.9174E+01    | -39.2  |
| 1.1500        | .1736               | 1.0062E+01          | -80.6  | 2.0940E+01    | -73.9  | 3.8985E+01    | -43.2  |
| 1.2000        | .1594               | 7.4286E+00          | -84.6  | 1.6814E+01    | -83.9  | 2.8305E+01    | -50.8  |
| 1.2500        | .1469               | 5.7699E+00          | -77.1  | 1.3142E+01    | -90.2  | 1.8028E+01    | -68.7  |
| 1.3000        | .1359               | 4.2607E+00          | -72.4  | 9.9216E+00    | -85.7  | 1.2293E+01    | -85.2  |
| 1.3500        | .1260               | 1.9986E+00          | -124.3 | 7.5478E+00    | -71.9  | 1.0036E+01    | -102.7 |
| 1.4000        | .1171               | 2.2104E+00          | -150.5 | 3.6659E+00    | -80.1  | 8.2011E+00    | -104.4 |
| 1.4500        | .1092               | 1.6680E+00          | -87.2  | 3.2095E+00    | -169.7 | 5.9262E+00    | -91.1  |
| 1.5000        | .1020               | 5.0605E-01          | 12.0   | 2.8117E+00    | -135.9 | 3.6558E+00    | -61.4  |
| 1.5500        | .0956               | 1.3717E+00          | 127.3  | 2.7898E+00    | -52.5  | 1.2902E+00    | -7.1   |
| 1.6000        | .0897               | 5.4408E-01          | -99.7  | 1.7273E+00    | 61.9   | 2.6118E+00    | 143.6  |
| 1.6500        | .0843               | 1.6508E+00          | -7.5   | 2.4397E+00    | 143.6  | 3.0083E+00    | -176.6 |
| 1.7000        | .0794               | 1.3999E+00          | 41.9   | 1.7401E+00    | -98.6  | 3.4779E+00    | -69.5  |
| 1.7500        | .0750               | 7.1058E-01          | -48.5  | 2.2187E+00    | -9.5   | 3.4941E+00    | -1.0   |
| 1.8000        | .0709               | 2.4130E+00          | -34.9  | 1.8044E+00    | 82.8   | 3.2340E+00    | 96.0   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

REGULAR WAVE LATERAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |               |                  |
|---------------|---------------------|---------------------|---------------|------------------|
|               |                     | 60.00 DEGREES       | 75.00 DEGREES | 90.00 DEGREES    |
| .2000         | 5.7398              | 1.1931E+00          | -49.8         | 1.1343E+00 -65.5 |
| .2500         | 3.6735              | 2.2373E+00          | -33.3         | 2.0857E+00 -51.2 |
| .3000         | 2.5510              | 4.7497E+00          | -28.6         | 3.0225E+00 -58.0 |
| .3500         | 1.8742              | 7.0816E+00          | -28.5         | 4.0118E+00 -46.1 |
| .4000         | 1.4349              | 1.1220E+01          | -22.3         | 5.8234E+00 -35.1 |
| .4500         | 1.1338              | 1.7814E+01          | -19.2         | 8.6549E+00 -27.0 |
| .5000         | .9184               | 2.7400E+01          | -18.3         | 1.2766E+01 -22.7 |
| .5500         | .7590               | 4.0414E+01          | -19.0         | 1.8371E+01 -20.0 |
| .6000         | .6378               | 5.6959E+01          | -20.5         | 2.5540E+01 -19.7 |
| .6500         | .5434               | 7.6518E+01          | -22.4         | 3.4342E+01 -16.8 |
| .7000         | .4686               | 9.7658E+01          | -24.5         | 4.4537E+01 -22.9 |
| .7500         | .4082               | 1.1797E+02          | -26.5         | 5.5929E+01 -25.6 |
| .8000         | .3587               | 1.3424E+02          | -28.2         | 6.7963E+01 -28.6 |
| .8500         | .3178               | 1.4312E+02          | -29.7         | 7.9889E+01 -31.9 |
| .9000         | .2834               | 1.4203E+02          | -30.9         | 9.0494E+01 -35.1 |
| .9500         | .2544               | 1.3018E+02          | -31.9         | 1.0002E+02 -39.1 |
| 1.0000        | .2296               | 1.0920E+02          | -33.1         | 1.0604E+02 -40.9 |
| 1.0500        | .2082               | 8.3033E+01          | -35.3         | 1.0749E+02 -43.3 |
| 1.1000        | .1897               | 5.7313E+01          | -40.2         | 1.0409E+02 -45.3 |
| 1.1500        | .1736               | 3.6584E+01          | -51.4         | 9.5293E+01 -46.8 |
| 1.2000        | .1594               | 2.5165E+01          | -70.2         | 8.1298E+01 -47.7 |
| 1.2500        | .1469               | 2.0741E+01          | -81.3         | 6.3058E+01 -47.8 |
| 1.3000        | .1359               | 1.6450E+01          | -79.7         | 4.2302E+01 -47.0 |
| 1.3500        | .1260               | 1.4740E+01          | -79.2         | 2.1161E+01 -44.4 |
| 1.4000        | .1171               | 1.2881E+01          | -78.5         | 2.3616E+00 -12.3 |
| 1.4500        | .1092               | 1.0872E+01          | -77.5         | 1.3063E+01 129.8 |
| 1.5000        | .1020               | 8.7175E+00          | -75.9         | 2.2256E+01 135.0 |
| 1.5500        | .0956               | 6.4243E+00          | -73.1         | 2.5185E+01 130.1 |
| 1.6000        | .0897               | 4.0196E+00          | -66.4         | 2.2386E+01 143.1 |
| 1.6500        | .0843               | 1.7076E+00          | -38.8         | 1.5386E+01 146.9 |
| 1.7000        | .0794               | 1.9877E+00          | 58.6          | 6.4601E+00 146.4 |
| 1.7500        | .0750               | 2.7665E+00          | 56.2          | 2.4148E+00 15.3  |
| 1.8000        | .0709               | 3.1998E+00          | 59.8          | 7.9545E+00 2.3   |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE LATERAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE<br>FREQ. | WAVE/SHIP<br>LENGTH | W A V E   A N G L E |                |                   |
|---------------|---------------------|---------------------|----------------|-------------------|
|               |                     | 105.00 DEGREES      | 120.00 DEGREES | 135.00 DEGREES    |
| .2000         | 5.7398              | 1.1794E+00          | -94.4          | 1.2487E+00 -101.0 |
| .2500         | 3.6735              | 2.0212E+00          | -112.4         | 1.8942E+00 -122.2 |
| .3000         | 2.5510              | 2.4941E+00          | -117.5         | 2.5411E+00 -126.3 |
| .3500         | 1.8742              | 3.1207E+00          | -124.0         | 3.4653E+00 -132.3 |
| .4000         | 1.4349              | 3.8366E+00          | -132.8         | 4.9120E+00 -139.5 |
| .4500         | 1.1338              | 4.7583E+00          | -143.0         | 7.4152E+00 -147.3 |
| .5000         | .9184               | 6.1940E+00          | -152.7         | 1.1472E+01 -154.2 |
| .5500         | .7590               | 8.1834E+00          | -160.5         | 1.7427E+01 -158.6 |
| .6000         | .6378               | 1.0869E+01          | -163.9         | 2.4892E+01 -161.8 |
| .6500         | .5434               | 1.4169E+01          | -164.2         | 3.4579E+01 -164.5 |
| .7000         | .4686               | 1.7674E+01          | -163.3         | 4.6470E+01 -166.6 |
| .7500         | .4082               | 2.1768E+01          | -162.4         | 5.9771E+01 -167.7 |
| .8000         | .3587               | 2.6735E+01          | -162.1         | 7.2633E+01 -167.9 |
| .8500         | .3178               | 3.2379E+01          | -161.9         | 8.2372E+01 -167.4 |
| .9000         | .2834               | 3.8546E+01          | -161.7         | 8.6440E+01 -166.4 |
| .9500         | .2544               | 4.5042E+01          | -161.4         | 8.2909E+01 -165.2 |
| 1.0000        | .2296               | 5.1042E+01          | -161.1         | 7.1541E+01 -163.6 |
| 1.0500        | .2082               | 5.5871E+01          | -160.7         | 5.4385E+01 -161.0 |
| 1.1000        | .1897               | 5.8578E+01          | -160.4         | 3.5371E+01 -155.0 |
| 1.1500        | .1736               | 5.8324E+01          | -160.3         | 1.9755E+01 -137.8 |
| 1.2000        | .1594               | 5.4610E+01          | -160.7         | 1.3487E+01 -100.7 |
| 1.2500        | .1469               | 4.7363E+01          | -161.7         | 1.4154E+01 -79.1  |
| 1.3000        | .1359               | 3.7055E+01          | -163.8         | 1.3429E+01 -82.7  |
| 1.3500        | .1260               | 2.4757E+01          | -168.3         | 1.0451E+01 -103.4 |
| 1.4000        | .1171               | 1.2195E+01          | 179.0          | 7.4697E+00 -141.5 |
| 1.4500        | .1092               | 4.5002E+00          | 100.7          | 5.9003E+00 168.3  |
| 1.5000        | .1020               | 1.0919E+01          | 39.3           | 5.1859E+00 115.8  |
| 1.5500        | .0956               | 1.6284E+01          | 27.2           | 3.0925E+00 67.7   |
| 1.6000        | .0897               | 1.7759E+01          | 19.9           | 4.7260E+00 36.1   |
| 1.6500        | .0843               | 1.5605E+01          | 13.7           | 1.8031E+00 -20.0  |
| 1.7000        | .0794               | 1.0779E+01          | 6.8            | 1.8384E+00 -156.7 |
| 1.7500        | .0750               | 4.7905E+00          | -3.1           | 3.4445E+00 155.7  |
| 1.8000        | .0709               | 9.7428E-01          | -151.8         | 3.8032E+00 115.3  |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

## REGULAR WAVE LATERAL SHEAR FORCE AT STATION 10 (L.TONS/ FEET )

| WAVE FREQ. | WAVE/SHIP LENGTH | 150.00 AMPLITUDE | DEGREES PHASE | W A V E A N G L E |
|------------|------------------|------------------|---------------|-------------------|
| .2000      | 5.7398           | 9.3396E-01       | -116.2        | 4.8888E-01 -120.7 |
| .2500      | 3.6735           | 1.1672E+00       | -126.4        | 6.1072E-01 -126.3 |
| .3000      | 2.5510           | 1.6959E+00       | -128.1        | 9.1300E-01 -127.6 |
| .3500      | 1.8742           | 2.7429E+00       | -134.0        | 1.5739E+00 -134.7 |
| .4000      | 1.4349           | 5.0051E+00       | -144.5        | 3.0713E+00 -147.0 |
| .4500      | 1.1338           | 9.3074E+00       | -155.6        | 5.8218E+00 -158.4 |
| .5000      | .9184            | 1.5720E+01       | -163.1        | 9.8019E+00 -166.3 |
| .5500      | .7590            | 2.4273E+01       | -168.7        | 1.4857E+01 -170.8 |
| .6000      | .6378            | 3.4278E+01       | -171.4        | 2.0109E+01 -172.4 |
| .6500      | .5434            | 4.3338E+01       | -171.7        | 2.3671E+01 -171.6 |
| .7000      | .4686            | 4.8183E+01       | -170.2        | 2.3822E+01 -168.7 |
| .7500      | .4082            | 4.6422E+01       | -167.3        | 2.0343E+01 -164.0 |
| .8000      | .3587            | 3.8454E+01       | -162.4        | 1.4983E+01 -155.2 |
| .8500      | .3178            | 2.7874E+01       | -153.4        | 1.0877E+01 -138.4 |
| .9000      | .2834            | 2.0177E+01       | -136.4        | 1.0097E+01 -120.0 |
| .9500      | .2544            | 1.8599E+01       | -117.9        | 1.0983E+01 -113.0 |
| 1.0000     | .2296            | 1.9891E+01       | -111.3        | 1.0854E+01 -113.9 |
| 1.0500     | .2082            | 1.9401E+01       | -113.1        | 9.0143E+00 -114.2 |
| 1.1000     | .1897            | 1.6004E+01       | -115.7        | 6.6547E+00 -103.7 |
| 1.1500     | .1736            | 1.1242E+01       | -108.6        | 5.8063E+00 -82.9  |
| 1.2000     | .1594            | 8.8718E+00       | -85.1         | 5.6701E+00 -76.3  |
| 1.2500     | .1469            | 8.8734E+00       | -73.6         | 4.5546E+00 -81.1  |
| 1.3000     | .1359            | 7.4939E+00       | -80.4         | 6.3666E+01 136.0  |
| 1.3500     | .1260            | 4.7430E+00       | -87.7         | 2.2886E+00 -34.4  |
| 1.4000     | .1171            | 2.7273E+00       | -45.3         | 2.2078E+00 -43.3  |
| 1.4500     | .1092            | 3.2746E+00       | -31.6         | 1.1464E+00 -71.9  |
| 1.5000     | .1020            | 2.4398E+00       | -62.0         | 5.3381E-01 70.6   |
| 1.5500     | .0956            | 7.2900E-01       | -132.5        | 7.9713E-01 46.4   |
| 1.6000     | .0897            | 1.5607E+00       | 84.6          | 5.3288E-01 -78.6  |
| 1.6500     | .0843            | 1.2286E+00       | 2.7           | 1.9809E+00 169.3  |
| 1.7000     | .0794            | 1.1188E+00       | -72.2         | 1.7536E+00 -174.9 |
| 1.7500     | .0750            | 2.9613E+00       | 166.3         | 2.8316E+00 25.5   |
| 1.8000     | .0709            | 7.4192E-01       | -124.2        | 1.4802E+01 -16.9  |

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SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## SHORT TERM LATERAL SHEAR FORCE AT STATION 10 (L.TONS)

| WAVE HT.<br>( FEET ) | ROOT MEAN<br>SQUARE | BROADNESS<br>EPS | PER HOUR |
|----------------------|---------------------|------------------|----------|
| 2.380                | 2.9486E+01          | .73990           | 951.7    |
| 4.879                | 5.8749E+01          | .73684           | 931.4    |
| 7.334                | 8.1608E+01          | .73297           | 901.2    |
| 10.497               | 1.1678E+02          | .73297           | 901.2    |
| 13.867               | 1.4407E+02          | .73139           | 884.8    |
| 17.894               | 1.9110E+02          | .73192           | 890.8    |
| 23.554               | 2.3099E+02          | .73063           | 874.2    |
| 28.835               | 2.6243E+02          | .73010           | 863.1    |
| 37.139               | 2.8541E+02          | .72996           | 844.8    |
| 47.602               | 3.5268E+02          | .73005           | 841.7    |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>( FEET ) | WIDE BAND<br>CORR. | 8.0 HRS    | HIGHEST OCCURANCE IN |            |            |
|----------------------|--------------------|------------|----------------------|------------|------------|
|                      |                    |            | 24.0 HRS             | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8522              | 1.1506E+02 | 1.2250E+02           | 1.2688E+02 | 1.2943E+02 |
| 4.879                | .8535              | 2.2877E+02 | 2.4357E+02           | 2.5224E+02 | 2.5729E+02 |
| 7.334                | .8552              | 3.1792E+02 | 3.3855E+02           | 3.5062E+02 | 3.5768E+02 |
| 10.497               | .8552              | 4.5495E+02 | 4.8446E+02           | 5.0174E+02 | 5.1184E+02 |
| 13.867               | .8559              | 5.6267E+02 | 5.9928E+02           | 6.2082E+02 | 6.3342E+02 |
| 17.894               | .8557              | 7.4551E+02 | 7.9395E+02           | 8.2240E+02 | 8.3904E+02 |
| 23.554               | .8562              | 9.0463E+02 | 9.6383E+02           | 9.9846E+02 | 1.0187E+03 |
| 28.835               | .8564              | 1.0316E+03 | 1.0995E+03           | 1.1391E+03 | 1.1622E+03 |
| 37.139               | .8565              | 1.1312E+03 | 1.2057E+03           | 1.2503E+03 | 1.2758E+03 |
| 47.602               | .8565              | 1.4001E+03 | 1.4924E+03           | 1.5479E+03 | 1.5794E+03 |

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISSC

SHORT CRESTED SEAS- 90.0 DEG - COS\*\* 2.0

## LONG TERM LATERAL SHEAR FORCE AT STATION 10 (L.TONS)

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+08        | 0.         |
| 1.2609E+02        | 2.0827E-01                   | .68                    | 2.0827E+07        | 7.9173E+07 |
| 2.5219E+02        | 3.6234E-02                   | 1.44                   | 3.6234E+06        | 1.7204E+07 |
| 3.7828E+02        | 8.1669E-03                   | 2.09                   | 8.1669E+05        | 2.8067E+06 |
| 5.0437E+02        | 2.0133E-03                   | 2.70                   | 2.0133E+05        | 6.1535E+05 |
| 6.3047E+02        | 4.6297E-04                   | 3.33                   | 4.6297E+04        | 1.5504E+05 |
| 7.5656E+02        | 9.1845E-05                   | 4.04                   | 9.1845E+03        | 3.7112E+04 |
| 8.8265E+02        | 1.5551E-05                   | 4.81                   | 1.5551E+03        | 7.6295E+03 |
| 1.0087E+03        | 2.2936E-06                   | 5.64                   | 2.2936E+02        | 1.3257E+03 |
| 1.1348E+03        | 3.1187E-07                   | 6.51                   | 3.1187E+01        | 1.9817E+02 |
| 1.2609E+03        | 4.3531E-08                   | 7.36                   | 4.3531E+00        | 2.6834E+01 |
| 1.3870E+03        | 6.9494E-09                   | 8.16                   | 6.9494E-01        | 3.6582E+00 |
| 1.5131E+03        | 1.2531E-09                   | 8.90                   | 1.2531E-01        | 5.6962E-01 |
| 1.6392E+03        | 2.2921E-10                   | 9.64                   | 2.2921E-02        | 1.0239E-01 |
| 1.7653E+03        | 3.9133E-11                   | 10.41                  | 3.9133E-03        | 1.9008E-02 |
| 1.8914E+03        | 6.0153E-12                   | 11.22                  | 6.0153E-04        | 3.3117E-03 |
| 2.0175E+03        | 8.2258E-13                   | 12.08                  | 8.2258E-05        | 5.1927E-04 |
| 2.1436E+03        | 9.9708E-14                   | 13.00                  | 9.9708E-06        | 7.2287E-05 |
| 2.2697E+03        | 1.0701E-14                   | 13.97                  | 1.0701E-06        | 8.9007E-06 |
| 2.3958E+03        | 1.0165E-15                   | 14.99                  | 1.0165E-07        | 9.6845E-07 |
| 2.5219E+03        | 8.5438E-17                   | 16.07                  | 8.5438E-09        | 9.3104E-08 |
| 2.6480E+03        | 6.3537E-18                   | 17.20                  | 6.3537E-10        | 7.9085E-09 |
| 2.7741E+03        | 4.1796E-19                   | 18.38                  | 4.1796E-11        | 5.9357E-10 |
| 2.9001E+03        | 2.4318E-20                   | 19.61                  | 2.4318E-12        | 3.9365E-11 |
| 3.0262E+03        | 1.2512E-21                   | 20.90                  | 1.2512E-13        | 2.3067E-12 |
| 3.1523E+03        | 5.6914E-23                   | 22.24                  | 5.6914E-15        | 1.1943E-13 |
| 3.2784E+03        | 2.2886E-24                   | 23.64                  | 2.2886E-16        | 5.4626E-15 |
| 3.4045E+03        | 8.1339E-26                   | 25.09                  | 8.1339E-18        | 2.2073E-16 |
| 3.5306E+03        | 2.5546E-27                   | 26.59                  | 2.5546E-19        | 7.8785E-18 |
| 3.6567E+03        | 7.0891E-29                   | 28.15                  | 7.0891E-21        | 2.4837E-19 |
| 3.7828E+03        | 1.7379E-30                   | 29.76                  | 1.7379E-22        | 6.9153E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 7.4993E+02 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 9.1174E+02 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 1.0612E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 1.2077E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 1.3620E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 1.5299E+03 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 1.6984E+03 (AMPLITUDE)

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APPENDIX B

EXPLANATION OF RESULTS

This appendix will briefly describe the meaning and significance of the results generated by program SCOMOT. The program capabilities and limitations will be explained in the following sections.

### 1. Response Amplitude Operators

The six basic responses calculated by program SCOTMOT are vertical plane motions of heave, pitch and surge and lateral plane motions of sway, yaw and roll. The results are expressed in complex notation, for instance, heave,  $\delta_1$ ,

$$\delta_1 = \delta_{1R} + i\delta_{1I}$$

or as an amplitude and phase

$$\delta_1 = \delta_{10} e^{-i\varepsilon_1} = \delta_{10} \sin \varepsilon_1 + i\delta_{10} \cos \varepsilon_1$$

$$\text{where } \delta_{10} = \sqrt{\delta_{1R}^2 + \delta_{1I}^2}$$

$$\text{and } \varepsilon = \arctan (\delta_{1R} / \delta_{1I})$$

The phase angle,  $\varepsilon_1$ , represents the heave motion lead with respect to the wave elevation and  $\delta_{10}$  is the amplitude of the sinusoidal oscillation with a frequency of encounter,  $\omega_e$ . Therefore, the equation for heave displacement is expressed as follows:

$$\delta_1 = \delta_{10} e^{-i(\omega_e t + \varepsilon_1)}$$

For heave velocity and acceleration two successive differentiations with respect to  $t$  produce:

$$\dot{\delta}_1 = \delta_{10} \omega_e e^{-i(\omega_e t + \varepsilon_1)} = -i\omega_e \delta_1$$

$$\ddot{\delta}_1 = -\delta_{10} i\omega_e^2 e^{-i(\omega_e t + \varepsilon_1)} = -\omega_e^2 \delta_1$$

The expressions for the other five primary motions,  $\delta_i$  for  $i = 2$  to  $6$ , are identical to that just described for heave.

Three motions, in the vertical, lateral, and longitudinal, plane directions can be calculated for any input coordinate point  $x_p, y_p, z_p$ , measured from the forward perpendicular, the centerline and baseline respectively. These distances are transformed to the center of gravity therefore

$$x = XCG - x_p$$

$$y = y_p$$

$$z = KG - z_p$$

The vertical, lateral and longitudinal point displacements,  $\delta_7, \delta_8, \delta_9$ , respectively are given as follows:

$$\delta_7 = \delta_1 - x\delta_2 + y\delta_6$$

$$\delta_8 = \delta_4 + x\delta_5 - z\delta_6$$

$$\delta_9 = \delta_3 + z\delta_2 + y\delta_5$$

Where  $\delta_1$  to  $\delta_6$  are heave, pitch, surge, sway, yaw and roll displacements. Differentiating each of these components with respect to time will result in point velocities and accelerations.

In order to determine relative motion at any point, that is displacement, velocity and acceleration, the wave motion must be calculated at a specific point and subtracted from the point motion illustrated above. The vertical wave motions in complex form are as follows:

$$\eta = Aic^{-i}(-kx\cos\beta + kysin\beta + \omega t)$$

$$\dot{\eta} = Awc^{-i}(-kx\cos\beta + kysin\beta + \omega t) = -iwn$$

$$\ddot{\eta} = -Aie^{-i}(-kx\cos\beta + kysin\beta + \omega t) = -\omega^2\eta$$

for displacement, velocity and acceleration respectively, where A is the wave amplitude,  $\omega$  the wave frequency, k the wave number and  $\beta$  the wave angle.

The vertical relative motion for displacement, velocity and acceleration are:

$$\begin{aligned}\delta_{10} &= \delta_7 - \eta \\ \dot{\delta}_{10} &= \dot{\delta}_7 - \dot{\eta} = -i\omega_e \delta_7 + i\omega \eta \\ \ddot{\delta}_{10} &= \ddot{\delta}_7 - \ddot{\eta} = -\omega_e^2 \delta_7 + \omega^2 \eta\end{aligned}$$

These relative motions are used to calculate shipping of water, slamming and racing of the propeller statistics which are described in a later section.

The final RAO's calculated by SCOMOT are torsion and vertical and lateral bending moments and shear forces. These are explained in II.A of the main body of this report.

The six primary motions and forces and moments, calculated by SCOMOT for a range of ship speeds, wave headings, and wave frequency are written to a file, RAOname, specified in Data Set 1. This is performed for the first execution of SCOMOT and is controlled by option control F of Data Set 3. For subsequent runs of SCOMOT, providing that the ship characteristics remain unchanged, the calculation of these primary motions can be skipped and any response discussed previously can be printed out and studied. This capability is again controlled by option control tag F of Data Set 3.

The choice of RAO's is specified in Data Set 23, the Response Control Card. Each card, selects a response type, IZ, which can range from 1 to 23 for heave, pitch, etc. The next entry on this card, IMOT, controls the motion type; displacement, velocity or acceleration for any motion other than the moments and shear forces. The next entry, IR, enables the user to print the RAO's as a function of wave heading and frequency. The RAO's can be plotted with the frequency as the abscissa and response as ordinate if the plot option, IPLRAO, is greater than zero. If IPLRAO is equal to 1, RAO's for every wave heading is plotted, if 2, every other wave heading is plotted, etc. An example of this is shown in figure B1. You must contact your UCS salesman to arrange for plotting and its delivery.

## 2. Wave Spectra

The wave spectra used in determining the short term responses can be analytical of Betschneider type, measured such as INDIA, PAPA, KILO, Great Lakes or a FNOC forecast or hindcast spectra from their SOWM wave model as discussed in the body of this report. The printing of the mean wave spectrum and the spectral properties is controlled by option E of Data Set 3. These printed characteristics for the mean spectra of each group are summarized here for convenience:

$H_{1/3}$

significant wave height =  $4\sqrt{m_0}$

T(1)

mean average period =  $2\pi m_0/m_1$

|                     |   |
|---------------------|---|
| $T(-1)$             | energy average period = $2\pi(m_{-1}/m_0)$                                |
| $T(2)$              | zero-crossing period = $2\pi\sqrt{m_0/m_2}$                               |
| $T(4)$              | average apparent period = $2\pi\sqrt{(m_2/m_4)}$                          |
| $H(1/3)$            | $H_{1/3} \times \sqrt{1 - \frac{1}{2}\epsilon^2}$                         |
| Skewness            | $m_3/m_2^{3/2}$   |
| $\epsilon$          | $\sqrt{1 - \frac{m_2^2}{m_0 m_4}}$ - spectral width parameter (broadness) |
| Flatness            | $m_4/m_2^2$   |
| $\omega_0$          | peak spectral frequency   |
| $H_{1/3}/\lambda_0$ | wave slope  |

$m(-1)$   
 $m_0$   
 $m_1$   
 $m_2$   
 $m_3$   
 $m_4$

$$m_n = \int_0^n \omega^n S_\zeta(\omega) \cdot d\omega$$

### 3. Short Term Responses

The response spectrum is created by the linear superposition of the RAO's squared with the energy wave spectrum. The properties of this curve, area,  $m_0$  and first moment through fourth moments  $m_i$  to  $m_4$  are calculated for each wave heading as follows:

$$m_n(\beta) = \int_0^{\infty} \text{RAO}(\omega_1 \beta)^2 S\xi(\omega) \omega^n d\omega \quad \text{for } n = 0 \text{ to } 4$$

These properties combined with the appropriate spreading function will give the short crested moments that are used to calculate the root mean square (RMS) response, the spectral width parameter (broadness) and cycles per hour for any wave heading as follows:

$$\text{RMS} = \sqrt{m_0}$$

$$\epsilon = \sqrt{1 - \frac{m_2^2}{m_0 m_4}} \quad \text{- broadness}$$

$$\begin{aligned} \text{Cycles per hour} &= 7200/T_2 \\ &= 7200/(2\pi \sqrt{m_0/m_2}) \end{aligned}$$

where 7200 zero crossings (3600 cycles) per hour.

Quite often a spectra family with more than one spectra within a wave height band (group) is used to describe a certain sea condition. In these cases the mean RMS<sub>a</sub>, and the standard deviation are as follows:

$$\begin{aligned} \text{RMS}_a &= \frac{1}{N} \sum_{i=1}^N \text{RMS}_i \\ \sigma &= \left[ \frac{1}{N} \sum_{i=1}^N \text{RMS}_i^2 - \text{RMS}_a^2 \right]^{1/2} \end{aligned}$$

The new moments used to calculate the broadness and cycles per hour are the average values of the N spectra within that wave height group.

These short term results are performed for the response chosen by IZ on Data Set 23 providing that either the IS or IL options on the same card are greater than zero. If IS is specified to be 1, a detailed printout of each wave height group showing the RMS, standard deviation, broadness and cycles per hour for each wave heading is given. If IS is set equal to 2, a summary printout showing the averages for each group is given using the probability of headings specified in Option control tag N of Data Set 3. The short term responses as a function of wave height and wave direction can be plotted if the IPLSHT variable of Data Set 23 is greater than zero. Again, if it is equal to 1 every wave heading is plotted, to 2 every other wave heading is plotted, etc. and an example can be seen in Figure B2.

These short term calculations for relative motion and relative velocity are needed to determine the slamming, shipping of water or racing of the propeller statistics. Given the coordinate point, the RAO vertical relative displacement and velocity can be generated as previously explained. These RAO's are used to determine RMS values for different wave angles and wave height groups. The statistics are defined as the probability of exceeding a threshold value and the number of exceedances over a certain time period. These as given by Ochi can be written as follows:

$$\Pr \{ \text{slam impact} \} = e^{-\left(\frac{H^2}{R_{r1}} + \frac{r_*^2}{R_{r1}^2}\right)}$$

where

$H$  = ship draft at location considered

$r^*$  = threshold relative velocity,  $0.093 \sqrt{g L}$

$R_{r1}$  = twice variance of the relative motion

$R_{r1}'$  = twice variance of the relative velocity

$g$  = acceleration of gravity

$L$  = ship length

The variances of relative motion and velocity in the above equation are equal to the areas under the spectral density functions of relative motion and velocity, respectively, at the desired location.

The number of impacts in  $T$  hours can be written as follows:

$$N(T) = 3600 \frac{T}{2\pi} \sqrt{\frac{R_{r1}'}{R_{r1}}} \cdot \Pr \{ \text{slam impact} \}$$

In a similar manner the shipping of water statistics are as follows:

$$\Pr \{ \text{shipping of water} \} = e^{-\frac{F^2}{R_{r1}}}$$

where  $F$  = freeboard at location considered and the number of exceedances in  $T$  hours is

$$N(T) = 3600 \frac{T}{2\pi} \sqrt{\frac{R_{r1}'}{R_{r1}}} \cdot \Pr \{ \text{slam impact} \}$$

the propeller racing is as follows:

$$\Pr \{ \text{propeller racing} \} = e^{-\frac{B^2}{R_{r1}}}$$

where  $B$  = clearance between the tip of the propeller blade and the water surface

The number of occurrences in T hours is:

$$N(T) = \frac{T}{2\pi} \sqrt{\frac{R_f}{R_{r1}}} \cdot Pr \text{ (propeller racing)}$$

These statistics are calculated when input option tag I on Data Set 3 is set equal to 1 with additional input from Data Set 11. In addition, slamming and shipping of water can be calculated at any location given in Data Set 12 if IZ of Data Set 23 is defined as 23. If more than one input point is defined in Data Set 12, then the use of variables J1, J2 and JINC in Data Set 23 enables the user to selective run the slamming and shipping of water statistics only for the points of interest.

#### 4. Long Term Responses

The long term responses are executed if variable IL on Data Set 23 is defined to 1. Two tables of long term responses are produced. The first is the highest response expected during a time period defined in Data Set 22 for each height group shown in Figure B3 while the second is a combined distribution including the combined effect of all wave heights as shown in Figure B4. In order to run the combined long term response, the probability of each wave height group must be defined as explained in Data Set 20.

The wide band correction factor is defined as

$$= \sqrt{1 - \frac{1}{2} \epsilon^2}$$

and is a correction that Ochi has introduced into the long term statistics to account for processes which are not narrow banded, ( $\epsilon$  large). This number is included in the long term statistics since this correction is used by the ABS to calculate its bending moment.

The long term vertical bending moment at Station 10 shown in Figure B4 is given with its corresponding probability of exceedance. The negative log of the probability is a convenient representation of the probability level. The highest response in  $10^8$  cycles would correspond to 8 in this column. The number in life corresponds to the number of occurrences of the specified response value assuming  $10^8$  cycles in a lifetime. The histogram represents the total number of occurrences above the specified response value, i.e., there are 10 occurrences of  $1.0921 \times 10^8$  ft-tons or larger in the ships lifetime.

The bending moment at midships for the SL-7 seen in Figure B4 can be compared with that generated using the 1979 ABS rules.

From these rules:

$$M_w = C_2 L^2 B H_e K_b$$

$$K_B = 1.4 - 0.5 C_B = 1.125$$

$$C_2 = (6.53 C_B + 0.57) 10^{-4} = 4.1615 \times 10^{-4}$$

$$L = 880.5 \text{ ft}$$

$$B = 105.5 \text{ ft}$$

$$C_B = .55$$

$$H_e = 4.50L - 0.00216 L^2 + 335 \quad 10^{-2} = 59.7186 \text{ ft}$$

therefore the wave induced bending moment is

$$M_w = 2.28677 \times 10^6 \text{ ft-tons}$$

yet the bending moment calculated for  $10^8$  cycles from the program SCOMOT is

$$M_w = 1.1942 \times 10^6 \text{ ft-tons}$$

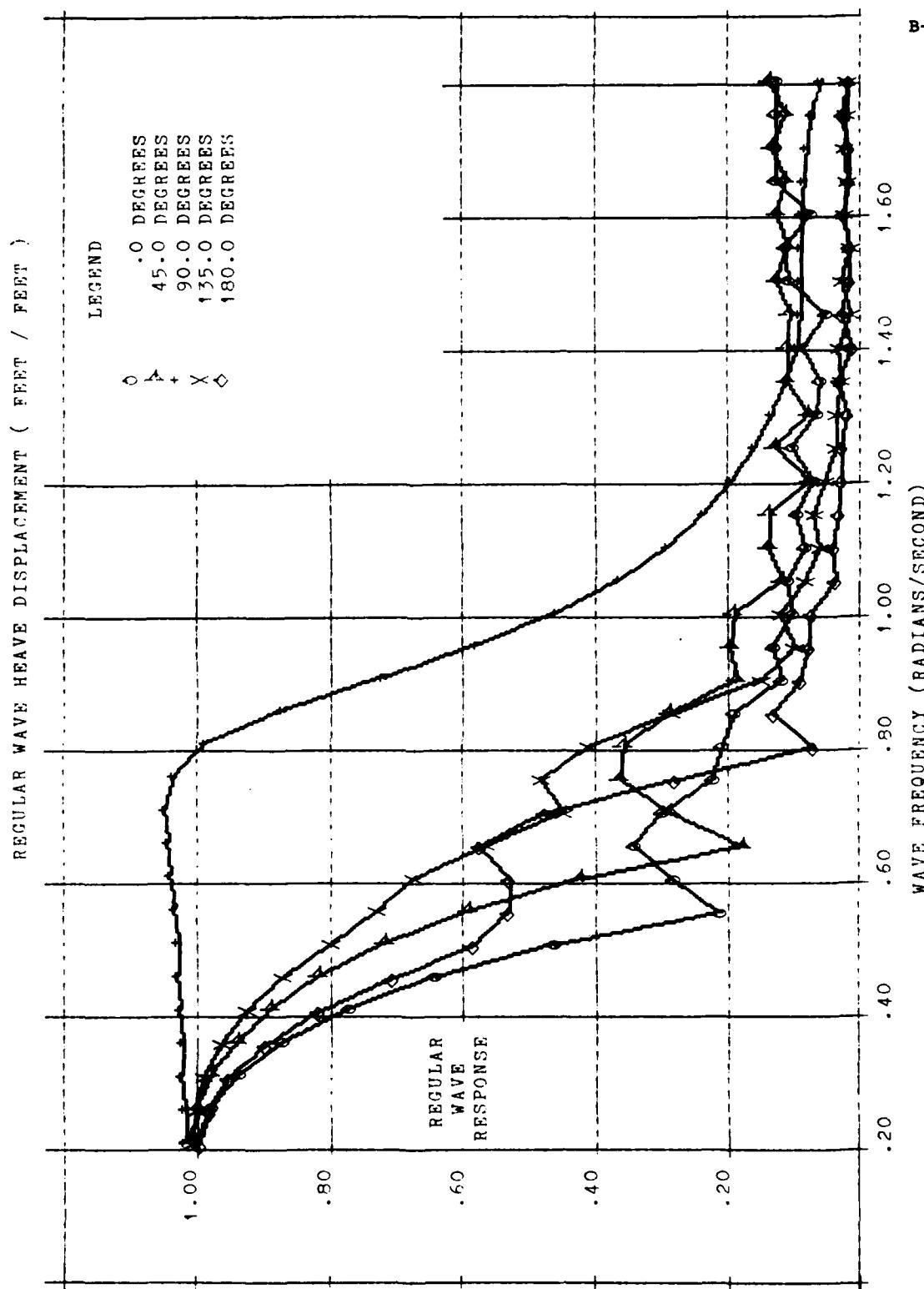
This large discrepancy is caused by utilizing an ISSC spectra with a single spectrum in each wave height group rather than wave families employed by ABS. Consequently, the standard deviation of the response is zero and a small long term value will result.

In order to compare "apples to apples" the H Family or Station INDIA Family must be used with Program SCOMOT to determine the long term wave induced bending moment for comparison to ABS rules.

SHIP MOTION PROGRAM VER. (12/79)  
SL-7 FULL LOAD EXAMPLE

DATE OF RUN - 2/25/81

TIME OF RUN - 12:22:29  
SHIP SPEED = 10.000 KNOTS

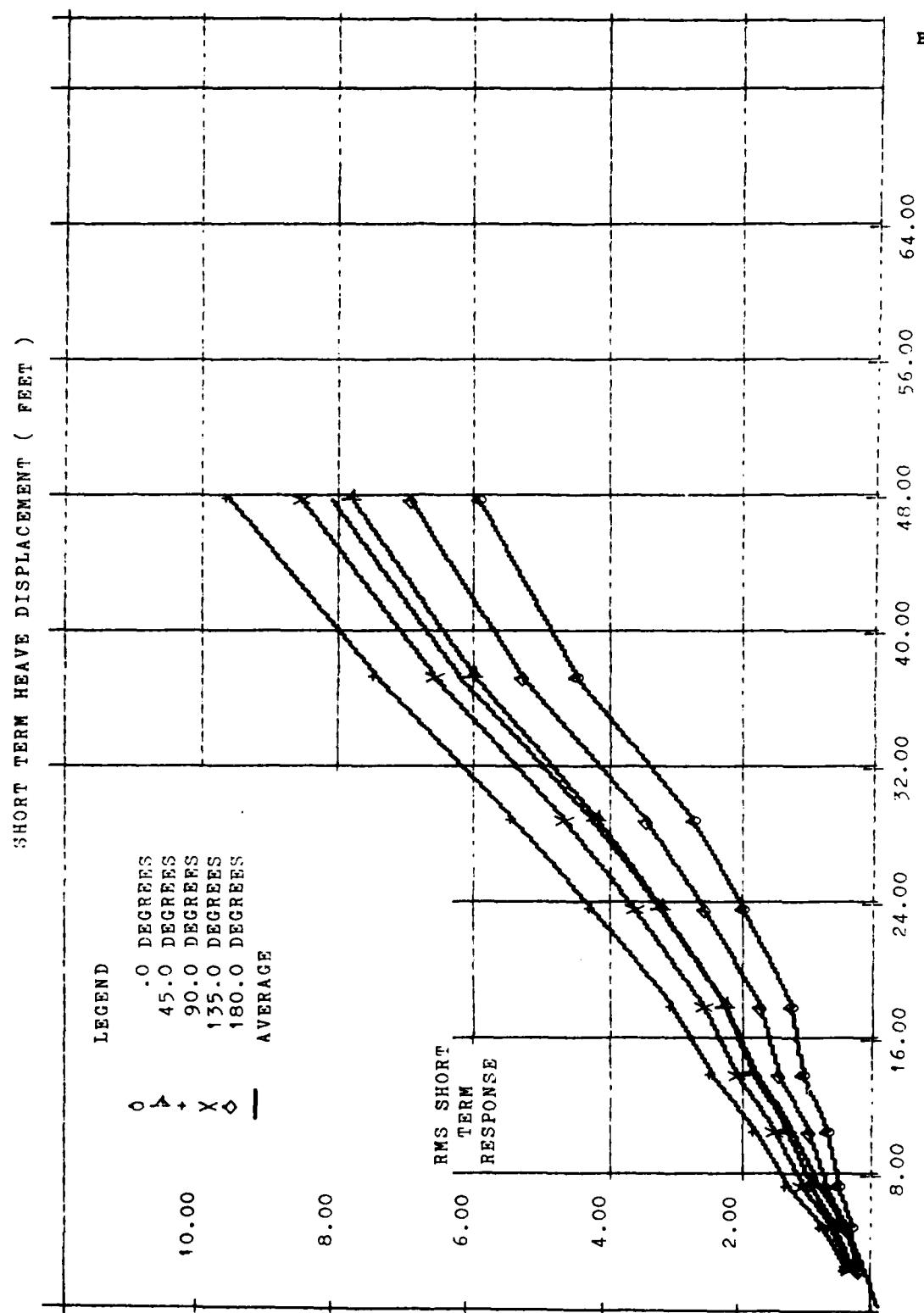


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Figure B1 - Response Amplitude Operators for Heave

SHIP MOTION PROGRAM VER. (12/79)  
SL-7 FULL LOAD EXAMPLE  
TWO PARAMETER ISSC +/- 90.0 DEGREES COS\*\*2.0 SPREADING FUNCTION

DATE OF RUN - 2/25/81 TIME OF RUN - 12:22:29  
SHIP SPEED = 10.000 KNOTS  
SHORT CRESTED SEAS



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Figure B2 - Short Term Responses for Heave

SHIP MOTION PROGRAM SL-7

02/24/81

05.40.10

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SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 20.000 KNOTS

TWO PARAMETER LOAD

SHORT CRESTED SEAS - 90.0 DEG - COS\*\* 2.1

SHRT TERM VERTICAL BENDING MOMENT AT STATION 10 ' FEET - L.TOKN'

| WAVE HT. | ROOT MEAN SQUARED | PEAK      | HIGHEST OCCURRANCE |
|----------|-------------------|-----------|--------------------|
| 2.380    | 5.014E+04         | .6171E+04 | 785.7              |
| 4.670    | 1.0796E+04        | .6453E+04 | 760.1              |
| 7.372    | 2.4155E+04        | .6404E+04 | 722.7              |
| 10.407   | 5.7966E+04        | .6404E+04 | 722.6              |
| 13.867   | 7.9721E+04        | .6256E+04 | 702.0              |
| 17.894   | 1.0159E+05        | .6770E+04 | 709.6              |
| 22.554   | 1.3774E+05        | .6212E+04 | 688.5              |
| 28.875   | 1.6854E+05        | .6152E+04 | 674.0              |
| 37.173   | 2.0843E+05        | .6062E+04 | 649.0              |
| 47.602   | 2.6330E+05        | .6050E+04 | 644.6              |

## LONG TERM RESULTS FOR INDIVIDUAL WAVE HEIGHT GROUPS

| WAVE HT.<br>' FEET ' | WIDE BAND<br>CORR. | 9.0 HRS    | HIGHEST OCCURRANCE IN |            |            |
|----------------------|--------------------|------------|-----------------------|------------|------------|
|                      |                    |            | 24.0 HRS              | 48.0 HRS   | 72.0 HRS   |
| 2.380                | .8777              | 4.0817E+04 | 4.3501E+04            | 4.5169E+04 | 4.6080E+04 |
| 4.670                | .8833              | 9.5229E+04 | 1.0187E+05            | 1.0588E+05 | 1.0821E+05 |
| 7.374                | .8916              | 1.7126E+05 | 1.8380E+05            | 1.9126E+05 | 1.9562E+05 |
| 10.407               | .8911              | 2.4518E+05 | 2.6314E+05            | 2.7782E+05 | 2.8605E+05 |
| 13.867               | .8957              | 3.4941E+05 | 3.7545E+05            | 3.9087E+05 | 3.9982E+05 |
| 17.894               | .8942              | 4.7371E+05 | 4.7228E+05            | 4.9157E+05 | 5.0285E+05 |
| 22.554               | .8981              | 6.1491E+05 | 6.6117E+05            | 6.8835E+05 | 7.0426E+05 |
| 28.875               | .9004              | 7.6920E+05 | 8.2732E+05            | 8.6147E+05 | 8.8144E+05 |
| 37.173               | .8934              | 9.7601E+05 | 1.0508E+06            | 1.0945E+06 | 1.1200E+06 |
| 47.602               | .9038              | 1.2777E+06 | 1.3322E+06            | 1.3877E+06 | 1.4201E+06 |

Figure B3 - Short and Long Term by Wave Height Results for SL-7

SL-7 - NORMAL FULL LOAD DEPARTURE

SPEED = 25.000 KNOTS

TWO PARAMETER ISCT

SHORT CRESTED SEAS- 30.0 DEG - COS\*\* 2.1

## LONG TERM VERTICAL PENDING MOMENT AT STATION 10' FEET -L.TONS'

| RESPONSE<br>VALUE | PROBABILITY OF<br>EXCEEDENCE | -LOG OF<br>PROBABILITY | NUMBER<br>IN LIFE | HISTOGRAM  |
|-------------------|------------------------------|------------------------|-------------------|------------|
| 0.                | 1.0000E+00                   | 0.00                   | 1.0000E+00        | 0.         |
| 1.2135E+05        | 5.5747E-02                   | 1.25                   | 5.5747E+16        | 9.4425E+07 |
| 2.4270E+05        | 5.8449E-02                   | 2.15                   | 6.8449E+05        | 4.8902E+07 |
| 3.6404E+05        | 1.1575E-02                   | 2.94                   | 1.1575E+05        | 5.6875E+05 |
| 4.8539E+05        | 1.9457E-02                   | 3.74                   | 1.9457E+04        | 3.6362E+04 |
| 6.0674E+05        | 3.0567E-02                   | 4.53                   | 3.0055E+03        | 1.6482E+04 |
| 7.2809E+05        | 4.4252E-02                   | 5.33                   | 4.4252E+01        | 1.1619E+07 |
| 8.4944E+05        | 6.9825E-02                   | 6.12                   | 6.9825E+01        | 7.7271E+02 |
| 9.7079E+05        | 1.3648E-02                   | 6.86                   | 1.3648E+01        | 5.8178E+01 |
| 1.0921E+06        | 2.2745E-02                   | 7.43                   | 2.2745E+01        | 1.0617E+01 |
| 1.2135E+06        | 6.0071E-09                   | 8.10                   | 6.0071E-01        | 2.4735E+00 |
| 1.3348E+06        | 1.8799E-09                   | 8.73                   | 1.8799E-01        | 6.1272E-01 |
| 1.4562E+06        | 4.0291E-10                   | 9.39                   | 4.0291E-02        | 1.4770E-01 |
| 1.5775E+06        | 7.7611E-11                   | 10.11                  | 7.7611E-03        | 3.2530E-02 |
| 1.6989E+06        | 1.3334E-11                   | 10.88                  | 1.3334E-03        | 6.4277E-03 |
| 1.8202E+06        | 2.0355E-12                   | 11.69                  | 2.0355E-04        | 1.1299E-03 |
| 1.9416E+06        | 2.7554E-13                   | 12.56                  | 2.7554E-05        | 1.7600E-04 |
| 2.0629E+06        | 3.3041E-14                   | 13.48                  | 3.3041E-06        | 2.4250E-05 |
| 2.1843E+06        | 3.5077E-15                   | 14.45                  | 3.5077E-07        | 2.9533E-06 |
| 2.3056E+06        | 3.2958E-16                   | 15.48                  | 3.2958E-08        | 3.1782E-07 |
| 2.4270E+06        | 2.7399E-17                   | 16.56                  | 2.7399E-09        | 3.0218E-08 |
| 2.5483E+06        | 2.0151E-18                   | 17.70                  | 2.0151E-10        | 2.5384E-09 |
| 2.6697E+06        | 1.3111E-19                   | 18.86                  | 1.3111E-11        | 1.8840E-10 |
| 2.7910E+06        | 1.5470E-21                   | 20.12                  | 1.5470E-12        | 1.2357E-11 |
| 2.9124E+06        | 7.8474E-22                   | 21.40                  | 7.8474E-14        | 7.1620E-12 |
| 3.0337E+06        | 1.7319E-22                   | 22.76                  | 1.7319E-15        | 7.6703E-14 |
| 3.1551E+06        | 6.9057E-25                   | 24.16                  | 6.9057E-17        | 1.6628E-15 |
| 3.2764E+06        | 2.4368E-26                   | 25.61                  | 2.4368E-18        | 6.6620E-17 |
| 3.3977E+06        | 7.6096E-28                   | 27.12                  | 7.6096E-20        | 2.3607E-18 |
| 3.5191E+06        | 2.1030E-29                   | 28.65                  | 2.1030E-21        | 7.3993E-20 |
| 3.6404E+06        | 5.1431E-31                   | 30.29                  | 5.1431E-22        | 2.0516E-21 |

## INTERPOLATED VALUES

MAXIMUM VALUE IN 10\*\* 4 CYCLES = 5.2870E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 5 CYCLES = 6.7645E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 6 CYCLES = 8.2583E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 7 CYCLES = 9.9700E+05 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 8 CYCLES = 1.1942E+06 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\* 9 CYCLES = 1.3846E+06 (AMPLITUDE)  
 MAXIMUM VALUE IN 10\*\*10 CYCLES = 1.5589E+06 (AMPLITUDE)

Figure B4 - Combined Long Term Results for SL-7

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APPENDIX C

JOB CONTROL FILES

07/31/80. 15.41.52.

LIST OF COMSMOT

00100 JOB,CM20000,L05,T200.  
00110 ACCOUNT,U707008, [REDACTED]  
00120 GET,SCOMOT.  
00130 RFL,200000.  
00140 UNIFORE(-BATCH, LN=SMOTCOM, T=SCOMOT)  
00150 PUT,LGO=SMOTBIN.  
00160 GET,ZETASFO/LIB.  
00170 LDSET(LIB=ZETASFO)  
00180 LGO.  
00190 PUT,TAPE99=PLOTOUT.  
00200 PUT,OUTPUT=RESULT1.  
00210 PUT,SMOTCOM.  
00220 PUT,DAY1.  
00230 DFD,DAY1,R.  
00240 EXIT.  
00250 NOEXIT.  
00260 PUT,OUTPUT=RESULT1.  
00270 PUT,TAPE99=PLOTOUT.  
00280 PUT,SMOTCOM.  
00290 PUT,DAY1.  
00300 DFD,DAY1,R.  
00310 EOR.  
00320 SDMSL7  
00330 EOF.

TABLE 1.

07/31/80. 15.40.27.

LIST OF RUNSMOT

```
00100 JOB,CM20000,L05,T200.  
00110 ACCOUNT,U707008, [REDACTED].  
00120 GET,LGO=SMOTBIN.  
00130 RFL,200000.  
00140 GET,ZFTASFC/LIB.  
00150 LD$SET(LIB=ZETASFO1  
00160 LGO.  
00170 PUT,TAPE99=PLOTOUT.  
00180 PUT,OUTPUT=RESULT1.  
00190 PUT,DAY1.  
00200 DFD,DAY1,R.  
00210 EXIT.  
00220 NOEXIT.  
00230 PUT,OUTPUT=RESULT1.  
00240 PUT,TAPE99=PLOTOUT.  
00250 PUT,DAY1.  
00260 DFD,DAY1,R.  
00270 EOR.  
00280 SDMSL7  
00290 EOF.
```

TABLE 2.

TABLE 3

APPENDIX D  
TWO DIMENSIONAL PROPERTIES FILE

```
PROGRAM TDPREAD(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE1)
```

```
C
```

```
C
```

```
C THIS PROGRAM READS THE TWO DIMENSIONAL PROPERTIES (TDP)  
C FILE CREATED BY PROGRAM "STATIC" AND READ BY PROGRAM  
C "SCOMOT"
```

```
C
```

```
C
```

```
C THE VARIABLE DEFINITION IS AS FOLLOWS:
```

```
C
```

```
C XOFF(J) = DISTANCE OF STATION J FROM F.P.  
C NOFF(J) = NUMBER OF OFFSET PAIRS ON STATION J  
C YOFF(I,J) = DISTANCE FROM C.L. FOR OFFSET I, STATION J  
C ZOFF(I,J) = DISTANCE FROM B.L. FOR OFFSET I, STATION J  
C NWET(J) = NUMBER OF WETTED OFFSET PAIRS ON STATION J  
C YWET(I,J) = DISTANCE FROM C.L. FOR OFFSET I, STATION J  
C ZWET(I,J) = DISTANCE FROM W.L. FOR OFFSET I, STATION J  
C TDP(K,L,J) = TWO-DIMENSION HYDRODYNAMIC COEFFICIENT L, FOR  
C FREQUENCY K AND STATION J
```

```
C
```

```
C COMMON/GEO/XOFF(21),NOFF(21),YOFF(29,21),ZOFF(29,21),  
& NWET(21),YWET(21,21),ZWET(21,21),TDP(25,10,21)  
DIMENSION Z2(21),Y2(21),SNE(20),CSE(20),DEL(20),TDPIN(25,10)  
WRITE(6,900)  
READ(5,800)TDPNAM  
III=-1  
CALL DFUR(4HGETR,1,TDPNAM,0,0,III)  
NSTA = 21  
DO 40 J = 1,NSTA  
READ(1)XOFF(J),NON,(ZOFF(I,J),YOFF(I,J),I=1,NON)  
NOFF(J) = NON  
READ(1)NONP1,DFT,Y2,Z2,SNE,CSE,DEL  
WRITE(6,910)J,XOFF(J),NON,DFT  
READ(1) TDPIN  
NONP1 = NON + 1  
NWET(J) = NONP1  
DO 20 I = 1,NONP1  
YWET(I,J) = Y2(I)  
ZWET(I,J) = Z2(I)  
20 CONTINUE  
40 STOP  
800 FORMAT(A7)  
900 FORMAT(5X,22HENTER TDP FILE NAME ? )  
910 FORMAT(I5,F10.4,I5,F10.4 )  
END
```

APPENDIX E  
RESULTS FROM PROGRAM STATIC

PROGRAM STATIC (05/79)

07/28/80

20.21.08

PAGE 1

## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500 BEAM = 105.500 DEPTH = 64.305

|           |            |            |
|-----------|------------|------------|
| STATION 1 | STATION 2  | STATION 3  |
| 21 POINTS | 21 POINTS  | 21 POINTS  |
| X = 0.000 | X = 11.006 | X = 22.013 |

|    | HEIGHT Z | H-B Y |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|-------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000 | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .820     | 3.035 | 2  | .820     | 3.180  | 2  | .820     | 3.324  |
| 3  | 1.640    | 4.480 | 3  | 1.640    | 4.625  | 3  | 1.640    | 4.769  |
| 4  | 3.281    | 6.070 | 4  | 3.281    | 6.214  | 4  | 3.281    | 6.359  |
| 5  | 4.921    | 6.648 | 5  | 4.921    | 6.995  | 5  | 4.921    | 7.082  |
| 6  | 6.562    | 7.024 | 6  | 6.562    | 7.226  | 6  | 6.562    | 7.515  |
| 7  | 8.202    | 7.082 | 7  | 8.202    | 7.226  | 7  | 8.202    | 7.573  |
| 8  | 9.842    | 6.735 | 8  | 9.842    | 6.995  | 8  | 9.842    | 7.284  |
| 9  | 11.483   | 6.214 | 9  | 11.483   | 6.590  | 9  | 11.483   | 6.937  |
| 10 | 13.123   | 5.492 | 10 | 13.123   | 5.839  | 10 | 13.123   | 6.301  |
| 11 | 16.404   | 3.815 | 11 | 16.404   | 4.278  | 11 | 16.404   | 4.654  |
| 12 | 19.685   | 2.341 | 12 | 19.685   | 2.890  | 12 | 19.685   | 3.324  |
| 13 | 22.966   | 1.156 | 13 | 22.966   | 1.792  | 13 | 22.966   | 2.283  |
| 14 | 26.247   | .289  | 14 | 26.247   | 1.156  | 14 | 26.247   | 1.532  |
| 15 | 29.528   | 0.000 | 15 | 29.528   | .867   | 15 | 29.528   | 1.301  |
| 16 | 32.808   | 0.000 | 16 | 32.808   | 1.098  | 16 | 32.808   | 1.503  |
| 17 | 39.370   | 1.012 | 17 | 39.370   | 2.023  | 17 | 39.370   | 2.862  |
| 18 | 45.932   | 2.515 | 18 | 45.932   | 3.613  | 18 | 45.932   | 4.971  |
| 19 | 52.493   | 4.278 | 19 | 52.493   | 5.839  | 19 | 52.493   | 7.717  |
| 20 | 59.055   | 6.272 | 20 | 59.055   | 8.382  | 20 | 59.055   | 10.608 |
| 21 | 65.125   | 8.238 | 21 | 65.026   | 10.897 | 21 | 64.993   | 13.354 |

|            |            |            |
|------------|------------|------------|
| STATION 4  | STATION 5  | STATION 6  |
| 21 POINTS  | 21 POINTS  | 21 POINTS  |
| X = 44.025 | X = 66.037 | X = 88.050 |

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .820     | 3.757  | 2  | .820     | 4.191  | 2  | .820     | 4.625  |
| 3  | 1.640    | 5.203  | 3  | 1.640    | 5.578  | 3  | 1.640    | 6.128  |
| 4  | 3.281    | 6.879  | 4  | 3.281    | 7.399  | 4  | 3.281    | 8.035  |
| 5  | 4.921    | 7.660  | 5  | 4.921    | 8.527  | 5  | 4.921    | 9.163  |
| 6  | 6.562    | 8.151  | 6  | 6.562    | 8.671  | 6  | 6.562    | 9.481  |
| 7  | 8.202    | 8.238  | 7  | 8.202    | 8.902  | 7  | 8.202    | 9.770  |
| 8  | 9.842    | 8.093  | 8  | 9.842    | 8.816  | 8  | 9.842    | 9.683  |
| 9  | 11.483   | 7.804  | 9  | 11.483   | 8.527  | 9  | 11.483   | 9.336  |
| 10 | 13.123   | 7.226  | 10 | 13.123   | 8.093  | 10 | 13.123   | 8.960  |
| 11 | 16.404   | 5.839  | 11 | 16.404   | 6.648  | 11 | 16.404   | 7.949  |
| 12 | 19.685   | 4.336  | 12 | 19.685   | 5.347  | 12 | 19.685   | 6.937  |
| 13 | 22.966   | 3.180  | 13 | 22.966   | 4.393  | 13 | 22.966   | 6.214  |
| 14 | 26.247   | 2.601  | 14 | 26.247   | 4.133  | 14 | 26.247   | 6.214  |
| 15 | 29.528   | 2.544  | 15 | 29.528   | 4.336  | 15 | 29.528   | 6.879  |
| 16 | 32.808   | 3.035  | 16 | 32.808   | 5.000  | 16 | 32.808   | 8.006  |
| 17 | 39.370   | 5.058  | 17 | 39.370   | 7.602  | 17 | 39.370   | 10.926 |
| 18 | 45.932   | 7.862  | 18 | 45.932   | 10.984 | 18 | 45.932   | 14.452 |
| 19 | 52.493   | 11.273 | 19 | 52.493   | 11.909 | 19 | 52.493   | 18.267 |
| 20 | 59.055   | 14.886 | 20 | 59.055   | 18.788 | 20 | 59.055   | 23.066 |
| 21 | 64.961   | 18.007 | 21 | 64.895   | 22.545 | 21 | 64.797   | 27.112 |

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## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

STATION 7

21 POINTS

X = 110.062

STATION 8

22 POINTS

X = 132.075

STATION 9

22 POINTS

X = 176.100

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .820     | 5.145  | 2  | .066     | 2.890  | 2  | .131     | 4.336  |
| 3  | 1.640    | 6.879  | 3  | .820     | 5.925  | 3  | .820     | 6.937  |
| 4  | 3.281    | 8.460  | 4  | 1.640    | 7.226  | 4  | 1.640    | 8.758  |
| 5  | 4.921    | 9.394  | 5  | 3.281    | 8.960  | 5  | 3.281    | 10.695 |
| 6  | 6.562    | 9.827  | 6  | 4.921    | 10.059 | 6  | 4.921    | 11.909 |
| 7  | 8.202    | 10.261 | 7  | 6.562    | 10.666 | 7  | 6.562    | 12.862 |
| 8  | 9.842    | 10.406 | 8  | 8.202    | 10.952 | 8  | 8.202    | 13.585 |
| 9  | 11.483   | 10.203 | 9  | 9.842    | 11.273 | 9  | 9.842    | 14.306 |
| 10 | 13.123   | 10.050 | 10 | 11.483   | 11.330 | 10 | 11.483   | 14.741 |
| 11 | 16.404   | 9.394  | 11 | 13.123   | 11.273 | 11 | 13.123   | 15.319 |
| 12 | 19.685   | 8.758  | 12 | 16.404   | 11.128 | 12 | 16.404   | 16.331 |
| 13 | 22.966   | 8.613  | 13 | 19.685   | 11.041 | 13 | 19.685   | 17.342 |
| 14 | 26.247   | 9.018  | 14 | 22.966   | 11.330 | 14 | 22.966   | 18.354 |
| 15 | 29.528   | 9.827  | 15 | 26.247   | 12.140 | 15 | 26.247   | 19.741 |
| 16 | 32.808   | 11.041 | 16 | 29.528   | 13.151 | 16 | 29.528   | 21.042 |
| 17 | 39.370   | 14.452 | 17 | 32.808   | 14.597 | 17 | 32.808   | 22.487 |
| 18 | 45.932   | 18.267 | 18 | 39.370   | 18.094 | 18 | 39.370   | 25.783 |
| 19 | 52.493   | 22.545 | 19 | 45.932   | 22.112 | 19 | 45.932   | 29.482 |
| 20 | 59.055   | 27.112 | 20 | 52.493   | 26.303 | 20 | 52.493   | 33.529 |
| 21 | 64.698   | 31.303 | 21 | 59.055   | 30.927 | 21 | 59.055   | 37.864 |
|    |          |        | 22 | 64.633   | 34.974 | 22 | 64.534   | 41.911 |

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## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

STATION 10

22 POINTS

X = 220.125

STATION 11

22 POINTS

X = 264.150

STATION 12

22 POINTS

X = 308.175

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .197     | 4.336  | 2  | .262     | 7.226  | 2  | .328     | 11.562 |
| 3  | .820     | 8.960  | 3  | .820     | 12.284 | 3  | .820     | 17.198 |
| 4  | 1.640    | 10.839 | 4  | 1.640    | 14.741 | 4  | 1.640    | 20.233 |
| 5  | 3.281    | 13.296 | 5  | 3.281    | 18.210 | 5  | 3.281    | 24.424 |
| 6  | 4.921    | 15.319 | 6  | 4.921    | 20.666 | 6  | 4.921    | 27.025 |
| 7  | 6.562    | 16.967 | 7  | 6.562    | 22.776 | 7  | 6.562    | 29.338 |
| 8  | 8.202    | 18.152 | 8  | 8.202    | 24.279 | 8  | 8.202    | 31.216 |
| 9  | 9.842    | 19.366 | 9  | 9.842    | 25.667 | 9  | 9.842    | 32.806 |
| 10 | 11.483   | 20.233 | 10 | 11.483   | 26.736 | 10 | 11.483   | 34.107 |
| 11 | 13.123   | 21.158 | 11 | 13.123   | 27.893 | 11 | 13.123   | 35.465 |
| 12 | 16.404   | 23.037 | 12 | 16.404   | 30.003 | 12 | 16.404   | 37.489 |
| 13 | 19.685   | 24.568 | 13 | 19.685   | 31.794 | 13 | 19.685   | 39.136 |
| 14 | 22.966   | 26.014 | 14 | 22.966   | 33.297 | 14 | 22.966   | 40.408 |
| 15 | 26.247   | 27.459 | 15 | 26.247   | 34.830 | 15 | 26.247   | 41.622 |
| 16 | 29.528   | 28.904 | 16 | 29.528   | 36.188 | 16 | 29.528   | 42.720 |
| 17 | 32.808   | 30.349 | 17 | 32.808   | 37.633 | 17 | 32.808   | 43.790 |
| 18 | 39.370   | 33.297 | 18 | 39.370   | 40.177 | 18 | 39.370   | 45.697 |
| 19 | 45.932   | 36.708 | 19 | 45.932   | 42.720 | 19 | 45.932   | 47.605 |
| 20 | 52.493   | 40.119 | 20 | 52.493   | 45.380 | 20 | 52.493   | 49.224 |
| 21 | 59.055   | 43.790 | 21 | 59.055   | 45.183 | 21 | 59.055   | 50.871 |
| 22 | 64.370   | 46.969 | 22 | 64.337   | 50.351 | 22 | 64.305   | 52.027 |

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## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

STATION 13

22 POINTS

X = 352.200

STATION 14

22 POINTS

X = 396.225

STATION 15

18 POINTS

X = 440.250

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .394     | 19.366 | 2  | .591     | 26.303 | 2  | .656     | 32.662 |
| 3  | .820     | 23.412 | 3  | .820     | 30.060 | 3  | .820     | 34.685 |
| 4  | 1.640    | 27.314 | 4  | 1.640    | 33.962 | 4  | 1.640    | 39.310 |
| 5  | 3.281    | 31.505 | 5  | 3.281    | 38.298 | 5  | 3.281    | 43.212 |
| 6  | 4.921    | 33.962 | 6  | 4.921    | 40.610 | 6  | 4.921    | 45.380 |
| 7  | 6.562    | 36.564 | 7  | 6.562    | 42.778 | 7  | 6.562    | 47.114 |
| 8  | 8.202    | 38.298 | 8  | 8.202    | 44.310 | 8  | 8.202    | 48.559 |
| 9  | 9.842    | 39.888 | 9  | 9.842    | 45.524 | 9  | 9.842    | 49.571 |
| 10 | 11.483   | 41.044 | 10 | 11.483   | 46.478 | 10 | 11.483   | 50.293 |
| 11 | 13.123   | 42.142 | 11 | 13.123   | 47.345 | 11 | 13.123   | 50.958 |
| 12 | 16.404   | 43.934 | 12 | 16.404   | 48.703 | 12 | 16.404   | 51.912 |
| 13 | 19.685   | 45.235 | 13 | 19.685   | 49.715 | 13 | 19.685   | 52.374 |
| 14 | 22.966   | 46.247 | 14 | 22.966   | 50.351 | 14 | 22.966   | 52.605 |
| 15 | 26.247   | 47.171 | 15 | 26.247   | 50.929 | 15 | 26.247   | 52.663 |
| 16 | 29.528   | 47.836 | 16 | 29.528   | 51.305 | 16 | 29.528   | 52.721 |
| 17 | 32.808   | 48.559 | 17 | 32.808   | 51.594 | 17 | 32.808   | 52.750 |
| 18 | 39.370   | 49.715 | 18 | 39.370   | 52.027 | 18 | 64.305   | 52.750 |
| 19 | 45.932   | 50.640 | 19 | 45.932   | 52.374 |    |          |        |
| 20 | 52.493   | 51.565 | 20 | 52.493   | 52.605 |    |          |        |
| 21 | 59.055   | 52.259 | 21 | 59.055   | 52.750 |    |          |        |
| 22 | 64.305   | 52.548 | 22 | 64.305   | 52.750 |    |          |        |

STATION 16

15 POINTS

X = 484.275

STATION 17

15 POINTS

X = 528.300

STATION 18

17 POINTS

X = 572.325

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .656     | 32.751 | 2  | .656     | 32.751 | 2  | .492     | 24.636 |
| 3  | .820     | 35.650 | 3  | .820     | 33.911 | 3  | .820     | 28.694 |
| 4  | 1.640    | 40.867 | 4  | 1.640    | 38.548 | 4  | 1.640    | 33.621 |
| 5  | 3.281    | 44.635 | 5  | 3.281    | 42.751 | 5  | 3.281    | 38.548 |
| 6  | 4.921    | 46.953 | 6  | 4.921    | 45.359 | 6  | 4.921    | 41.504 |
| 7  | 6.562    | 48.692 | 7  | 6.562    | 47.185 | 7  | 6.562    | 43.910 |
| 8  | 8.202    | 49.910 | 8  | 8.202    | 48.692 | 8  | 8.202    | 45.794 |
| 9  | 9.842    | 50.721 | 9  | 9.842    | 49.649 | 9  | 9.842    | 47.243 |
| 10 | 11.483   | 51.446 | 10 | 11.483   | 50.489 | 10 | 11.483   | 48.547 |
| 11 | 13.123   | 52.025 | 11 | 13.123   | 51.214 | 11 | 13.123   | 49.562 |
| 12 | 16.404   | 52.518 | 12 | 16.404   | 52.083 | 12 | 16.404   | 51.011 |
| 13 | 19.685   | 52.750 | 13 | 19.685   | 52.605 | 13 | 19.685   | 51.880 |
| 14 | 22.966   | 52.750 | 14 | 22.966   | 52.750 | 14 | 22.966   | 52.402 |
| 15 | 68.242   | 52.750 | 15 | 68.242   | 52.750 | 15 | 26.247   | 52.692 |
|    |          |        |    |          |        | 16 | 29.528   | 52.750 |
|    |          |        |    |          |        | 17 | 68.242   | 52.750 |

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## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

## STATION 19

18 POINTS

X = 616.350

## STATION 20

21 POINTS

X = 660.375

## STATION 21

21 POINTS

X = 704.400

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | .328     | 15.941 | 2  | 0.000    | 3.188  | 2  | 0.000    | 2.811  |
| 3  | .820     | 20.868 | 3  | .820     | 11.593 | 3  | .820     | 4.898  |
| 4  | 1.640    | 26.085 | 4  | 1.640    | 16.028 | 4  | 1.640    | 8.202  |
| 5  | 3.281    | 31.592 | 5  | 3.281    | 22.317 | 5  | 3.281    | 13.187 |
| 6  | 4.921    | 35.505 | 6  | 4.921    | 27.201 | 6  | 4.921    | 17.245 |
| 7  | 6.562    | 38.548 | 7  | 6.562    | 31.302 | 7  | 6.562    | 21.390 |
| 8  | 8.202    | 41.070 | 8  | 8.202    | 34.229 | 8  | 8.202    | 24.694 |
| 9  | 9.842    | 42.954 | 9  | 9.842    | 36.867 | 9  | 9.842    | 28.085 |
| 10 | 11.483   | 44.780 | 10 | 11.483   | 39.041 | 10 | 11.483   | 30.665 |
| 11 | 13.123   | 46.142 | 11 | 13.123   | 40.925 | 11 | 13.123   | 33.215 |
| 12 | 16.404   | 48.547 | 12 | 16.404   | 44.113 | 12 | 16.404   | 37.041 |
| 13 | 19.685   | 50.141 | 13 | 19.685   | 46.634 | 13 | 19.685   | 40.229 |
| 14 | 22.966   | 51.243 | 14 | 22.966   | 48.402 | 14 | 22.966   | 42.606 |
| 15 | 26.247   | 51.938 | 15 | 26.247   | 49.707 | 15 | 26.247   | 44.664 |
| 16 | 29.528   | 52.460 | 16 | 29.528   | 50.750 | 16 | 29.528   | 46.374 |
| 17 | 32.808   | 52.750 | 17 | 32.808   | 51.620 | 17 | 32.808   | 47.765 |
| 18 | 39.370   | 52.750 | 18 | 39.370   | 52.199 | 18 | 39.370   | 49.852 |
|    |          |        | 19 | 45.932   | 52.750 | 19 | 45.932   | 51.388 |
|    |          |        | 20 | 52.493   | 52.750 | 20 | 52.493   | 52.605 |
|    |          |        | 21 | 68.242   | 52.750 | 21 | 68.242   | 52.750 |

## STATION 22

22 POINTS

X = 748.425

## STATION 23

22 POINTS

X = 770.437

## STATION 24

22 POINTS

X = 792.450

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  | 1  | 0.000    | 0.000  |
| 2  | 0.000    | 2.464  | 2  | 0.000    | 2.174  | 2  | 0.000    | 2.029  |
| 3  | .820     | 3.246  | 3  | .820     | 2.609  | 3  | .820     | 2.174  |
| 4  | 1.640    | 4.290  | 4  | 1.640    | 3.188  | 4  | 1.640    | 2.522  |
| 5  | 3.281    | 6.724  | 5  | 3.281    | 4.637  | 5  | 3.281    | 3.333  |
| 6  | 4.921    | 9.420  | 6  | 4.921    | 6.521  | 6  | 4.921    | 4.347  |
| 7  | 6.562    | 12.376 | 7  | 6.562    | 8.840  | 7  | 6.562    | 5.797  |
| 8  | 8.202    | 14.985 | 8  | 8.202    | 10.869 | 8  | 8.202    | 7.275  |
| 9  | 9.842    | 17.970 | 9  | 9.842    | 13.274 | 9  | 9.842    | 9.014  |
| 10 | 11.483   | 20.288 | 10 | 11.483   | 15.245 | 10 | 11.483   | 10.666 |
| 11 | 13.123   | 22.781 | 11 | 13.123   | 17.622 | 11 | 13.123   | 12.550 |
| 12 | 16.404   | 27.100 | 12 | 16.404   | 21.767 | 12 | 16.404   | 16.694 |
| 13 | 19.685   | 30.925 | 13 | 19.685   | 25.592 | 13 | 19.685   | 19.825 |
| 14 | 22.966   | 34.200 | 14 | 22.966   | 28.984 | 14 | 22.966   | 23.477 |
| 15 | 26.247   | 37.099 | 15 | 26.247   | 32.288 | 15 | 26.247   | 26.810 |
| 16 | 29.528   | 39.562 | 16 | 29.528   | 35.128 | 16 | 29.528   | 30.259 |
| 17 | 32.808   | 41.823 | 17 | 32.808   | 37.679 | 17 | 32.808   | 33.375 |
| 18 | 39.370   | 45.504 | 18 | 39.370   | 42.171 | 18 | 39.370   | 38.432 |
| 19 | 45.932   | 48.692 | 19 | 45.932   | 45.504 | 19 | 45.932   | 42.925 |
| 20 | 52.493   | 51.301 | 20 | 52.493   | 48.692 | 20 | 52.493   | 47.069 |
| 21 | 54.626   | 52.025 | 21 | 54.626   | 51.359 | 21 | 54.626   | 48.344 |
| 22 | 69.212   | 52.025 | 22 | 69.105   | 52.002 | 22 | 69.105   | 48.344 |

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## ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

## STATION 25

22 POINTS

X = 814.463

## STATION 26

15 POINTS

X = 836.475

## STATION 27

12 POINTS

X = 858.487

|    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |    | HEIGHT Z | H-B Y  |
|----|----------|--------|----|----------|--------|----|----------|--------|
| 1  | 0.000    | 0.000  | 1  | 11.024   | 0.000  | 1  | 16.404   | 0.000  |
| 2  | 0.000    | 1.594  | 2  | 11.024   | 3.072  | 2  | 16.404   | 2.753  |
| 3  | .820     | 1.739  | 3  | 11.483   | 3.623  | 3  | 19.685   | 3.739  |
| 4  | 1.640    | 1.971  | 4  | 13.123   | 4.492  | 4  | 22.966   | 5.507  |
| 5  | 3.281    | 2.522  | 5  | 16.404   | 6.376  | 5  | 26.247   | 8.463  |
| 6  | 4.921    | 3.130  | 6  | 19.685   | 8.840  | 6  | 29.528   | 12.028 |
| 7  | 6.562    | 4.000  | 7  | 22.966   | 11.535 | 7  | 32.808   | 16.173 |
| 8  | 8.202    | 4.782  | 8  | 26.247   | 14.955 | 8  | 39.370   | 23.766 |
| 9  | 9.842    | 5.884  | 9  | 29.528   | 18.549 | 9  | 45.932   | 29.998 |
| 10 | 11.483   | 6.956  | 10 | 32.808   | 22.317 | 10 | 52.463   | 35.447 |
| 11 | 13.123   | 8.289  | 11 | 39.370   | 29.042 | 11 | 54.626   | 37.099 |
| 12 | 16.404   | 11.159 | 12 | 45.932   | 34.780 | 12 | 68.898   | 37.099 |
| 13 | 19.685   | 14.318 | 13 | 52.493   | 36.693 |    |          |        |
| 14 | 22.966   | 17.535 | 14 | 54.626   | 41.475 |    |          |        |
| 15 | 26.247   | 21.013 | 15 | 68.635   | 41.475 |    |          |        |
| 16 | 29.528   | 24.491 |    |          |        |    |          |        |
| 17 | 32.808   | 28.027 |    |          |        |    |          |        |
| 18 | 39.370   | 33.911 |    |          |        |    |          |        |
| 19 | 45.932   | 39.273 |    |          |        |    |          |        |
| 20 | 52.493   | 44.055 |    |          |        |    |          |        |
| 21 | 54.626   | 45.301 |    |          |        |    |          |        |
| 22 | 68.537   | 45.301 |    |          |        |    |          |        |

## STATION 28

10 POINTS

X = 869.494

## STATION 29

9 POINTS

X = 880.500

## STATION 30

7 POINTS

X = 902.513

|    | HEIGHT Z | H-B Y  |   | HEIGHT Z | H-B Y  |   | HEIGHT Z | H-B Y  |
|----|----------|--------|---|----------|--------|---|----------|--------|
| 1  | 22.966   | 0.000  | 1 | 26.247   | 0.000  | 1 | 30.512   | 0.000  |
| 2  | 22.966   | 2.753  | 2 | 26.247   | 2.058  | 2 | 32.808   | 2.840  |
| 3  | 26.247   | 5.507  | 3 | 29.528   | 5.652  | 3 | 39.370   | 10.811 |
| 4  | 29.528   | 8.898  | 4 | 32.808   | 9.391  | 4 | 45.932   | 18.115 |
| 5  | 32.808   | 12.956 | 5 | 39.370   | 17.390 | 5 | 52.493   | 24.781 |
| 6  | 39.370   | 20.607 | 6 | 45.932   | 24.346 | 6 | 54.626   | 26.665 |
| 7  | 45.932   | 27.303 | 7 | 52.493   | 30.375 | 7 | 68.898   | 26.665 |
| 8  | 52.493   | 33.012 | 8 | 54.626   | 32.085 |   |          |        |
| 9  | 54.626   | 34.780 | 9 | 68.898   | 32.085 |   |          |        |
| 10 | 68.898   | 34.780 |   |          |        |   |          |        |

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ORIG.OFFSETS TABLE ( FEET ) SEA-LAND 7 CONTAINERSHIP

LENGTH = 880.500

BEAM = 105.500

DEPTH = 64.305

AFTER PROFILE

|   | HEIGHT Z | DIST X  |
|---|----------|---------|
| 1 | 0.000    | 814.463 |
| 2 | 11.024   | 836.475 |
| 3 | 16.404   | 858.487 |
| 4 | 22.966   | 869.494 |
| 5 | 26.247   | 880.500 |
| 6 | 30.512   | 902.513 |
| 7 | 68.898   | 902.513 |

FORWARD PROFILE

|   | HEIGHT Z | DIST X |
|---|----------|--------|
| 1 | 0.000    | 0.000  |
| 2 | 68.898   | 0.000  |

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## WEIGHT BLOCK DATA

## SL-7 - NORMAL FULL LOAD DEPARTURE

| WEIGHT<br>TYPE | BLOCK WEIGHT<br>(L.TONS) | BLOCK LCG<br>( FEET ) | FWD END BLOCK<br>( FEET ) | AFT END BLOCK<br>( FEET ) |
|----------------|--------------------------|-----------------------|---------------------------|---------------------------|
| 1              | 765.20                   | 19.00                 | -20.00                    | 42.00                     |
| 1              | 1847.70                  | 84.32                 | 42.00                     | 115.25                    |
| 1              | 1205.70                  | 143.18                | 115.25                    | 167.75                    |
| 1              | 1613.40                  | 185.52                | 167.75                    | 207.75                    |
| 1              | 1943.60                  | 225.50                | 207.75                    | 247.75                    |
| 1              | 2379.20                  | 265.54                | 247.75                    | 287.75                    |
| 1              | 2305.60                  | 305.53                | 287.75                    | 327.75                    |
| 1              | 2610.80                  | 345.53                | 327.75                    | 367.75                    |
| 1              | 3148.70                  | 385.52                | 367.75                    | 407.75                    |
| 1              | 3343.70                  | 425.51                | 407.75                    | 447.75                    |
| 1              | 3299.00                  | 467.99                | 447.75                    | 492.75                    |
| 1              | 3179.20                  | 512.99                | 492.75                    | 537.75                    |
| 1              | 3293.30                  | 550.00                | 537.75                    | 562.75                    |
| 1              | 3039.80                  | 587.50                | 562.75                    | 612.75                    |
| 1              | 2661.30                  | 635.00                | 612.75                    | 652.75                    |
| 1              | 2898.70                  | 674.35                | 652.75                    | 697.75                    |
| 1              | 2116.10                  | 716.10                | 697.75                    | 737.75                    |
| 1              | 1678.30                  | 756.40                | 737.75                    | 777.75                    |
| 1              | 1597.20                  | 795.55                | 777.75                    | 817.75                    |
| 1              | 1244.50                  | 835.50                | 817.75                    | 852.50                    |
| 1              | 897.70                   | 869.50                | 852.50                    | 880.50                    |
| 1              | 691.30                   | 900.50                | 880.50                    | 920.50                    |

| BLOCK<br>TYPE | SUMMARY WEIGHT<br>(L.TONS) | SUMMARY LCG<br>( FEET ) |
|---------------|----------------------------|-------------------------|
| 1             | 47760.00                   | 478.86                  |
| TOTAL         | 47760.00                   | 478.86                  |

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BALANCING OF SHIP

SL-7 - NORMAL FULL LOAD DEPARTURE

6 ITERATIONS TO BALANCE SHIP

|                        |   |            |         |
|------------------------|---|------------|---------|
| TRIM ( + BOW UP )      | = | .3685      | FEET    |
| HEEL ( + ST'BD. DOWN ) | = | 0.0000     | DEGREES |
| DRAFT FOWARD           | = | 32.5905    | FEET    |
| DRAFT AFT              | = | 32.9590    | FEET    |
| WEIGHT                 | = | 47760.0000 | L.TONS  |
| BUOYANCY               | = | 47760.0009 | L.TONS  |
| LCG (FROM F.P.)        | = | 478.8632   | FEET    |
| LCB (FROM F.P.)        | = | 478.8730   | FEET    |
| VCG (FROM B.L.)        | = | 42.3100    | FEET    |
| VCB (FROM B.L.)        | = | 18.2237    | FEET    |
| HCG (FROM C.L.)        | = | 0.0000     | FEET    |
| HCB (FROM C.L.)        | = | 0.0000     | FEET    |

## SHEAR FORCE-BENDING MOMENT

## SL-7 - NORMAL FULL LOAD DEPARTURE

| DISTANCE<br>FROM FP<br>( FEET ) | WEIGHT<br>FORCE | BUOYANCY<br>FORCE<br>( L.TONS ) | SHEAR<br>FORCE | WEIGHT<br>MOMENT | BUOYANCY<br>MOMENT | BENDING<br>MOMENT<br>( FEET -L.TONS ) |
|---------------------------------|-----------------|---------------------------------|----------------|------------------|--------------------|---------------------------------------|
| -20.00                          | 0.              | 0.                              | 0.0            | 0.               | 0.                 | 0.0                                   |
| 42.00                           | 7.652E+02       | 3.341E+02                       | 431.1          | 1.760E+04        | 6.573E+03          | 11026.3                               |
| 115.25                          | 2.613E+03       | 1.306E+03                       | 1306.9         | 1.308E+05        | 6.286E+04          | 67937.7                               |
| 167.75                          | 3.819E+03       | 2.499E+03                       | 1320.1         | 2.976E+05        | 1.604E+05          | 137245.7                              |
| 207.75                          | 5.432E+03       | 3.810E+03                       | 1622.2         | 4.862E+05        | 2.852E+05          | 201004.8                              |
| 247.75                          | 7.376E+03       | 5.531E+03                       | 1844.4         | 7.467E+05        | 4.706E+05          | 276150.1                              |
| 287.75                          | 9.755E+03       | 7.695E+03                       | 2059.7         | 1.095E+06        | 7.336E+05          | 361003.9                              |
| 327.75                          | 1.206E+04       | 1.031E+04                       | 1745.5         | 1.536E+06        | 1.092E+06          | 443706.9                              |
| 367.75                          | 1.467E+04       | 1.336E+04                       | 1314.0         | 2.076E+06        | 1.564E+06          | 512003.2                              |
| 407.75                          | 1.782E+04       | 1.674E+04                       | 1078.2         | 2.733E+06        | 2.165E+06          | 567887.8                              |
| 447.75                          | 2.116E+04       | 2.036E+04                       | 798.8          | 3.520E+06        | 2.907E+06          | 613574.3                              |
| 492.75                          | 2.446E+04       | 2.456E+04                       | -95.1          | 4.555E+06        | 3.917E+06          | 637055.1                              |
| 537.75                          | 2.764E+04       | 2.873E+04                       | -1092.0        | 5.734E+06        | 5.117E+06          | 617298.1                              |
| 562.75                          | 3.094E+04       | 3.101E+04                       | -75.2          | 6.467E+06        | 5.864E+06          | 603446.9                              |
| 612.75                          | 3.397E+04       | 3.539E+04                       | -1418.3        | 8.091E+06        | 7.525E+06          | 565641.1                              |
| 652.75                          | 3.664E+04       | 3.863E+04                       | -1991.5        | 9.497E+06        | 9.006E+06          | 490391.0                              |
| 697.75                          | 3.953E+04       | 4.182E+04                       | -2283.2        | 1.121E+07        | 1.082E+07          | 394648.7                              |
| 737.75                          | 4.165E+04       | 4.413E+04                       | -2478.0        | 1.284E+07        | 1.254E+07          | 301089.2                              |
| 777.75                          | 4.333E+04       | 4.588E+04                       | -2549.2        | 1.454E+07        | 1.434E+07          | 200883.5                              |
| 817.75                          | 4.493E+04       | 4.705E+04                       | -2124.0        | 1.631E+07        | 1.620E+07          | 109029.6                              |
| 852.50                          | 4.617E+04       | 4.758E+04                       | -1411.7        | 1.789E+07        | 1.785E+07          | 45847.6                               |
| 880.50                          | 4.707E+04       | 4.773E+04                       | -664.7         | 1.920E+07        | 1.918E+07          | 13612.7                               |
| 920.50                          | 4.776E+04       | 4.776E+04                       | -1.9           | 2.109E+07        | 2.109E+07          | -23.8                                 |

## HYDROSTATICS

## SL-7 - NORMAL FULL LOAD DEPARTURE

| STATION<br>FROM F.P. | MEAN DRAFT<br>( FEET ) | BEAM<br>( FEET ) | AREA<br>( FEET **2 ) | S.A. COEF. | VCB<br>( FEET ) | HCB<br>( FEET ) |
|----------------------|------------------------|------------------|----------------------|------------|-----------------|-----------------|
| 0.0000               | 32.5905                | 0.0000           | 222.324              | 1.00000    | 10.3399         | 0.0000          |
| 44.0250              | 32.6084                | 6.0099           | 337.108              | 1.72017    | 13.5076         | 0.0000          |
| 88.0500              | 32.6264                | 15.8877          | 496.078              | .95701     | 15.8027         | 0.0000          |
| 132.0750             | 32.6444                | 29.0487          | 720.049              | .75932     | 17.6532         | 0.0000          |
| 176.1000             | 32.6624                | 44.8461          | 1042.487             | .71170     | 18.6250         | 0.0000          |
| 220.1250             | 32.6803                | 60.5858          | 1429.605             | .72204     | 18.8288         | 0.0000          |
| 264.1500             | 32.6983                | 75.1694          | 1854.109             | .75434     | 18.5917         | 0.0000          |
| 308.1750             | 32.7163                | 87.5194          | 2298.414             | .80271     | 18.2402         | 0.0000          |
| 352.2000             | 32.7343                | 97.0852          | 2705.843             | .85143     | 17.8329         | 0.0000          |
| 396.2250             | 32.7523                | 103.1777         | 3022.527             | .89442     | 17.5017         | 0.0000          |
| 440.2500             | 32.7702                | 105.4993         | 3226.108             | .93315     | 17.2232         | 0.0000          |
| 484.2750             | 32.7882                | 105.5000         | 3272.334             | .94599     | 17.1294         | 0.0000          |
| 528.3000             | 32.8062                | 105.5000         | 3233.935             | .93438     | 17.2562         | 0.0000          |
| 572.3250             | 32.8242                | 105.5000         | 3132.758             | .90465     | 17.5684         | 0.0000          |
| 616.3500             | 32.8421                | 105.5000         | 2942.562             | .84926     | 18.1028         | 0.0000          |
| 660.3750             | 32.8601                | 103.2483         | 2633.081             | .77609     | 18.8959         | 0.0000          |
| 704.4000             | 32.8781                | 95.5739          | 2183.000             | .69472     | 19.8488         | 0.0000          |
| 748.4250             | 32.8961                | 83.7448          | 1649.810             | .59887     | 20.9084         | 0.0000          |
| 792.4500             | 32.9141                | 66.9123          | 1089.759             | .49482     | 22.0763         | 0.0000          |
| 836.4750             | 32.9320                | 44.8880          | 504.901              | .51341     | 25.0462         | 0.0000          |
| 880.5000             | 32.9500                | 19.1267          | 77.319               | .60306     | 30.3253         | 0.0000          |

|                                      |           |          |
|--------------------------------------|-----------|----------|
| VOLUME (MLD.)                        | 1670467.8 | FEET **3 |
| DISPLACEMENT (MLD.)                  | 47727.652 | L.TONS   |
| BLOCK COEFFICIENT (MLD.)             | .548756   |          |
| HALF-AREA MIDSHIP SECTION            | 1613.054  | FEET **2 |
| MIDSHIP SECTION COEFFICIENT          | .933146   |          |
| PRISMATIC COEFFICIENT (MLD.),        | .588071   |          |
| TRIM                                 | .369      | FEET     |
| HEEL                                 | 0.000     | DEGREES  |
| VCB (FROM B.L.)                      | 18.235    | FEET     |
| HCB (FROM C.L.)                      | 0.000     | FEET     |
| LCB (FROM F.P.)                      | 478.872   | FEET     |
| BM, TRANSVERSE                       | 26.964    | FEET     |
| BM, LONGITUDINAL                     | 1456.275  | FEET     |
| MOMENT TO ALTER TRIM 0.1 FEET        | 7893.761  |          |
| L.TONS PER 0.1 FEET IMMERSION        | 183.086   |          |
| AREA OF WATERPLANE                   | 64080.218 | FEET **2 |
| WATERPLANE COEFFICIENT (MLD.)        | .689835   |          |
| L.C.F. FROM F.P.                     | 500.541   | FEET     |
| CHANGE IN DISPL. FOR 1 FEET TRIM AFT | -125.366  | L.TONS   |
| WETTED SURFACE (MLD.)                | 99282.402 | FEET **2 |

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\*COEFFICIENT(DMAX=0.1, OUTPUT=TDPSSL7F)

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SL-7 - NORMAL FULL LOAD DEPARTURE  
 FRANK CLOSE FIT -21 POINTS

STATION 1  
 DRAFT = 32.590 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT  |
|-----------------------|---------|--------|-------------------|---------|-------|--------|---------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |        |         |
| .000                  | -32.590 | 1.933  | .933              | -32.338 | .2609 | .9654  | -7.536  |
| 1.866                 | -32.086 | 1.919  | 2.765             | -31.750 | .3505 | .9366  | -8.539  |
| 3.664                 | -31.413 | 1.914  | 4.418             | -30.825 | .6153 | .7883  | -15.484 |
| 5.172                 | -30.236 | 1.894  | 5.728             | -29.469 | .8096 | .5870  | -20.497 |
| 6.284                 | -28.703 | 1.930  | 6.559             | -27.778 | .9584 | .2855  | -24.748 |
| 6.835                 | -26.853 | 1.925  | 6.948             | -25.897 | .9930 | .1180  | -24.896 |
| 7.062                 | -24.941 | 1.922  | 6.929             | -23.990 | .9904 | -.1384 | -24.718 |
| 6.796                 | -23.038 | 1.932  | 6.518             | -22.113 | .9577 | -.2879 | -23.053 |
| 6.240                 | -21.188 | 1.933  | 5.853             | -20.302 | .9164 | -.4003 | -20.948 |
| 5.466                 | -19.417 | 1.933  | 5.026             | -18.556 | .8905 | -.4550 | -18.811 |
| 4.586                 | -17.695 | 1.933  | 4.152             | -16.832 | .8933 | -.4495 | -16.902 |
| 3.717                 | -15.968 | 1.933  | 3.321             | -15.087 | .9122 | -.4098 | -15.123 |
| 2.925                 | -14.205 | 1.932  | 2.547             | -13.316 | .9201 | -.3916 | -13.250 |
| 2.168                 | -12.427 | 1.933  | 1.840             | -11.518 | .9405 | -.3397 | -11.458 |
| 1.512                 | -10.609 | 1.931  | 1.221             | -9.688  | .9535 | -.3014 | -9.605  |
| .930                  | -8.767  | 1.933  | .682              | -7.832  | .9668 | -.2555 | -7.747  |
| .435                  | -6.898  | .964   | .369              | -6.421  | .9904 | -.1379 | -6.410  |
| .303                  | -5.943  | .964   | .236              | -5.466  | .9904 | -.1379 | -5.446  |
| .170                  | -4.989  | .967   | .127              | -4.507  | .9961 | -.0877 | -4.501  |
| .085                  | -4.026  | .967   | .042              | -3.544  | .9961 | -.0877 | -3.534  |
| 0.000                 | -3.063  |        |                   |         |       |        |         |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
FRANK CLOSE FIT -20 POINTS

STATION 1  
DRAFT = 32.590 FEET

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | .715   | 0.000  | 12.90    | 0.00     | 247.4  | 0.0    |
| .01             | .134     | -.000   | .716   | .000   | 12.92    | .00      | 247.3  | .0     |
| .03             | .134     | -.000   | .722   | .000   | 13.03    | .00      | 249.3  | .0     |
| .06             | .135     | .000    | .732   | .001   | 13.21    | .01      | 252.6  | .3     |
| .10             | .137     | .000    | .745   | .003   | 13.45    | .05      | 257.1  | 1.0    |
| .15             | .138     | .001    | .762   | .007   | 13.76    | .14      | 262.6  | 2.6    |
| .21             | .140     | .001    | .781   | .016   | 14.09    | .31      | 268.6  | 5.7    |
| .28             | .141     | .003    | .800   | .032   | 14.42    | .60      | 274.3  | 11.3   |
| .36             | .142     | .005    | .815   | .058   | 14.67    | 1.07     | 278.4  | 19.9   |
| .45             | .142     | .008    | .821   | .093   | 14.76    | 1.73     | 279.5  | 32.0   |
| .55             | .142     | .011    | .816   | .140   | 14.62    | 2.56     | 276.4  | 47.2   |
| .67             | .140     | .016    | .793   | .198   | 14.17    | 3.61     | 267.3  | 66.0   |
| .82             | .137     | .021    | .748   | .266   | 13.30    | 4.80     | 250.8  | 86.9   |
| 1.01            | .132     | .027    | .681   | .333   | 12.04    | 5.93     | 227.3  | 106.2  |
| 1.25            | .125     | .032    | .599   | .383   | 10.57    | 6.72     | 200.6  | 118.4  |
| 1.55            | .118     | .035    | .521   | .404   | 9.19     | 6.96     | 176.3  | 120.3  |
| 1.95            | .111     | .034    | .455   | .395   | 8.06     | 6.62     | 157.4  | 111.3  |
| 2.45            | .107     | .029    | .412   | .358   | 7.39     | 5.81     | 147.1  | 94.4   |
| 3.05            | .105     | .022    | .390   | .307   | 7.12     | 4.78     | 144.2  | 74.6   |
| 3.80            | .106     | .014    | .385   | .248   | 7.13     | 3.67     | 146.1  | 54.5   |
| 4.70            | .107     | .008    | .390   | .191   | 7.32     | 2.68     | 150.7  | 37.6   |
| 5.80            | .110     | .004    | .402   | .141   | 7.59     | 1.85     | 156.1  | 24.5   |
| 7.10            | .112     | .002    | .415   | .100   | 7.86     | 1.24     | 161.2  | 15.5   |
| 8.70            | .113     | .001    | .429   | .068   | 8.11     | .80      | 165.5  | 9.4    |
| 10.70           | .117     | 0.000   | .494   | 0.000  | 9.12     | 0.00     | 181.5  | 0.0    |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
 FRANK CLOSE FIT -21 POINTS

STATION 2  
 DRAFT = 32.608 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE   | COSINE  | MOMENT  |
|-----------------------|---------|--------|-------------------|---------|--------|---------|---------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |        |         |         |
| .000                  | -32.608 | 2.136  | 1.044             | -32.381 | .2133  | .9770   | -5.886  |
| 2.087                 | -32.153 | 2.121  | 3.108             | -31.865 | .2712  | .9625   | -5.651  |
| 4.129                 | -31.578 | 2.119  | 4.988             | -30.958 | .5852  | .8109   | -14.070 |
| 5.847                 | -30.338 | 2.107  | 6.512             | -29.520 | .7759  | .6309   | -18.795 |
| 7.177                 | -28.703 | 2.130  | 7.563             | -27.710 | .9318  | .3631   | -23.073 |
| 7.950                 | -26.718 | 2.123  | 8.088             | -25.665 | .9915  | .1304   | -24.392 |
| 8.227                 | -24.613 | 2.133  | 8.135             | -23.550 | .9963  | -.0856  | -24.160 |
| 8.044                 | -22.488 | 2.130  | 7.799             | -21.451 | .9731  | -.2303  | -22.671 |
| 7.554                 | -20.415 | 2.135  | 7.166             | -19.420 | .9317  | -.3633  | -20.697 |
| 6.778                 | -18.426 | 2.136  | 6.362             | -17.442 | .9210  | -.3895  | -18.542 |
| 5.946                 | -16.458 | 2.136  | 5.505             | -15.485 | .9107  | -.4130  | -16.376 |
| 5.064                 | -14.512 | 2.135  | 4.635             | -13.535 | .9159  | -.4014  | -14.257 |
| 4.206                 | -12.557 | 2.136  | 3.851             | -11.550 | .9432  | -.3323  | -12.173 |
| 3.496                 | -10.542 | 2.129  | 3.235             | -9.510  | .9695  | -.2453  | -10.013 |
| 2.974                 | -8.478  | 2.136  | 2.789             | -7.426  | .9848  | -.1735  | -7.797  |
| 2.604                 | -6.374  | 2.136  | 2.584             | -5.306  | .9998  | -.0185  | -5.353  |
| 2.564                 | -4.238  | 2.129  | 2.626             | -3.175  | .9983  | .0585   | -3.016  |
| 2.689                 | -2.113  | 2.136  | 2.847             | -1.056  | .9890  | .1481   | -.623   |
| 3.005                 | 0.000   | 1.502  | 2.254             | 0.000   | 0.0000 | -1.0000 | -2.254  |
| 1.502                 | 0.000   | 1.502  | .751              | 0.000   | 0.0000 | -1.0000 | -.751   |
| 0.000                 | 0.000   |        |                   |         |        |         |         |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
FRANK CLOSE FIT -20 POINTSSTATION 2  
DRAFT = 32.608 FEET

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.729  | 0.000  | 24.64    | 0.00     | 383.3  | 0.0    |
| .01             | .170     | .002    | 1.386  | .000   | 20.69    | .00      | 337.5  | .0     |
| .03             | .159     | .004    | 1.412  | .000   | 21.07    | .01      | 343.1  | .1     |
| .06             | .151     | .006    | 1.454  | .003   | 21.69    | .04      | 352.2  | .6     |
| .10             | .145     | .007    | 1.516  | .010   | 22.58    | .15      | 365.3  | 2.4    |
| .15             | .140     | .007    | 1.596  | .028   | 23.74    | .43      | 382.3  | 6.7    |
| .21             | .137     | .007    | 1.694  | .068   | 25.13    | 1.04     | 402.4  | 16.1   |
| .28             | .135     | .006    | 1.798  | .147   | 26.57    | 2.23     | 422.5  | 34.3   |
| .36             | .135     | .005    | 1.879  | .285   | 27.63    | 4.31     | 436.2  | 65.5   |
| .45             | .135     | .003    | 1.893  | .498   | 27.62    | 7.44     | 433.2  | 111.9  |
| .55             | .136     | .002    | 1.788  | .771   | 25.83    | 11.36    | 403.3  | 168.9  |
| .67             | .138     | .001    | 1.527  | 1.065  | 21.78    | 15.46    | 340.5  | 226.4  |
| .82             | .141     | - .000  | 1.141  | 1.288  | 16.03    | 18.35    | 254.6  | 263.6  |
| 1.01            | .143     | .000    | .752   | 1.361  | 10.44    | 18.91    | 174.2  | 265.1  |
| 1.25            | .144     | .002    | .469   | 1.296  | 6.56     | 17.44    | 121.3  | 236.8  |
| 1.55            | .144     | .005    | .307   | 1.158  | 4.55     | 14.96    | 97.2   | 195.0  |
| 1.95            | .143     | .008    | .232   | .989   | 3.86     | 12.07    | 92.8   | 148.7  |
| 2.45            | .141     | .009    | .216   | .822   | 4.03     | 9.34     | 100.5  | 107.0  |
| 3.05            | .139     | .009    | .233   | .673   | 4.62     | 7.01     | 113.1  | 73.7   |
| 3.80            | .138     | .007    | .267   | .539   | 5.40     | 5.07     | 127.2  | 48.0   |
| 4.70            | .138     | .004    | .307   | .429   | 6.19     | 3.60     | 140.0  | 30.4   |
| 5.80            | .139     | .002    | .347   | .341   | 6.91     | 2.54     | 150.8  | 19.0   |
| 7.10            | .139     | .001    | .383   | .273   | 7.49     | 1.83     | 159.0  | 12.2   |
| 8.70            | .140     | .000    | .415   | .220   | 7.97     | 1.34     | 165.4  | 8.1    |
| 10.70           | .141     | 0.000   | .571   | 0.000  | 9.85     | 0.00     | 188.2  | 0.0    |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
FRANK CLOSE FIT -21 POINTSSTATION 3  
DRAFT = 32.626 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |        | SINE    | COSINE  | MOMENT |
|-----------------------|---------|--------|-------------------|---------|--------|---------|---------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |        |         |         |        |
| .000                  | -32.626 | 2.188  | 1.077             | -32.435 | .1746  | .9846   | -4.603  |        |
| 2.154                 | -32.244 | 2.188  | 3.232             | -32.053 | .1746  | .9846   | -2.415  |        |
| 4.309                 | -31.862 | 2.169  | 5.277             | -31.374 | .4506  | .8927   | -9.425  |        |
| 6.245                 | -30.885 | 2.188  | 7.075             | -30.172 | .6520  | .7582   | -14.308 |        |
| 7.904                 | -29.458 | 2.181  | 8.536             | -28.569 | .8152  | .5792   | -18.345 |        |
| 9.167                 | -27.681 | 2.188  | 9.371             | -26.606 | .9825  | .1861   | -24.397 |        |
| 9.575                 | -25.531 | 2.174  | 9.644             | -24.446 | .9980  | .0639   | -23.780 |        |
| 9.713                 | -23.361 | 2.183  | 9.532             | -22.285 | .9860  | -.1666  | -23.561 |        |
| 9.350                 | -21.209 | 2.187  | 9.090             | -20.147 | .9715  | -.2372  | -21.728 |        |
| 8.831                 | -19.084 | 2.188  | 8.509             | -18.039 | .9556  | -.2947  | -19.745 |        |
| 8.186                 | -16.993 | 2.188  | 7.864             | -15.948 | .9556  | -.2947  | -17.557 |        |
| 7.542                 | -14.902 | 2.188  | 7.225             | -13.855 | .9571  | -.2898  | -15.354 |        |
| 6.908                 | -12.809 | 2.188  | 6.672             | -11.740 | .9766  | -.2151  | -12.901 |        |
| 6.437                 | -10.672 | 2.175  | 6.326             | -9.590  | .9947  | -.1024  | -10.187 |        |
| 6.214                 | -8.508  | 2.187  | 6.220             | -7.414  | 1.0000 | .0054   | -7.380  |        |
| 6.226                 | -6.321  | 2.188  | 6.444             | -5.249  | .9801  | .1986   | -3.865  |        |
| 6.661                 | -4.176  | 2.183  | 6.947             | -3.123  | .9651  | .2620   | -1.194  |        |
| 7.233                 | -2.069  | 2.188  | 7.588             | -1.035  | .9457  | .3249   | 1.487   |        |
| 7.944                 | 0.000   | 3.972  | 5.958             | 0.000   | 0.0000 | -1.0000 | -5.958  |        |
| 3.972                 | 0.000   | 3.972  | 1.986             | 0.000   | 0.0000 | -1.0000 | -1.986  |        |
| 0.000                 | 0.000   |        |                   |         |        |         |         |        |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
 FRANK CLOSE FIT -20 POINTS

STATION 3  
 DRAFT = 32.626 FEET

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.742  | 0.000  | 23.89    | 0.00     | 360.1  | 0.0    |
| .01             | .381     | .016    | 1.581  | .000   | 22.13    | .00      | 340.1  | .0     |
| .03             | .315     | .028    | 1.615  | .001   | 22.59    | .01      | 346.4  | .1     |
| .06             | .269     | .038    | 1.671  | .004   | 23.34    | .05      | 356.7  | .8     |
| .10             | .234     | .046    | 1.751  | .014   | 24.43    | .20      | 371.4  | 2.9    |
| .15             | .206     | .052    | 1.857  | .041   | 25.84    | .58      | 390.5  | 8.3    |
| .21             | .185     | .055    | 1.982  | .100   | 27.48    | 1.41     | 412.2  | 20.2   |
| .28             | .169     | .056    | 2.104  | .216   | 29.03    | 3.03     | 432.0  | 42.8   |
| .36             | .158     | .054    | 2.175  | .416   | 29.82    | 5.78     | 440.3  | 80.7   |
| .45             | .151     | .050    | 2.123  | .704   | 28.86    | 9.67     | 424.0  | 133.6  |
| .55             | .147     | .046    | 1.899  | 1.030  | 25.56    | 13.97    | 375.7  | 190.5  |
| .67             | .146     | .040    | 1.507  | 1.319  | 20.07    | 17.61    | 298.8  | 236.4  |
| .82             | .147     | .032    | 1.048  | 1.474  | 13.84    | 19.30    | 214.3  | 253.9  |
| 1.01            | .150     | .025    | .663   | 1.467  | 8.80     | 18.72    | 148.7  | 240.0  |
| 1.25            | .156     | .017    | .416   | 1.351  | 5.77     | 16.68    | 111.9  | 206.9  |
| 1.55            | .162     | .012    | .289   | 1.192  | 4.40     | 14.12    | 98.2   | 167.8  |
| 1.95            | .168     | .007    | .238   | 1.016  | 4.09     | 11.37    | 99.2   | 127.6  |
| 2.45            | .173     | .005    | .236   | .850   | 4.44     | 8.86     | 108.4  | 92.5   |
| 3.05            | .176     | .004    | .260   | .703   | 5.09     | 6.74     | 120.5  | 64.6   |
| 3.80            | .179     | .003    | .298   | .572   | 5.87     | 4.97     | 133.3  | 42.9   |
| 4.70            | .181     | .004    | .340   | .463   | 6.63     | 3.60     | 144.7  | 27.7   |
| 5.80            | .183     | .005    | .381   | .373   | 7.32     | 2.58     | 154.4  | 17.6   |
| 7.10            | .183     | .006    | .419   | .302   | 7.89     | 1.87     | 161.8  | 11.3   |
| 8.70            | .184     | .006    | .452   | .244   | 8.36     | 1.36     | 167.7  | 7.3    |
| 10.70           | .187     | 0.000   | .624   | 0.000  | 10.27    | 0.00     | 189.0  | 0.0    |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 7 COEFFICIENTSSTATION 4  
DRAFT = 32.644 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT  |
|-----------------------|---------|--------|-------------------|---------|-------|--------|---------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |        |         |
| .000                  | -32.644 | 2.242  | 1.121             | -32.619 | .0227 | .9997  | .381    |
| 2.242                 | -32.594 | 2.231  | 3.339             | -32.394 | .1790 | .9839  | -2.511  |
| 4.437                 | -32.194 | 1.109  | 4.959             | -32.007 | .3373 | .9414  | -6.129  |
| 5.481                 | -31.820 | 1.109  | 6.003             | -31.633 | .3373 | .9414  | -5.020  |
| 6.525                 | -31.446 | 2.233  | 7.389             | -30.739 | .6331 | .7740  | -13.743 |
| 8.253                 | -30.033 | 2.229  | 8.960             | -29.171 | .7733 | .6341  | -16.876 |
| 9.666                 | -28.309 | 2.229  | 10.129            | -27.295 | .9097 | .4153  | -20.623 |
| 10.592                | -26.282 | 2.239  | 10.807            | -25.183 | .9814 | .1921  | -22.637 |
| 11.022                | -24.084 | 2.236  | 11.164            | -22.975 | .9919 | .1267  | -21.375 |
| 11.306                | -21.866 | 2.241  | 11.291            | -20.746 | .9999 | -.0131 | -20.892 |
| 11.276                | -19.625 | 2.242  | 11.227            | -18.505 | .9990 | -.0436 | -18.977 |
| 11.179                | -17.385 | 2.242  | 11.139            | -16.264 | .9994 | -.0354 | -16.649 |
| 11.099                | -15.144 | 2.242  | 11.073            | -14.023 | .9997 | -.0235 | -14.280 |
| 11.046                | -12.902 | 2.242  | 11.145            | -11.786 | .9961 | .0877  | -10.762 |
| 11.243                | -10.669 | 2.236  | 11.436            | -9.567  | .9850 | .1727  | -7.448  |
| 11.629                | -8.466  | 2.242  | 11.901            | -7.379  | .9702 | .2423  | -4.276  |
| 12.173                | -6.291  | 2.242  | 12.503            | -5.219  | .9556 | .2947  | -1.303  |
| 12.833                | -4.148  | 2.239  | 13.227            | -3.100  | .9362 | .3515  | 1.747   |
| 13.620                | -2.052  | 2.242  | 14.072            | -1.026  | .9151 | .4031  | 4.734   |
| 14.524                | 0.000   |        |                   |         |       |        |         |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00 INFINITY    | 0.000    | 1.668   | 0.000  | 19.69  | 0.00     | 266.1    | 0.0    |        |
| .01 .989        | .067     | 1.685   | .000   | 19.87  | .00      | 268.1    | .0     |        |
| .03 .727        | .109     | 1.725   | .001   | 20.31  | .01      | 273.0    | .1     |        |
| .06 .563        | .143     | 1.791   | .005   | 21.04  | .06      | 281.2    | .7     |        |
| .10 .447        | .168     | 1.885   | .019   | 22.08  | .23      | 292.7    | 2.7    |        |
| .15 .361        | .186     | 2.006   | .055   | 23.39  | .65      | 307.1    | 7.6    |        |
| .21 .297        | .197     | 2.141   | .135   | 24.82  | 1.56     | 322.2    | 18.2   |        |
| .28 .249        | .201     | 2.252   | .286   | 25.92  | 3.28     | 333.0    | 37.8   |        |
| .36 .215        | .200     | 2.270   | .529   | 25.91  | 6.00     | 330.6    | 68.3   |        |
| .45 .190        | .195     | 2.123   | .844   | 24.03  | 9.43     | 306.8    | 105.8  |        |
| .55 .174        | .186     | 1.805   | 1.149  | 20.29  | 12.63    | 263.0    | 139.4  |        |
| .67 .163        | .173     | 1.374   | 1.370  | 15.43  | 14.77    | 208.2    | 159.8  |        |
| .82 .159        | .157     | .948    | 1.452  | 10.78  | 15.27    | 157.8    | 161.2  |        |
| 1.01 .160       | .138     | .623    | 1.406  | 7.41   | 14.34    | 123.1    | 146.5  |        |
| 1.25 .166       | .116     | .422    | 1.285  | 5.50   | 12.59    | 105.7    | 123.4  |        |
| 1.55 .177       | .095     | .320    | 1.135  | 4.72   | 10.58    | 100.9    | 98.5   |        |
| 1.95 .190       | .075     | .281    | .972   | 4.66   | 8.47     | 103.9    | 73.5   |        |
| 2.45 .204       | .058     | .283    | .817   | 5.03   | 6.54     | 111.2    | 52.0   |        |
| 3.05 .219       | .043     | .305    | .679   | 5.59   | 4.93     | 120.1    | 35.7   |        |
| 3.80 .230       | .034     | .343    | .552   | 6.25   | 3.55     | 128.7    | 22.7   |        |
| 4.70 .239       | .027     | .384    | .444   | 6.88   | 2.48     | 136.2    | 13.8   |        |
| 5.80 .246       | .021     | .425    | .352   | 7.45   | 1.69     | 142.4    | 8.0    |        |
| 7.10 .251       | .017     | .463    | .278   | 7.92   | 1.14     | 147.2    | 4.6    |        |
| 8.70 .256       | .014     | .497    | .218   | 8.31   | .75      | 150.9    | 2.5    |        |
| 10.70 .260      | .010     | .528    | .166   | 8.63   | .47      | 153.8    | 1.3    |        |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 5  
DRAFT = 32.662 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE  | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|---------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |         |        |
| .000                  | -32.662 | 2.408  | 1.203             | -32.626 | .0302 | .9995 | .216    |        |
| 2.407                 | -32.590 | 2.398  | 3.602             | -32.499 | .0754 | .9972 | 1.142   |        |
| 4.798                 | -32.409 | 2.405  | 5.956             | -32.086 | .2688 | .9632 | -2.888  |        |
| 7.114                 | -31.762 | 1.195  | 7.641             | -31.479 | .4734 | .8808 | -8.172  |        |
| 8.167                 | -31.196 | 1.195  | 8.693             | -30.914 | .4734 | .8808 | -6.977  |        |
| 9.220                 | -30.631 | 2.398  | 10.098            | -29.815 | .6803 | .7329 | -12.881 |        |
| 10.977                | -29.000 | 2.404  | 11.654            | -28.006 | .8262 | .5634 | -16.573 |        |
| 12.332                | -27.013 | 2.404  | 12.870            | -25.938 | .8943 | .4474 | -17.438 |        |
| 13.407                | -24.863 | 2.406  | 13.880            | -23.757 | .9197 | .3927 | -16.397 |        |
| 14.352                | -22.651 | 2.406  | 14.694            | -21.497 | .9588 | .2840 | -16.438 |        |
| 15.036                | -20.344 | 2.407  | 15.406            | -19.199 | .9514 | .3081 | -13.519 |        |
| 15.777                | -18.054 | 2.408  | 16.132            | -16.903 | .9556 | .2947 | -11.399 |        |
| 16.487                | -15.753 | 2.408  | 16.841            | -14.602 | .9556 | .2947 | -8.991  |        |
| 17.196                | -13.452 | 2.408  | 17.551            | -12.301 | .9556 | .2946 | -6.584  |        |
| 17.906                | -11.151 | 2.405  | 18.302            | -10.016 | .9440 | .3299 | -3.417  |        |
| 18.699                | -8.881  | 2.408  | 19.168            | -7.772  | .9210 | .3895 | .308    |        |
| 19.637                | -6.663  | 2.408  | 20.083            | -5.545  | .9287 | .3709 | 2.299   |        |
| 20.530                | -4.427  | 2.407  | 20.991            | -3.315  | .9237 | .3832 | 4.982   |        |
| 21.452                | -2.203  | 2.408  | 21.938            | -1.102  | .9151 | .4031 | 7.835   |        |
| 22.423                | 0.000   |        |                   |         |       |       |         |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.563  | 0.000  | 12.31    | 0.00     | 127.4  | 0.0    |
| .01             | 2.230    | .158    | 1.578  | .000   | 12.42    | .00      | 128.2  | .0     |
| .03             | 1.613    | .255    | 1.616  | .001   | 12.68    | .01      | 130.0  | .1     |
| .06             | 1.234,   | .330    | 1.678  | .006   | 13.11    | .04      | 133.0  | .3     |
| .10             | .972     | .387    | 1.765  | .021   | 13.70    | .16      | 137.1  | 1.2    |
| .15             | .782     | .427    | 1.871  | .060   | 14.40    | .45      | 141.7  | 3.4    |
| .21             | .642     | .452    | 1.976  | .141   | 15.06    | 1.04     | 145.8  | 7.7    |
| .28             | .538     | .464    | 2.041  | .284   | 15.38    | 2.06     | 147.2  | 14.9   |
| .36             | .460     | .466    | 2.012  | .493   | 15.00    | 3.50     | 143.4  | 24.9   |
| .45             | .404     | .458    | 1.854  | .739   | 13.71    | 5.13     | 133.3  | 35.7   |
| .55             | .365     | .443    | 1.591  | .962   | 11.75    | 6.52     | 119.0  | 44.2   |
| .67             | .338     | .420    | 1.268  | 1.124  | 9.47     | 7.40     | 103.1  | 48.6   |
| .82             | .321     | .389    | .950   | 1.199  | 7.34     | 7.60     | 89.2   | 48.1   |
| 1.01            | .317     | .350    | .694   | 1.188  | 5.74     | 7.18     | 79.6   | 43.3   |
| 1.25            | .324     | .304    | .519   | 1.116  | 4.79     | 6.34     | 74.9   | 36.0   |
| 1.55            | .340     | .255    | .417   | 1.011  | 4.37     | 5.32     | 74.0   | 27.9   |
| 1.95            | .366     | .204    | .367   | .885   | 4.34     | 4.19     | 75.5   | 19.8   |
| 2.45            | .394     | .158    | .356   | .756   | 4.55     | 3.14     | 78.5   | 13.0   |
| 3.05            | .422     | .121    | .368   | .635   | 4.89     | 2.25     | 81.6   | 7.9    |
| 3.80            | .449     | .090    | .395   | .522   | 5.27     | 1.51     | 84.6   | 4.4    |
| 4.70            | .473     | .063    | .427   | .417   | 5.62     | .95      | 87.1   | 2.1    |
| 5.80            | .492     | .045    | .462   | .330   | 5.94     | .56      | 89.0   | .9     |
| 7.10            | .507     | .032    | .495   | .260   | 6.20     | .31      | 90.4   | .4     |
| 8.70            | .520     | .022    | .525   | .202   | 6.40     | .15      | 91.4   | .1     |
| 10.70           | .531     | .014    | .553   | .152   | 6.57     | .06      | 92.2   | .0     |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 6  
DRAFT = 32.680 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|--------|--------|
| H-BRDT                | HEIGHT  | LENGTH | H-BRDT            | HEIGHT  |       |        |        |
| .000                  | -32.680 | 2.686  | 1.342             | -32.619 | .0454 | .9990  | -.140  |
| 2.683                 | -32.558 | 2.683  | 4.021             | -32.452 | .0793 | .9968  | 1.434  |
| 5.358                 | -32.346 | 1.343  | 6.023             | -32.256 | .1336 | .9910  | 1.661  |
| 6.689                 | -32.166 | 1.343  | 7.354             | -32.077 | .1336 | .9910  | 3.004  |
| 8.020                 | -31.987 | 2.662  | 9.286             | -31.576 | .3086 | .9512  | -.913  |
| 10.552                | -31.165 | 2.682  | 11.682            | -30.444 | .5381 | .8429  | -6.533 |
| 12.812                | -29.722 | 2.684  | 13.871            | -28.898 | .6141 | .7892  | -6.799 |
| 14.931                | -28.074 | 2.684  | 15.899            | -27.146 | .6920 | .7219  | -7.307 |
| 16.868                | -26.217 | 2.684  | 17.665            | -25.138 | .8043 | .5942  | -9.723 |
| 18.463                | -24.058 | 2.678  | 19.187            | -22.932 | .8411 | .5409  | -8.908 |
| 19.912                | -21.805 | 2.686  | 20.563            | -20.631 | .8743 | .4853  | -8.059 |
| 21.215                | -19.457 | 2.686  | 21.882            | -18.292 | .8678 | .4969  | -4.999 |
| 22.550                | -17.126 | 2.684  | 23.154            | -15.928 | .8928 | .4504  | -3.793 |
| 23.758                | -14.730 | 2.686  | 24.319            | -13.510 | .9087 | .4174  | -2.127 |
| 24.879                | -12.290 | 2.686  | 25.421            | -11.061 | .9152 | .4031  | .125   |
| 25.962                | -9.832  | 2.686  | 26.503            | -8.603  | .9151 | .4031  | 2.811  |
| 27.045                | -7.374  | 2.686  | 27.586            | -6.145  | .9151 | .4031  | 5.497  |
| 28.127                | -4.916  | 2.686  | 28.669            | -3.687  | .9151 | .4031  | 8.183  |
| 29.210                | -2.458  | 2.686  | 29.752            | -1.229  | .9151 | .4031  | 10.869 |
| 30.293                | 0.000   |        |                   |         |       |        |        |

| FREQ.  | A'       | N'    | M     | N     | M    | N    | I    | N   |
|--------|----------|-------|-------|-------|------|------|------|-----|
| PARAM. | 33       | Z     | S     | S     | S.R  | S.R  | R    | R   |
| .00    | INFINITY | 0.000 | 1.518 | 0.000 | 3.30 | 0.00 | 25.6 | 0.0 |
| .01    | 4.001    | .290  | 1.535 | .000  | 3.33 | .00  | 25.6 | .0  |
| .03    | 2.868    | .461  | 1.575 | .001  | 3.38 | .00  | 25.7 | .0  |
| .06    | 2.187    | .590  | 1.640 | .007  | 3.47 | .01  | 25.8 | .0  |
| .10    | 1.726    | .684  | 1.729 | .026  | 3.59 | .05  | 26.0 | .1  |
| .15    | 1.399    | .747  | 1.830 | .072  | 3.70 | .13  | 26.1 | .2  |
| .21    | 1.162    | .785  | 1.916 | .163  | 3.76 | .28  | 26.2 | .5  |
| .28    | .988     | .802  | 1.944 | .313  | 3.70 | .50  | 26.0 | .8  |
| .36    | .862     | .800  | 1.869 | .513  | 3.46 | .77  | 25.5 | 1.2 |
| .45    | .771     | .784  | 1.685 | .725  | 3.08 | 1.00 | 24.9 | 1.4 |
| .55    | .710     | .755  | 1.433 | .902  | 2.64 | 1.13 | 24.3 | 1.4 |
| .67    | .667     | .715  | 1.154 | 1.024 | 2.24 | 1.13 | 23.8 | 1.2 |
| .82    | .644     | .660  | .891  | 1.079 | 1.93 | .99  | 23.6 | .9  |
| 1.01   | .639     | .591  | .678  | 1.071 | 1.77 | .75  | 23.7 | .5  |
| 1.25   | .654     | .513  | .529  | 1.015 | 1.74 | .44  | 23.9 | .2  |
| 1.55   | .685     | .429  | .438  | .930  | 1.81 | .13  | 24.0 | .0  |
| 1.95   | .730     | .339  | .387  | .822  | 1.96 | -.18 | 24.6 | .0  |
| 2.45   | .781     | .259  | .373  | .708  | 2.14 | -.43 | 24.8 | .3  |
| 3.05   | .831     | .193  | .381  | .598  | 2.32 | -.59 | 24.8 | .6  |
| 3.80   | .877     | .139  | .404  | .493  | 2.47 | -.68 | 24.7 | .9  |
| 4.70   | .917     | .099  | .432  | .399  | 2.59 | -.69 | 24.6 | 1.2 |
| 5.80   | .951     | .068  | .464  | .318  | 2.68 | -.64 | 24.5 | 1.3 |
| 7.10   | .978     | .047  | .493  | .251  | 2.73 | -.56 | 24.3 | 1.3 |
| 8.70   | 1.000    | .031  | .522  | .194  | 2.76 | -.46 | 24.3 | 1.1 |
| 10.70  | 1.018    | .020  | .547  | .148  | 2.77 | -.36 | 24.2 | .9  |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 7  
DRAFT = 32.698 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |        |        |
| .000                  | -32.698 | 3.033  | 1.516             | -32.643 | .0363 | .9993  | .330   |
| 3.031                 | -32.588 | 3.033  | 4.547             | -32.533 | .0363 | .9993  | 3.363  |
| 6.062                 | -32.478 | 3.031  | 7.573             | -32.355 | .0815 | .9967  | 4.911  |
| 9.083                 | -32.231 | 3.033  | 10.591            | -32.065 | .1096 | .9940  | 7.013  |
| 12.098                | -31.899 | 3.027  | 13.535            | -31.424 | .3139 | .9495  | 2.989  |
| 14.972                | -30.949 | 1.517  | 15.658            | -30.624 | .4275 | .9040  | 1.062  |
| 16.343                | -30.300 | 1.517  | 17.029            | -29.976 | .4275 | .9040  | 2.578  |
| 17.714                | -29.652 | 3.028  | 18.995            | -28.845 | .5331 | .8461  | .695   |
| 20.276                | -28.037 | 3.032  | 21.484            | -27.120 | .6049 | .7963  | .701   |
| 22.691                | -26.203 | 3.031  | 23.711            | -25.083 | .7394 | .6732  | -2.584 |
| 24.731                | -23.962 | 3.027  | 25.632            | -22.745 | .8038 | .5949  | -3.036 |
| 26.532                | -21.528 | 3.033  | 27.389            | -20.277 | .8251 | .5649  | -1.259 |
| 28.245                | -19.026 | 3.033  | 29.066            | -17.751 | .8411 | .5409  | .793   |
| 29.886                | -16.475 | 3.033  | 30.620            | -15.148 | .8752 | .4838  | 1.557  |
| 31.353                | -13.821 | 3.032  | 32.014            | -12.457 | .9000 | .4358  | 2.740  |
| 32.674                | -11.092 | 3.033  | 33.311            | -9.716  | .9076 | .4198  | 5.167  |
| 33.948                | -8.340  | 3.032  | 34.570            | -6.957  | .9119 | .4105  | 7.847  |
| 35.193                | -5.574  | 3.033  | 35.777            | -4.175  | .9227 | .3855  | 9.939  |
| 36.362                | -2.776  | 3.033  | 36.973            | -1.388  | .9151 | .4031  | 13.636 |
| 37.585                | 0.000   |        |                   |         |       |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.558  | 0.000  | -5.66    | 0.00     | 28.8   | 0.0    |
| .01             | 6.037    | .444    | 1.577  | .000   | -5.74    | -.00     | 29.1   | .0     |
| .03             | 4.295    | .698    | 1.624  | .002   | -5.92    | -.01     | 29.9   | .0     |
| .06             | 3.266    | .884    | 1.698  | .009   | -6.21    | -.04     | 31.1   | .1     |
| .10             | 2.583    | 1.014   | 1.797  | .034   | -6.61    | -.13     | 32.6   | .5     |
| .15             | 2.107    | 1.097   | 1.902  | .092   | -7.03    | -.35     | 34.4   | 1.3    |
| .21             | 1.768    | 1.142   | 1.975  | .202   | -7.35    | -.78     | 35.8   | 3.0    |
| .28             | 1.526    | 1.155   | 1.966  | .371   | -7.36    | -1.44    | 36.0   | 5.6    |
| .36             | 1.353    | 1.142   | 1.841  | .579   | -6.92    | -2.27    | 34.5   | 9.0    |
| .45             | 1.235    | 1.109   | 1.617  | .780   | -6.07    | -3.10    | 31.3   | 12.3   |
| .55             | 1.157    | 1.059   | 1.351  | .932   | -5.05    | -3.75    | 27.4   | 15.1   |
| .67             | 1.108    | .991    | 1.082  | 1.028  | -3.98    | -4.19    | 23.1   | 17.2   |
| .82             | 1.087    | .905    | .839   | 1.065  | -3.00    | -4.42    | 19.2   | 18.4   |
| 1.01            | 1.094    | .800    | .648   | 1.050  | -2.19    | -4.44    | 15.7   | 19.0   |
| 1.25            | 1.128    | .683    | .513   | .994   | -1.59    | -4.31    | 13.1   | 18.8   |
| 1.55            | 1.183    | .562    | .430   | .912   | -1.18    | -4.06    | 11.1   | 18.3   |
| 1.95            | 1.256    | .440    | .385   | .809   | -.91     | -3.71    | 9.7    | 17.2   |
| 2.45            | 1.334    | .331    | .373   | .698   | -.79     | -3.30    | 8.8    | 15.8   |
| 3.05            | 1.408    | .244    | .383   | .592   | -.76     | -2.87    | 8.3    | 14.2   |
| 3.80            | 1.477    | .169    | .404   | .486   | -.80     | -2.40    | 8.3    | 11.9   |
| 4.70            | 1.533    | .117    | .433   | .394   | -.89     | -1.97    | 8.5    | 9.9    |
| 5.80            | 1.581    | .079    | .464   | .314   | -1.00    | -1.57    | 8.9    | 7.9    |
| 7.10            | 1.618    | .053    | .494   | .248   | -1.12    | -1.23    | 9.4    | 6.1    |
| 8.70            | 1.648    | .035    | .522   | .194   | -1.25    | -.93     | 9.9    | 4.5    |
| 10.70           | 1.674    | .021    | .548   | .145   | -1.37    | -.67     | 10.5   | 3.1    |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTS

STATION 8  
DRAFT = 32.716 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |        |        |
| .000                  | -32.716 | 3.397  | 1.698             | -32.668 | .0284 | .9996 | .770   |        |
| 3.395                 | -32.620 | 3.397  | 5.093             | -32.572 | .0284 | .9996 | 4.167  |        |
| 6.790                 | -31.524 | 3.397  | 8.488             | -32.475 | .0284 | .9996 | 7.563  |        |
| 10.185                | -32.427 | 3.395  | 11.880            | -32.320 | .0632 | .9980 | 9.812  |        |
| 13.574                | -32.213 | 3.397  | 15.266            | -32.065 | .0870 | .9962 | 12.419 |        |
| 16.957                | -31.917 | 1.696  | 17.779            | -31.706 | .2491 | .9685 | 9.319  |        |
| 18.600                | -31.494 | 1.696  | 19.422            | -31.283 | .2491 | .9685 | 11.016 |        |
| 20.243                | -31.072 | 3.397  | 21.825            | -30.453 | .3645 | .9312 | 9.224  |        |
| 23.406                | -29.834 | 3.383  | 24.889            | -29.020 | .4809 | .8767 | 7.864  |        |
| 26.373                | -28.207 | 3.396  | 27.769            | -27.242 | .5685 | .8227 | 7.360  |        |
| 29.166                | -26.276 | 3.393  | 30.432            | -25.147 | .6658 | .7462 | 5.966  |        |
| 31.698                | -24.017 | 3.392  | 32.813            | -22.739 | .7538 | .6571 | 4.420  |        |
| 33.927                | -21.460 | 3.390  | 34.953            | -20.111 | .7962 | .6051 | 5.138  |        |
| 35.978                | -18.761 | 3.395  | 36.850            | -17.305 | .8581 | .5135 | 4.075  |        |
| 37.722                | -15.848 | 3.395  | 38.473            | -14.326 | .8967 | .4426 | 4.183  |        |
| 39.225                | -12.803 | 3.397  | 39.837            | -11.219 | .9326 | .3609 | 3.914  |        |
| 40.450                | -9.636  | 3.397  | 41.039            | -8.043  | .9379 | .3469 | 6.691  |        |
| 41.628                | -6.450  | 3.397  | 42.168            | -4.840  | .9483 | .3175 | 8.798  |        |
| 42.707                | -3.229  | 3.397  | 43.233            | -1.615  | .9507 | .3100 | 11.867 |        |
| 43.760                | 0.000   |        |                   |         |       |       |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.637  | 0.000  | -13.39   | 0.00     | 141.0  | 0.0    |
| .01             | 8.078    | .601    | 1.660  | .000   | -13.57   | -.00     | 142.4  | .0     |
| .03             | 5.715    | .935    | 1.716  | .002   | -14.01   | -.02     | 146.0  | .2     |
| .06             | 4.338    | 1.171   | 1.805  | .012   | -14.71   | -.10     | 151.5  | .9     |
| .10             | 3.439    | 1.329   | 1.920  | .044   | -15.60   | -.36     | 158.4  | 3.0    |
| .15             | 2.823    | 1.422   | 2.035  | .118   | -16.46   | -.97     | 164.8  | 7.9    |
| .21             | 2.393    | 1.464   | 2.098  | .255   | -16.86   | -2.06    | 167.3  | 16.7   |
| .28             | 2.092    | 1.463   | 2.049  | .455   | -16.35   | -3.63    | 162.4  | 29.1   |
| .36             | 1.885    | 1.427   | 1.866  | .682   | -14.79   | -5.38    | 149.1  | 42.5   |
| .45             | 1.750    | 1.365   | 1.591  | .884   | -12.53   | -6.86    | 130.7  | 53.4   |
| .55             | 1.669    | 1.283   | 1.296  | 1.024  | -10.19   | -7.82    | 112.2  | 59.9   |
| .67             | 1.629    | 1.178   | 1.014  | 1.103  | -8.03    | -8.28    | 95.6   | 62.3   |
| .82             | 1.627    | 1.049   | .772   | 1.125  | -6.22    | -8.26    | 82.3   | 60.9   |
| 1.01            | 1.663    | .900    | .584   | 1.096  | -4.90    | -7.85    | 73.1   | 56.5   |
| 1.25            | 1.733    | .740    | .455   | 1.030  | -4.06    | -7.16    | 67.8   | 50.1   |
| 1.55            | 1.827    | .583    | .377   | .939   | -3.63    | -6.32    | 65.7   | 42.8   |
| 1.95            | 1.940    | .430    | .338   | .826   | -3.51    | -5.34    | 65.9   | 34.8   |
| 2.45            | 2.054    | .304    | .332   | .707   | -3.62    | -4.38    | 67.7   | 27.4   |
| 3.05            | 2.154    | .209    | .347   | .594   | -3.85    | -3.51    | 70.1   | 21.0   |
| 3.80            | 2.244    | .133    | .375   | .479   | -4.15    | -2.68    | 72.9   | 15.0   |
| 4.70            | 2.314    | .085    | .409   | .383   | -4.46    | -2.02    | 75.5   | 10.7   |
| 5.80            | 2.371    | .053    | .444   | .301   | -4.76    | -1.49    | 77.9   | 7.4    |
| 7.10            | 2.415    | .032    | .477   | .235   | -5.02    | -1.08    | 79.9   | 5.0    |
| 8.70            | 2.450    | .019    | .507   | .181   | -5.26    | -.76     | 81.5   | 3.3    |
| 10.70           | 2.478    | .011    | .535   | .134   | -5.46    | -.51     | 82.9   | 2.0    |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 9  
DRAFT = 32.734 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |        |        |
| .000                  | -32.734 | 3.742  | 1.870             | -32.696 | .0203 | .9998 | 1.205  |        |
| 3.741                 | -32.658 | 3.742  | 5.611             | -32.620 | .0203 | .9998 | 4.947  |        |
| 7.482                 | -32.582 | 3.742  | 9.352             | -32.544 | .0203 | .9998 | 8.689  |        |
| 11.223                | -32.506 | 3.742  | 13.093            | -32.468 | .0203 | .9998 | 12.430 |        |
| 14.963                | -32.430 | 3.742  | 16.834            | -32.392 | .0203 | .9998 | 16.172 |        |
| 18.704                | -32.354 | 3.740  | 20.567            | -32.186 | .0899 | .9959 | 17.589 |        |
| 22.429                | -32.018 | 3.738  | 24.268            | -31.683 | .1792 | .9838 | 18.196 |        |
| 26.106                | -31.348 | 3.730  | 27.878            | -30.764 | .3130 | .9497 | 16.846 |        |
| 29.649                | -30.180 | 1.860  | 30.477            | -29.756 | .4563 | .8898 | 13.542 |        |
| 31.304                | -29.331 | 1.860  | 32.132            | -28.907 | .4563 | .8898 | 15.402 |        |
| 32.959                | -28.483 | 3.741  | 34.533            | -27.472 | .5405 | .8413 | 14.206 |        |
| 36.107                | -26.461 | 3.731  | 37.486            | -25.204 | .6736 | .7391 | 10.729 |        |
| 38.865                | -23.947 | 3.730  | 40.028            | -22.489 | .7817 | .6236 | 7.383  |        |
| 41.191                | -21.031 | 3.738  | 42.154            | -19.429 | .8572 | .5151 | 5.058  |        |
| 43.116                | -17.827 | 3.735  | 43.900            | -16.132 | .9076 | .4199 | 3.790  |        |
| 44.684                | -14.438 | 3.739  | 45.291            | -12.669 | .9459 | .3244 | 2.708  |        |
| 45.897                | -10.901 | 3.741  | 46.419            | -9.104  | .9604 | .2787 | 4.196  |        |
| 46.940                | -7.308  | 3.740  | 47.343            | -5.482  | .9766 | .2153 | 4.838  |        |
| 47.745                | -3.656  | 3.742  | 48.144            | -1.828  | .9770 | .2131 | 8.473  |        |
| 48.543                | 0.000   |        |                   |         |       |       |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.748  | 0.000  | -18.74   | 0.00     | 352.0  | 0.0    |
| .01             | 9.917    | .743    | 1.775  | .000   | -19.03   | -.00     | 355.0  | .0     |
| .03             | 6.989    | 1.146   | 1.842  | .003   | -19.72   | -.03     | 362.3  | .4     |
| .06             | 5.303    | 1.422   | 1.949  | .016   | -20.81   | -.18     | 373.5  | 2.1    |
| .10             | 4.215    | 1.598   | 2.083  | .056   | -22.13   | -.63     | 386.7  | 7.1    |
| .15             | 3.481    | 1.694   | 2.210  | .149   | -23.27   | -1.64    | 396.9  | 18.1   |
| .21             | 2.977    | 1.724   | 2.261  | .316   | -23.50   | -3.40    | 396.3  | 36.7   |
| .28             | 2.633    | 1.702   | 2.168  | .550   | -22.17   | -5.77    | 378.8  | 60.5   |
| .36             | 2.407    | 1.638   | 1.924  | .801   | -19.30   | -8.15    | 346.3  | 83.1   |
| .45             | 2.268    | 1.542   | 1.593  | 1.007  | -15.73   | -9.93    | 308.4  | 98.1   |
| .55             | 2.197    | 1.423   | 1.263  | 1.139  | -12.37   | -10.86   | 274.8  | 103.7  |
| .67             | 2.177    | 1.279   | .963   | 1.205  | -9.50    | -11.04   | 248.0  | 101.3  |
| .82             | 2.206    | 1.109   | .713   | 1.212  | -7.30    | -10.59   | 229.5  | 92.7   |
| 1.01            | 2.280    | .919    | .524   | 1.169  | -5.85    | -9.65    | 219.4  | 79.9   |
| 1.25            | 2.393    | .725    | .397   | 1.089  | -5.09    | -8.41    | 216.4  | 65.1   |
| 1.55            | 2.530    | .543    | .323   | .984   | -4.88    | -7.04    | 218.4  | 50.4   |
| 1.95            | 2.683    | .377    | .290   | .858   | -5.07    | -5.59    | 223.7  | 36.5   |
| 2.45            | 2.826    | .248    | .292   | .727   | -5.50    | -4.27    | 230.2  | 25.1   |
| 3.05            | 2.946    | .158    | .314   | .604   | -6.02    | -3.17    | 236.4  | 16.8   |
| 3.80            | 3.046    | .097    | .348   | .490   | -6.55    | -2.28    | 242.1  | 10.7   |
| 4.70            | 3.127    | .054    | .389   | .379   | -7.03    | -1.56    | 246.5  | 6.4    |
| 5.80            | 3.188    | .031    | .430   | .295   | -7.44    | -1.07    | 250.2  | 3.9    |
| 7.10            | 3.234    | .018    | .466   | .228   | -7.78    | -.72     | 252.9  | 2.3    |
| 8.70            | 3.271    | .009    | .500   | .171   | -8.06    | -.47     | 255.1  | 1.3    |
| 10.70           | 3.299    | .005    | .530   | .128   | -8.29    | -.30     | 256.8  | .7     |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 10  
DRAFT = 32.752 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |        |        |
| .000                  | -32.752 | 4.027  | 2.013             | -32.707 | .0224 | .9997 | 1.278  |        |
| 4.026                 | -32.662 | 4.027  | 6.039             | -32.617 | .0224 | .9997 | 5.305  |        |
| 8.052                 | -32.571 | 4.027  | 10.065            | -32.526 | .0224 | .9997 | 9.332  |        |
| 12.078                | -32.481 | 4.027  | 14.091            | -32.436 | .0224 | .9997 | 13.359 |        |
| 16.104                | -32.391 | 4.027  | 18.117            | -32.345 | .0224 | .9997 | 17.386 |        |
| 20.130                | -32.300 | 4.027  | 22.143            | -32.255 | .0224 | .9997 | 21.413 |        |
| 24.156                | -32.210 | 4.026  | 26.167            | -32.128 | .0404 | .9992 | 24.846 |        |
| 28.179                | -32.047 | 2.008  | 29.173            | -31.908 | .1383 | .9904 | 24.479 |        |
| 30.168                | -31.769 | 2.008  | 31.162            | -31.630 | .1383 | .9904 | 26.487 |        |
| 32.156                | -31.491 | 4.015  | 34.080            | -30.916 | .2868 | .9580 | 23.780 |        |
| 36.003                | -30.340 | 3.996  | 37.792            | -29.451 | .4451 | .8955 | 20.733 |        |
| 39.581                | -28.561 | 4.026  | 41.195            | -27.359 | .5973 | .8020 | 16.699 |        |
| 42.810                | -26.157 | 4.020  | 44.104            | -24.618 | .7652 | .6438 | 9.553  |        |
| 45.398                | -23.080 | 4.024  | 46.383            | -21.326 | .8719 | .4897 | 4.121  |        |
| 47.369                | -19.572 | 4.025  | 48.115            | -17.703 | .9286 | .3710 | 1.412  |        |
| 48.862                | -15.834 | 4.022  | 49.396            | -13.895 | .9641 | .2656 | -.274  |        |
| 49.930                | -11.956 | 4.027  | 50.298            | -9.977  | .9832 | .1827 | -.618  |        |
| 50.666                | -7.997  | 4.025  | 50.941            | -6.003  | .9907 | .1363 | .997   |        |
| 51.215                | -4.009  | 4.027  | 51.402            | -2.005  | .9957 | .0929 | 2.777  |        |
| 51.589                | 0.000   |        |                   |         |       |       |        |        |

| FREQ.  | A'       | N'    | M     | N     | M      | N      | I     | N    |
|--------|----------|-------|-------|-------|--------|--------|-------|------|
| PARAM. | 33       | Z     | S     | S     | S.R    | S.R    | R     | R    |
| .00    | INFINITY | 0.000 | 1.871 | 0.000 | -18.10 | 0.00   | 603.6 | 0.0  |
| .01    | 11.129   | .831  | 1.904 | .000  | -18.42 | -.00   | 606.7 | .0   |
| .03    | 7.843    | 1.273 | 1.983 | .003  | -19.19 | -.04   | 614.5 | .5   |
| .06    | 5.962    | 1.567 | 2.110 | .019  | -20.38 | -.22   | 626.1 | 2.6  |
| .10    | 4.760    | 1.745 | 2.270 | .068  | -21.77 | -.77   | 638.5 | 8.6  |
| .15    | 3.958    | 1.830 | 2.416 | .182  | -22.81 | -1.97  | 645.1 | 21.3 |
| .21    | 3.418    | 1.838 | 2.462 | .386  | -22.59 | -3.99  | 637.2 | 41.2 |
| .28    | 3.062    | 1.785 | 2.326 | .666  | -20.47 | -6.52  | 610.2 | 63.9 |
| .36    | 2.841    | 1.684 | 2.009 | .953  | -16.77 | -8.78  | 570.7 | 81.1 |
| .45    | 2.722    | 1.548 | 1.605 | 1.175 | -12.68 | -10.13 | 531.9 | 87.4 |
| .55    | 2.681    | 1.389 | 1.221 | 1.305 | -9.21  | -10.45 | 503.1 | 83.7 |
| .67    | 2.701    | 1.203 | .885  | 1.357 | -6.58  | -9.96  | 485.1 | 73.0 |
| .82    | 2.779    | .995  | .614  | 1.344 | -4.88  | -8.83  | 477.5 | 57.9 |
| 1.01   | 2.908    | .775  | .417  | 1.278 | -4.09  | -.30   | 478.3 | 41.5 |
| 1.25   | 3.075    | .564  | .290  | 1.173 | -4.03  | -5.61  | 484.8 | 26.6 |
| 1.55   | 3.257    | .382  | .223  | 1.045 | -4.48  | -3.99  | 493.6 | 15.0 |
| 1.95   | 3.443    | .232  | .201  | .897  | -5.26  | -2.49  | 502.9 | 6.8  |
| 2.45   | 3.605    | .129  | .215  | .739  | -6.10  | -1.32  | 510.7 | 2.3  |
| 3.05   | 3.731    | .068  | .250  | .600  | -6.87  | -.57   | 516.1 | .5   |
| 3.80   | 3.830    | .034  | .297  | .473  | -7.52  | -.12   | 520.0 | .0   |
| 4.70   | 3.903    | .016  | .347  | .365  | -8.00  | .10    | 522.5 | .0   |
| 5.80   | 3.958    | .007  | .394  | .277  | -8.36  | .17    | 524.3 | .1   |
| 7.10   | 3.999    | .003  | .436  | .210  | -8.61  | .16    | 525.6 | .1   |
| 8.70   | 4.031    | .002  | .473  | .157  | -8.78  | .13    | 526.6 | .1   |
| 10.70  | 4.057    | .001  | .505  | .116  | -8.92  | .10    | 527.4 | .1   |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTSSTATION 11  
DRAFT = 32.770 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |        |        |
| .000                  | -32.770 | 4.235  | 2.117             | -32.728 | .0201 | .9998 | 1.459  |        |
| 4.234                 | -32.685 | 4.235  | 6.352             | -32.643 | .0201 | .9998 | 5.695  |        |
| 8.469                 | -32.600 | 4.235  | 10.586            | -32.558 | .0201 | .9998 | 9.930  |        |
| 12.703                | -32.515 | 4.235  | 14.820            | -32.472 | .0201 | .9998 | 14.165 |        |
| 16.937                | -32.430 | 4.235  | 19.055            | -32.387 | .0201 | .9998 | 18.400 |        |
| 21.172                | -32.345 | 4.235  | 23.289            | -32.302 | .0201 | .9998 | 22.635 |        |
| 25.406                | -32.260 | 4.235  | 27.523            | -32.217 | .0201 | .9998 | 26.871 |        |
| 29.641                | -32.175 | 4.234  | 31.756            | -32.095 | .0375 | .9993 | 30.530 |        |
| 33.871                | -32.016 | 4.232  | 35.961            | -31.684 | .1566 | .9877 | 30.554 |        |
| 38.051                | -31.353 | 2.107  | 39.047            | -31.011 | .3250 | .9457 | 26.850 |        |
| 40.043                | -30.668 | 2.107  | 41.040            | -30.326 | .3250 | .9457 | 28.956 |        |
| 42.036                | -29.984 | 4.204  | 43.795            | -28.834 | .5472 | .8370 | 20.879 |        |
| 45.555                | -27.683 | 4.231  | 47.025            | -26.162 | .7191 | .6949 | 13.866 |        |
| 48.495                | -24.641 | 4.222  | 49.473            | -22.770 | .8862 | .4632 | 2.737  |        |
| 50.450                | -20.900 | 4.230  | 51.107            | -18.889 | .9506 | .3103 | -2.099 |        |
| 51.763                | -16.878 | 4.229  | 52.082            | -14.788 | .9885 | .1510 | -6.754 |        |
| 52.402                | -12.697 | 4.234  | 52.515            | -10.583 | .9986 | .0537 | -7.747 |        |
| 52.629                | -8.470  | 4.235  | 52.666            | -6.352  | .9998 | .0176 | -5.424 |        |
| 52.704                | -4.235  | 4.235  | 52.727            | -2.117  | .9999 | .0109 | -1.544 |        |
| 52.750                | 0.000   |        |                   |         |       |       |        |        |

| FREQ.  | A'       | N'    | M     | N     | M      | N      | I     | N    |
|--------|----------|-------|-------|-------|--------|--------|-------|------|
| PARAM. | 33       | Z     | S     | S     | S.R    | S.R    | R     | R    |
| .00    | INFINITY | 0.000 | 1.977 | 0.000 | -17.07 | 0.00   | 829.5 | 0.0  |
| .01    | 11.979   | .893  | 2.013 | .000  | -17.41 | -.00   | 832.9 | .0   |
| .03    | 8.441    | 1.362 | 2.102 | .004  | -18.25 | -.05   | 841.3 | .6   |
| .06    | 6.425    | 1.670 | 2.242 | .022  | -19.53 | -.25   | 853.6 | 3.0  |
| .10    | 5.144    | 1.850 | 2.419 | .077  | -20.98 | -.87   | 866.0 | 9.9  |
| .15    | 4.296    | 1.927 | 2.577 | .207  | -21.94 | -2.22  | 870.6 | 24.0 |
| .21    | 3.733    | 1.922 | 2.615 | .436  | -21.40 | -4.43  | 858.0 | 45.1 |
| .28    | 3.369    | 1.849 | 2.443 | .744  | -18.74 | -7.06  | 825.1 | 67.3 |
| .36    | 3.152    | 1.726 | 2.075 | 1.050 | -14.51 | -9.24  | 781.9 | 81.4 |
| .45    | 3.047    | 1.565 | 1.626 | 1.278 | -10.14 | -10.30 | 743.4 | 83.2 |
| .55    | 3.026    | 1.383 | 1.212 | 1.403 | -6.68  | -10.26 | 718.2 | 75.1 |
| .67    | 3.072    | 1.176 | .858  | 1.445 | -4.25  | -9.39  | 705.4 | 60.9 |
| .82    | 3.179    | .949  | .578  | 1.419 | -2.88  | -7.93  | 703.4 | 44.1 |
| 1.01   | 3.340    | .717  | .379  | 1.339 | -2.48  | -6.14  | 709.3 | 27.8 |
| 1.25   | 3.534    | .502  | .255  | 1.222 | -2.82  | -4.29  | 719.1 | 14.8 |
| 1.55   | 3.737    | .324  | .192  | 1.082 | -3.61  | -2.62  | 729.6 | 6.1  |
| 1.95   | 3.937    | .185  | .177  | .916  | -4.65  | -1.13  | 739.4 | 1.4  |
| 2.45   | 4.104    | .096  | .198  | .754  | -5.67  | -.16   | 746.1 | .0   |
| 3.05   | 4.231    | .047  | .240  | .606  | -6.51  | .38    | 750.3 | .2   |
| 3.80   | 4.329    | .021  | .292  | .473  | -7.17  | .60    | 752.9 | .8   |
| 4.70   | 4.400    | .009  | .346  | .364  | -7.62  | .60    | 754.5 | 1.0  |
| 5.80   | 4.454    | .004  | .397  | .276  | -7.92  | .51    | 755.8 | .9   |
| 7.10   | 4.493    | .002  | .442  | .209  | -8.12  | .38    | 756.7 | .7   |
| 8.70   | 4.524    | .001  | .481  | .155  | -8.25  | .27    | 757.6 | .5   |
| 10.70  | 4.549    | .000  | .514  | .115  | -8.34  | .18    | 758.3 | .3   |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 12  
DRAFT = 32.788 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |        | SINE   | COSINE  | MOMENT |
|-----------------------|---------|--------|-------------------|---------|--------|--------|---------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |        |        |         |        |
| .000                  | -32.788 | 4.300  | 2.150             | -32.745 | .0200  | .9998  | 1.493   |        |
| 4.299                 | -32.702 | 4.300  | 6.449             | -32.659 | .0200  | .9998  | 5.793   |        |
| 8.598                 | -32.616 | 4.300  | 10.748            | -32.573 | .0200  | .9998  | 10.093  |        |
| 12.897                | -32.530 | 4.300  | 15.047            | -32.487 | .0200  | .9998  | 14.393  |        |
| 17.196                | -32.444 | 4.300  | 19.346            | -32.401 | .0200  | .9998  | 18.693  |        |
| 21.495                | -32.358 | 4.300  | 23.645            | -32.314 | .0200  | .9998  | 22.993  |        |
| 25.794                | -32.271 | 4.300  | 27.944            | -32.228 | .0200  | .9998  | 27.293  |        |
| 30.093                | -32.185 | 4.299  | 32.242            | -32.112 | .0340  | .9994  | 31.133  |        |
| 34.390                | -32.039 | 4.296  | 36.521            | -31.768 | .1264  | .9920  | 32.211  |        |
| 38.651                | -31.496 | 2.133  | 39.677            | -31.204 | .2742  | .9617  | 29.600  |        |
| 40.702                | -30.911 | 2.133  | 41.727            | -30.619 | .2742  | .9617  | 31.733  |        |
| 42.753                | -30.327 | 4.277  | 44.611            | -29.268 | .4950  | .8689  | 24.274  |        |
| 46.469                | -28.209 | 4.276  | 47.973            | -26.689 | .7109  | .7033  | 14.766  |        |
| 49.477                | -25.169 | 4.287  | 50.451            | -23.260 | .8907  | .4546  | 2.216   |        |
| 51.426                | -21.351 | 4.280  | 51.912            | -19.267 | .9738  | .2272  | -6.967  |        |
| 52.398                | -17.182 | 4.297  | 52.574            | -15.041 | .9966  | .0819  | -10.686 |        |
| 52.750                | -12.900 | 4.300  | 52.750            | -10.750 | 1.0000 | 0.0000 | -10.750 |        |
| 52.750                | -8.600  | 4.300  | 52.750            | -6.450  | 1.0000 | 0.0000 | -6.450  |        |
| 52.750                | -4.300  | 4.300  | 52.750            | -2.150  | 1.0000 | 0.0000 | -2.150  |        |
| 52.750                | 0.000   |        |                   |         |        |        |         |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 2.017  | 0.000  | -15.65   | 0.00     | 885.6  | 0.0    |
| .01             | 12.109   | .901    | 2.054  | .000   | -15.98   | -.00     | 888.9  | .0     |
| .03             | 8.536    | 1.373   | 2.145  | .004   | -16.80   | -.05     | 896.7  | .5     |
| .06             | 6.502    | 1.681   | 2.291  | .022   | -18.04   | -.25     | 908.1  | 2.9    |
| .10             | 5.211    | 1.859   | 2.474  | .080   | -19.44   | -.87     | 919.1  | 9.4    |
| .15             | 4.358    | 1.933   | 2.636  | .214   | -20.32   | -2.20    | 922.5  | 22.6   |
| .21             | 3.794    | 1.923   | 2.673  | .452   | -19.68   | -4.35    | 909.3  | 42.1   |
| .28             | 3.433    | 1.845   | 2.491  | .771   | -16.94   | -6.89    | 877.5  | 61.8   |
| .36             | 3.221    | 1.714   | 2.105  | 1.086  | -12.73   | -8.91    | 837.1  | 73.3   |
| .45             | 3.122    | 1.548   | 1.639  | 1.317  | -8.47    | -9.79    | 802.8  | 73.0   |
| .55             | 3.109    | 1.360   | 1.212  | 1.441  | -5.19    | -9.59    | 781.6  | 63.9   |
| .67             | 3.163    | 1.148   | .850   | 1.479  | -2.98    | -8.60    | 772.4  | 49.9   |
| .82             | 3.280    | .918    | .566   | 1.448  | -1.84    | -7.06    | 773.0  | 34.2   |
| 1.01            | 3.450    | .684    | .366   | 1.363  | -1.64    | -5.24    | 780.3  | 19.8   |
| 1.25            | 3.651    | .472    | .242   | 1.241  | -2.14    | -3.41    | 790.5  | 9.1    |
| 1.55            | 3.859    | .298    | .181   | 1.093  | -3.07    | -1.74    | 801.0  | 2.8    |
| 1.95            | 4.060    | .166    | .168   | .926   | -4.17    | -.42     | 809.1  | .2     |
| 2.45            | 4.226    | .084    | .192   | .759   | -5.22    | .42      | 814.5  | .2     |
| 3.05            | 4.351    | .039    | .236   | .609   | -6.05    | .82      | 817.5  | 1.1    |
| 3.80            | 4.447    | .017    | .291   | .474   | -6.67    | .91      | 819.3  | 1.8    |
| 4.70            | 4.516    | .007    | .347   | .364   | -7.08    | .81      | 820.4  | 1.8    |
| 5.80            | 4.568    | .003    | .399   | .275   | -7.35    | .64      | 821.4  | 1.5    |
| 7.10            | 4.607    | .001    | .445   | .208   | -7.50    | .47      | 822.2  | 1.1    |
| 8.70            | 4.637    | .000    | .485   | .154   | -7.60    | .32      | 822.9  | .7     |
| 10.70           | 4.662    | .000    | .518   | .115   | -7.67    | .21      | 823.5  | .4     |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 13  
DRAFT = 32.806 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE   | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|--------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |        |        |        |
| .000                  | -32.806 | 4.238  | 2.119             | -32.764 | .0200  | .9998  | 1.462  |
| 4.237                 | -32.721 | 4.238  | 6.356             | -32.679 | .0200  | .9998  | 5.700  |
| 8.475                 | -32.636 | 4.238  | 10.594            | -32.594 | .0200  | .9998  | 9.939  |
| 12.712                | -32.551 | 4.238  | 14.831            | -32.509 | .0200  | .9998  | 14.177 |
| 16.950                | -32.467 | 4.238  | 19.068            | -32.424 | .0200  | .9998  | 18.415 |
| 21.187                | -32.382 | 4.238  | 23.306            | -32.339 | .0200  | .9998  | 22.653 |
| 25.425                | -32.297 | 4.238  | 27.543            | -32.254 | .0200  | .9998  | 26.892 |
| 29.662                | -32.212 | 4.232  | 31.775            | -32.101 | .0526  | .9986  | 30.042 |
| 33.888                | -31.989 | 4.238  | 35.975            | -31.620 | .1740  | .9847  | 29.925 |
| 38.062                | -31.252 | 2.115  | 39.056            | -30.890 | .3422  | .9396  | 26.126 |
| 40.049                | -30.528 | 2.115  | 41.043            | -30.166 | .3422  | .9396  | 28.241 |
| 42.037                | -29.804 | 4.220  | 43.843            | -28.714 | .5166  | .8562  | 22.704 |
| 45.649                | -27.624 | 4.233  | 47.153            | -26.134 | .7040  | .7102  | 15.088 |
| 48.656                | -24.644 | 4.234  | 49.662            | -22.781 | .8798  | .4753  | 3.558  |
| 50.668                | -20.919 | 4.227  | 51.311            | -18.905 | .9526  | .3041  | -2.405 |
| 51.954                | -16.892 | 4.233  | 52.288            | -14.802 | .9874  | .1582  | -6.345 |
| 52.623                | -12.712 | 4.237  | 52.687            | -10.594 | .9996  | .0299  | -9.013 |
| 52.750                | -8.477  | 4.238  | 52.750            | -6.357  | 1.0000 | 0.0000 | -6.357 |
| 52.750                | -4.238  | 4.238  | 52.750            | -2.119  | 1.0000 | 0.0000 | -2.119 |
| 52.750                | 0.000   |        |                   |         |        |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.974  | 0.000  | -17.63   | 0.00     | 836.?  | 0.0    |
| .01             | 12.040   | .898    | 2.009  | .000   | -17.98   | -.00     | 839.9  | .0     |
| .02             | 8.482    | 1.369   | 2.098  | .004   | -18.83   | -.05     | 848.?  | .6     |
| .06             | 6.456    | 1.679   | 2.238  | .022   | -20.14   | -.26     | 861.6  | 3.1    |
| .10             | 5.167    | 1.860   | 2.414  | .077   | -21.64   | -.89     | 874.6  | 10.3   |
| .15             | 4.315    | 1.938   | 2.570  | .206   | -22.63   | -2.26    | 879.7  | 25.0   |
| .21             | 3.748    | 1.933   | 2.608  | .434   | -22.10   | -4.52    | 866.8  | 47.1   |
| .28             | 3.382    | 1.862   | 2.437  | .740   | -19.40   | -7.22    | 832.7  | 70.5   |
| .36             | 3.163    | 1.738   | 2.072  | 1.045  | -15.10   | -9.45    | 787.5  | 85.7   |
| .45             | 3.057    | 1.578   | 1.626  | 1.272  | -10.64   | -10.57   | 747.0  | 88.0   |
| .55             | 3.034    | 1.396   | 1.213  | 1.397  | -7.09    | -10.57   | 720.1  | 80.0   |
| .67             | 3.078    | 1.189   | .860   | 1.439  | -4.58    | -9.71    | 706.1  | 65.5   |
| .82             | 3.185    | .961    | .582   | 1.414  | -3.14    | -8.25    | 703.4  | 47.9   |
| 1.01            | 3.345    | .727    | .383   | 1.336  | -2.68    | -6.45    | 709.0  | 30.8   |
| 1.25            | 3.539    | .511    | .258   | 1.220  | -2.98    | -4.57    | 719.0  | 16.8   |
| 1.55            | 3.742    | .331    | .194   | 1.081  | -3.76    | -2.86    | 729.9  | 7.3    |
| 1.95            | 3.943    | .190    | .179   | .916   | -4.79    | -1.33    | 740.2  | 1.9    |
| 2.45            | 4.111    | .099    | .199   | .754   | -5.82    | -.31     | 747.3  | .1     |
| 3.05            | 4.240    | .049    | .241   | .606   | -6.67    | .27      | 751.9  | .1     |
| 3.80            | 4.338    | .022    | .293   | .474   | -7.35    | .52      | 754.8  | .6     |
| 4.70            | 4.410    | .010    | .346   | .365   | -7.82    | .55      | 756.7  | .8     |
| 5.80            | 4.465    | .004    | .397   | .277   | -8.13    | .47      | 758.1  | .8     |
| 7.10            | 4.505    | .002    | .442   | .209   | -8.34    | .36      | 759.1  | .6     |
| 8.70            | 4.536    | .001    | .481   | .156   | -8.48    | .26      | 760.0  | .4     |
| 10.70           | 4.561    | .000    | .514   | .116   | -8.58    | .17      | 760.7  | .3     |

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HOFFMAN MARITIME CONSULTANTS INC GLEN HEAD NY

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USER MANUAL FOR PROGRAM SCOMOT SECOND PART OF U.S.C.G. SHIP MOT--ETC(U)

DOT-CG-958905-A

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 14  
DRAFT = 32.824 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |        | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|--------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |        |       |        |        |
| .000                  | -32.824 | 4.115  | 2.057             | -32.783 | .0200  | .9998 | 1.402  |        |
| 4.115                 | -32.742 | 4.115  | 6.172             | -32.701 | .0200  | .9998 | 5.518  |        |
| 8.229                 | -32.660 | 4.115  | 10.287            | -32.619 | .0200  | .9998 | 9.633  |        |
| 12.344                | -32.578 | 4.115  | 14.401            | -32.537 | .0200  | .9998 | 13.749 |        |
| 16.459                | -32.495 | 4.115  | 18.516            | -32.454 | .0200  | .9998 | 17.864 |        |
| 20.573                | -32.413 | 4.115  | 22.630            | -32.371 | .0207  | .9998 | 21.954 |        |
| 24.688                | -32.328 | 4.115  | 26.738            | -32.158 | .0826  | .9966 | 23.992 |        |
| 28.789                | -31.988 | 4.115  | 30.819            | -31.650 | .1642  | .9864 | 25.203 |        |
| 32.848                | -31.312 | 2.054  | 33.832            | -31.017 | .2876  | .9578 | 23.484 |        |
| 34.815                | -30.722 | 2.054  | 35.799            | -30.426 | .2876  | .9578 | 25.538 |        |
| 36.783                | -30.131 | 4.098  | 38.651            | -29.290 | .4104  | .9119 | 23.226 |        |
| 40.520                | -28.449 | 4.111  | 42.244            | -27.330 | .5443  | .8389 | 20.562 |        |
| 43.968                | -26.212 | 4.107  | 45.442            | -24.782 | .6963  | .7177 | 15.359 |        |
| 46.916                | -23.352 | 4.107  | 48.133            | -21.698 | .8055  | .5926 | 11.045 |        |
| 49.350                | -20.043 | 4.110  | 50.197            | -18.171 | .9112  | .4120 | 4.123  |        |
| 51.043                | -16.298 | 4.112  | 51.528            | -14.300 | .9718  | .2360 | -1.737 |        |
| 52.014                | -12.302 | 4.113  | 52.280            | -10.263 | .9916  | .1296 | -3.402 |        |
| 52.547                | -8.224  | 4.113  | 52.641            | -6.170  | .9989  | .0459 | -3.745 |        |
| 52.736                | -4.115  | 4.115  | 52.743            | -2.058  | 1.0000 | .0035 | -1.872 |        |
| 52.750                | 0.000   |        |                   |         |        |       |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.867  | 0.000  | -22.11   | 0.00     | 753.1  | 0.0    |
| .01             | 11.905   | .892    | 1.899  | .000   | -22.50   | -.00     | 757.8  | .0     |
| .03             | 8.377    | 1.364   | 1.980  | .003   | -23.44   | -.05     | 769.3  | .7     |
| .06             | 6.365    | 1.677   | 2.107  | .020   | -24.90   | -.27     | 786.5  | 3.8    |
| :10             | 5.082    | 1.865   | 2.267  | .070   | -26.61   | -.94     | 805.0  | 12.7   |
| .15             | 4.229    | 1.954   | 2.408  | .186   | -27.85   | -2.41    | 815.0  | 31.4   |
| .21             | 3.656    | 1.963   | 2.445  | .390   | -27.56   | -4.86    | 803.8  | 60.7   |
| .28             | 3.279    | 1.907   | 2.301  | .666   | -24.98   | -7.91    | 764.8  | 94.1   |
| .36             | 3.044    | 1.800   | 1.982  | .945   | -20.56   | -10.64   | 707.7  | 120.0  |
| .45             | 2.918    | 1.656   | 1.585  | 1.159  | -15.70   | -12.30   | 651.3  | 130.6  |
| .55             | 2.873    | 1.488   | 1.211  | 1.285  | -11.56   | -12.77   | 608.6  | 126.8  |
| .67             | 2.893    | 1.293   | .883   | 1.337  | -8.38    | -12.29   | 580.7  | 112.8  |
| .82             | 2.974    | 1.073   | .619   | 1.325  | -6.26    | -11.06   | 567.2  | 92.2   |
| 1.01            | 3.110    | .840    | .425   | 1.262  | -5.17    | -9.35    | 566.1  | 69.0   |
| 1.25            | 3.285    | .616    | .299   | 1.162  | -4.96    | -7.41    | 573.4  | 46.9   |
| 1.55            | 3.476    | .421    | .232   | 1.038  | -5.37    | -5.50    | 584.9  | 28.8   |
| 1.95            | 3.674    | .259    | .208   | .892   | -6.19    | -3.69    | 598.0  | 15.0   |
| 2.45            | 3.845    | .148    | .220   | .745   | -7.15    | -2.25    | 609.3  | 6.6    |
| 3.05            | 3.981    | .080    | .253   | .610   | -8.03    | -1.24    | 617.9  | 2.4    |
| 3.80            | 4.087    | .041    | .297   | .487   | -8.80    | -.56     | 624.1  | .6     |
| 4.70            | 4.167    | .019    | .348   | .369   | -9.37    | -.20     | 628.6  | .1     |
| 5.80            | 4.227    | .009    | .396   | .279   | -9.82    | -.02     | 631.6  | .0     |
| 7.10            | 4.271    | .004    | .437   | .211   | -10.14   | .04      | 633.8  | .0     |
| 8.70            | 4.306    | .002    | .474   | .158   | -10.38   | .06      | 635.5  | .0     |
| 10.70           | 4.333    | .001    | .506   | .117   | -10.56   | .05      | 636.8  | .0     |

PROGRAM STATIC (05/79)

07/28/80

20.21.08

PAGE 31

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTSSTATION 15  
DRAFT = 32.842 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|--------|--------|
| H-BRDT                | HEIGHT  | LENGTH | H-BRDT            | HEIGHT  |       |        |        |
| .000                  | -32.842 | 3.939  | 1.969             | -32.802 | .0206 | .9998  | 1.294  |
| 3.938                 | -32.761 | 3.939  | 5.907             | -32.721 | .0206 | .9998  | 5.232  |
| 7.876                 | -32.680 | 3.939  | 9.845             | -32.640 | .0206 | .9998  | 9.171  |
| 11.814                | -32.599 | 3.939  | 13.782            | -32.558 | .0206 | .9998  | 13.110 |
| 15.751                | -32.518 | 3.938  | 17.711            | -32.330 | .0956 | .9954  | 14.540 |
| 19.671                | -32.141 | 1.969  | 20.646            | -32.005 | .1383 | .9904  | 16.022 |
| 21.621                | -31.869 | 1.969  | 22.596            | -31.733 | .1383 | .9904  | 17.991 |
| 23.571                | -31.597 | 3.931  | 25.496            | -31.200 | .2018 | .9794  | 18.676 |
| 27.421                | -30.804 | 3.939  | 29.308            | -30.242 | .2855 | .9584  | 19.455 |
| 31.195                | -29.679 | 3.937  | 33.019            | -28.939 | .3762 | .9265  | 19.705 |
| 34.843                | -28.198 | 3.936  | 36.591            | -27.296 | .4588 | .8885  | 19.990 |
| 38.340                | -26.393 | 3.932  | 39.967            | -25.288 | .5617 | .8274  | 18.863 |
| 41.593                | -24.184 | 3.939  | 43.067            | -22.879 | .6630 | .7486  | 17.073 |
| 44.542                | -21.573 | 3.933  | 45.781            | -20.046 | .7763 | .6304  | 13.298 |
| 47.021                | -18.520 | 3.924  | 48.081            | -16.869 | .8416 | .5401  | 11.774 |
| 49.140                | -15.217 | 3.931  | 49.903            | -13.406 | .9216 | .3881  | 7.013  |
| 50.666                | -11.595 | 3.932  | 51.175            | -9.696  | .9659 | .2588  | 3.881  |
| 51.684                | -7.797  | 3.938  | 52.024            | -5.857  | .9850 | .1728  | 3.220  |
| 52.364                | -3.918  | 3.937  | 52.557            | -1.959  | .9952 | .0980  | 3.200  |
| 52.750                | 0.000   |        |                   |         |       |        |        |

| FREQ.<br>PARAM. | A'       | N'    | M     | N     | M      | N      | I     | N     |
|-----------------|----------|-------|-------|-------|--------|--------|-------|-------|
|                 | 33       | Z     | S     | S     | S.R    | S.R    | R     | R     |
| .00             | INFINITY | 0.000 | 1.706 | 0.000 | -27.32 | 0.00   | 688.1 | 0.0   |
| .01             | 11.652   | .878  | 1.734 | .000  | -27.74 | -.00   | 694.5 | .1    |
| .03             | 8.192    | 1.346 | 1.803 | .003  | -28.77 | -.05   | 710.2 | .8    |
| .06             | 6.215    | 1.662 | 1.911 | .017  | -30.36 | -.28   | 734.0 | 4.7   |
| .10             | 4.950    | 1.861 | 2.045 | .059  | -32.26 | -.97   | 761.2 | 15.9  |
| .15             | 4.103    | 1.965 | 2.164 | .156  | -33.78 | -2.50  | 780.0 | 40.0  |
| .21             | 3.525    | 1.994 | 2.200 | .326  | -33.83 | -5.09  | 773.9 | 79.5  |
| .28             | 3.135    | 1.962 | 2.091 | .556  | -31.59 | -8.44  | 732.1 | 128.3 |
| .36             | 2.880    | 1.882 | 1.839 | .795  | -27.29 | -11.70 | 661.5 | 172.1 |
| .45             | 2.727    | 1.765 | 1.515 | .988  | -22.20 | -14.03 | 583.6 | 199.2 |
| .55             | 2.652    | 1.622 | 1.198 | 1.110 | -17.54 | -15.17 | 516.7 | 207.3 |
| .67             | 2.636    | 1.450 | .912  | 1.172 | -13.61 | -15.30 | 464.6 | 200.0 |
| .82             | 2.677    | 1.248 | .674  | 1.178 | -10.63 | -14.57 | 429.6 | 180.3 |
| 1.01            | 2.772    | 1.024 | .492  | 1.138 | -8.69  | -13.17 | 411.6 | 152.5 |
| 1.25            | 2.912    | .797  | .369  | 1.062 | -7.72  | -11.34 | 408.1 | 121.1 |
| 1.55            | 3.077    | .585  | .297  | .961  | -7.52  | -9.33  | 414.5 | 90.5  |
| 1.95            | 3.261    | .395  | .264  | .839  | -7.88  | -7.22  | 427.3 | 62.1  |
| 2.45            | 3.431    | .251  | .265  | .710  | -8.58  | -5.32  | 442.2 | 39.7  |
| 3.05            | 3.572    | .153  | .287  | .590  | -9.39  | -3.79  | 455.8 | 24.2  |
| 3.80            | 3.688    | .088  | .321  | .478  | -10.20 | -2.57  | 467.6 | 13.8  |
| 4.70            | 3.780    | .047  | .362  | .369  | -10.91 | -1.65  | 476.8 | 7.4   |
| 5.80            | 3.849    | .025  | .401  | .286  | -11.52 | -1.05  | 483.8 | 3.8   |
| 7.10            | 3.900    | .013  | .437  | .221  | -11.99 | -.66   | 489.0 | 1.9   |
| 8.70            | 3.941    | .007  | .470  | .169  | -12.37 | -.41   | 493.0 | 1.0   |
| 10.70           | 3.973    | .003  | .500  | .124  | -12.68 | -.24   | 496.1 | .5    |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 16  
DRAFT = 32.860 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |        |        |
| .000                  | -32.860 | 3.706  | 1.853             | -32.835 | .0136 | .9999 | 1.405  |        |
| 3.706                 | -32.810 | 3.709  | 5.552             | -32.629 | .0971 | .9953 | 2.356  |        |
| 7.397                 | -32.449 | 3.709  | 9.243             | -32.269 | .0971 | .9953 | 6.065  |        |
| 11.088                | -32.089 | 3.707  | 12.914            | -31.774 | .1703 | .9854 | 7.313  |        |
| 14.741                | -31.458 | 3.706  | 16.545            | -31.036 | .2276 | .9737 | 9.046  |        |
| 18.350                | -30.614 | 3.709  | 20.144            | -30.146 | .2524 | .9676 | 11.884 |        |
| 21.938                | -29.678 | 3.708  | 23.700            | -29.101 | .3115 | .9502 | 13.455 |        |
| 25.462                | -28.523 | 3.707  | 27.201            | -27.883 | .3453 | .9385 | 15.899 |        |
| 28.941                | -27.243 | 1.851  | 29.785            | -26.865 | .4090 | .9125 | 16.191 |        |
| 30.630                | -26.486 | 1.851  | 31.474            | -26.107 | .4090 | .9125 | 18.042 |        |
| 32.319                | -25.729 | 3.708  | 33.919            | -24.793 | .5051 | .8631 | 16.753 |        |
| 35.518                | -23.856 | 3.705  | 37.039            | -22.798 | .5711 | .8209 | 17.382 |        |
| 38.560                | -21.740 | 3.705  | 39.954            | -20.521 | .6584 | .7527 | 16.561 |        |
| 41.348                | -19.301 | 3.709  | 42.640            | -17.971 | .7172 | .6969 | 16.829 |        |
| 43.933                | -16.641 | 3.707  | 45.074            | -15.181 | .7879 | .6158 | 15.793 |        |
| 46.215                | -13.721 | 3.701  | 47.141            | -12.118 | .8658 | .5004 | 13.098 |        |
| 48.067                | -10.516 | 3.705  | 48.790            | -8.810  | .9209 | .3898 | 10.905 |        |
| 49.512                | -7.104  | 3.707  | 50.091            | -5.344  | .9499 | .3126 | 10.583 |        |
| 50.671                | -3.583  | 3.707  | 51.147            | -1.791  | .9664 | .2572 | 11.425 |        |
| 51.624                | 0.000   |        |                   |         |       |       |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.514  | 0.000  | -29.23   | 0.00     | 641.7  | 0.0    |
| .01             | 11.045   | .831    | 1.536  | .000   | -29.63   | -.00     | 649.0  | .1     |
| .03             | 7.779    | 1.280   | 1.591  | .002   | -30.61   | -.05     | 666.8  | .9     |
| .06             | 5.907    | 1.591   | 1.676  | .013   | -32.14   | -.25     | 694.3  | 4.8    |
| .10             | 4.702    | 1.794   | 1.783  | .046   | -34.01   | -.88     | 727.0  | 16.6   |
| .15             | 3.887    | 1.911   | 1.879  | .121   | -35.61   | -2.26    | 753.6  | 42.4   |
| .21             | 3.324    | 1.961   | 1.916  | .252   | -36.02   | -4.66    | 756.7  | 86.2   |
| .28             | 2.933    | 1.956   | 1.845  | .433   | -34.42   | -7.89    | 722.4  | 143.9  |
| .36             | 2.666    | 1.906   | 1.663  | .628   | -30.84   | -11.26   | 652.9  | 201.9  |
| .45             | 2.493    | 1.823   | 1.416  | .795   | -26.21   | -13.99   | 566.9  | 246.3  |
| .55             | 2.389    | 1.713   | 1.164  | .910   | -21.63   | -15.70   | 484.6  | 271.1  |
| .67             | 2.338    | 1.575   | .927   | .978   | -17.47   | -16.48   | 412.4  | 278.1  |
| .82             | 2.337    | 1.405   | .720   | 1.000  | -14.01   | -16.39   | 355.3  | 269.0  |
| 1.01            | 2.384    | 1.208   | .557   | .982   | -11.44   | -15.55   | 316.2  | 246.6  |
| 1.25            | 2.477    | .995    | .441   | .932   | -9.80    | -14.15   | 294.7  | 215.2  |
| 1.55            | 2.601    | .783    | .367   | .857   | -8.98    | -12.39   | 287.7  | 179.3  |
| 1.95            | 2.753    | .577    | .327   | .762   | -8.78    | -10.33   | 291.8  | 140.6  |
| 2.45            | 2.906    | .404    | .317   | .658   | -9.06    | -8.29    | 302.9  | 105.0  |
| 3.05            | 3.042    | .274    | .327   | .557   | -9.61    | -6.47    | 316.7  | 75.6   |
| 3.80            | 3.161    | .177    | .350   | .460   | -10.29   | -4.87    | 331.2  | 51.8   |
| 4.70            | 3.257    | .112    | .378   | .375   | -10.97   | -3.58    | 344.2  | 34.5   |
| 5.80            | 3.337    | .064    | .410   | .288   | -11.64   | -2.45    | 355.8  | 20.9   |
| 7.10            | 3.397    | .038    | .439   | .226   | -12.19   | -1.71    | 364.8  | 12.9   |
| 8.70            | 3.444    | .022    | .467   | .175   | -12.66   | -1.16    | 372.1  | 7.6    |
| 10.70           | 3.482    | .012    | .492   | .130   | -13.07   | -.74     | 377.9  | 4.2    |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
 CONFORMAL MAPPING - 3 COEFFICIENTS

STATION 17  
 DRAFT = 32.878 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|--------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |        |        |
| .000                  | -32.878 | 3.353  | 1.673             | -32.773 | .0628 | .9980  | -.387  |
| 3.347                 | -32.668 | 3.379  | 4.957             | -32.156 | .3030 | .9530  | -5.020 |
| 6.567                 | -31.644 | 3.384  | 8.193             | -31.175 | .2771 | .9608  | -.767  |
| 9.819                 | -30.706 | 1.693  | 10.623            | -30.441 | .3126 | .9499  | .576   |
| 11.428                | -30.176 | 1.693  | 12.232            | -29.912 | .3126 | .9499  | 2.270  |
| 13.036                | -29.647 | 3.386  | 14.608            | -29.017 | .3719 | .9283  | 2.768  |
| 16.180                | -28.388 | 3.387  | 17.753            | -27.760 | .3703 | .9289  | 6.210  |
| 19.326                | -27.133 | 3.384  | 20.880            | -26.465 | .3947 | .9188  | 8.738  |
| 22.435                | -25.798 | 3.387  | 23.953            | -25.049 | .4423 | .8969  | 1.403  |
| 25.472                | -24.300 | 3.384  | 26.983            | -23.538 | .4503 | .8929  | 13.493 |
| 28.494                | -22.776 | 3.387  | 29.921            | -21.865 | .5377 | .8432  | 13.473 |
| 31.349                | -20.955 | 3.380  | 32.725            | -19.975 | .5801 | .8145  | 15.067 |
| 34.102                | -18.994 | 3.387  | 35.387            | -17.892 | .6510 | .7591  | 15.216 |
| 36.673                | -16.790 | 3.385  | 37.868            | -15.591 | .7080 | .7062  | 15.702 |
| 39.063                | -14.393 | 3.378  | 40.149            | -13.099 | .7660 | .6428  | 15.773 |
| 41.234                | -11.805 | 3.385  | 42.199            | -10.414 | .8218 | .5698  | 15.486 |
| 43.163                | -9.023  | 3.385  | 44.044            | -7.578  | .8541 | .5201  | 16.434 |
| 44.924                | -6.132  | 3.386  | 45.698            | -4.626  | .8895 | .4570  | 16.768 |
| 46.471                | -3.120  | 3.386  | 47.129            | -1.560  | .9214 | .3885  | 16.874 |
| 47.787                | 0.000   |        |                   |         |       |        |        |

| FREQ.  | A'       | N'    | M     | N     | M      | N      | I     | N     |
|--------|----------|-------|-------|-------|--------|--------|-------|-------|
| PARAM. | 33       | Z     | S     | S     | S.R    | S.R    | R     | R     |
| .00    | INFINITY | 0.000 | 1.325 | 0.000 | -24.87 | 0.00   | 480.1 | 0.0   |
| .01    | 9.570    | .712  | 1.342 | .000  | -25.17 | -.00   | 485.6 | .0    |
| .03    | 6.778    | 1.106 | 1.383 | .002  | -25.91 | -.03   | 499.2 | .6    |
| .06    | 5.164    | 1.386 | 1.447 | .009  | -27.08 | -.18   | 520.5 | 3.3   |
| .10    | 4.114    | 1.578 | 1.528 | .033  | -28.54 | -.61   | 547.0 | 11.3  |
| .15    | 3.396    | 1.698 | 1.605 | .086  | -29.92 | -1.59  | 571.6 | 29.5  |
| .21    | 2.890    | 1.763 | 1.644 | .181  | -30.58 | -3.34  | 582.7 | 61.7  |
| .28    | 2.531    | 1.782 | 1.611 | .317  | -29.89 | -5.82  | 568.6 | 107.1 |
| .36    | 2.277    | 1.765 | 1.494 | .472  | -27.65 | -8.63  | 526.1 | 157.9 |
| .45    | 2.100    | 1.718 | 1.317 | .614  | -24.35 | -11.17 | 464.4 | 203.3 |
| .55    | 1.983    | 1.648 | 1.124 | .721  | -20.76 | -13.04 | 398.1 | 236.1 |
| .67    | 1.907    | 1.553 | .930  | .794  | -17.22 | -14.24 | 333.3 | 255.8 |
| .82    | 1.870    | 1.430 | .754  | .829  | -14.03 | -14.73 | 275.8 | 262.1 |
| 1.01   | 1.872    | 1.279 | .609  | .829  | -11.45 | -14.55 | 230.0 | 255.8 |
| 1.25   | 1.913    | 1.106 | .501  | .799  | -9.59  | -13.81 | 198.0 | 239.0 |
| 1.55   | 1.987    | .923  | .429  | .748  | -8.40  | -12.66 | 178.9 | 214.8 |
| 1.95   | 2.090    | .732  | .385  | .676  | -7.76  | -11.14 | 170.2 | 184.2 |
| 2.45   | 2.205    | .557  | .367  | .595  | -7.61  | -9.49  | 170.3 | 151.9 |
| 3.05   | 2.316    | .412  | .368  | .514  | -7.78  | -7.87  | 176.1 | 121.3 |
| 3.80   | 2.421    | .294  | .380  | .434  | -8.16  | -6.33  | 185.1 | 93.1  |
| 4.70   | 2.510    | .206  | .399  | .360  | -8.62  | -4.97  | 195.2 | 69.5  |
| 5.80   | 2.589    | .130  | .421  | .286  | -9.14  | -3.68  | 206.1 | 47.4  |
| 7.10   | 2.650    | .085  | .444  | .229  | -9.61  | -2.74  | 215.3 | 32.7  |
| 8.70   | 2.700    | .054  | .466  | .180  | -10.05 | -1.98  | 223.4 | 21.8  |
| 10.70  | 2.741    | .033  | .487  | .140  | -10.44 | -1.39  | 230.3 | 13.9  |

SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTS

STATION 18  
DRAFT = 32.896 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE  | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|---------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |         |        |
| .000                  | -32.896 | 2.877  | 1.424             | -32.695 | .1401 | .9901 | -3.171  |        |
| 2.848                 | -32.493 | 3.012  | 4.032             | -31.562 | .6180 | .7861 | -16.337 |        |
| 5.216                 | -30.632 | 3.020  | 6.483             | -29.811 | .5435 | .8394 | -10.758 |        |
| 7.751                 | -28.990 | 3.020  | 9.052             | -28.224 | .5077 | .8615 | -6.532  |        |
| 10.353                | -27.457 | 3.020  | 11.664            | -26.707 | .4964 | .8681 | -3.131  |        |
| 12.975                | -25.958 | 3.020  | 14.263            | -25.170 | .5216 | .8532 | -.961   |        |
| 15.551                | -24.383 | 1.510  | 16.209            | -24.013 | .4901 | .8717 | 2.360   |        |
| 16.867                | -23.643 | 1.510  | 17.525            | -23.273 | .4901 | .8717 | 3.869   |        |
| 18.183                | -22.903 | 3.021  | 19.420            | -22.037 | .5735 | .8192 | 3.270   |        |
| 20.657                | -21.171 | 3.020  | 21.909            | -20.327 | .5587 | .8294 | 6.815   |        |
| 23.162                | -19.484 | 3.021  | 24.364            | -18.570 | .6049 | .7963 | 8.167   |        |
| 25.567                | -17.656 | 3.019  | 26.749            | -16.717 | .6219 | .7831 | 10.551  |        |
| 27.932                | -15.778 | 3.021  | 29.078            | -14.795 | .6510 | .7591 | 12.442  |        |
| 30.225                | -13.812 | 3.019  | 31.316            | -12.769 | .6908 | .7230 | 13.821  |        |
| 32.407                | -11.727 | 3.020  | 33.464            | -10.648 | .7146 | .6996 | 15.801  |        |
| 34.520                | -9.569  | 3.021  | 35.520            | -8.437  | .7494 | .6621 | 17.194  |        |
| 36.520                | -7.304  | 3.019  | 37.454            | -6.119  | .7856 | .6187 | 18.365  |        |
| 38.388                | -4.933  | 3.020  | 39.277            | -3.713  | .8082 | .5889 | 20.131  |        |
| 40.166                | -2.492  | 3.020  | 41.019            | -1.246  | .8252 | .5649 | 22.143  |        |
| 41.872                | 0.000   |        |                   |         |       |       |         |        |

| FREQ.  | A'       | N'    | M     | N     | M      | N      | I     | N     |
|--------|----------|-------|-------|-------|--------|--------|-------|-------|
| PARAM. | 33       | Z     | S     | S     | S.R    | S.R    | R     | R     |
| .00    | INFINITY | 0.000 | 1.198 | 0.000 | -16.98 | 0.00   | 313.5 | 0.0   |
| .01    | 7.632    | .558  | 1.210 | .000  | -17.17 | -.00   | 316.7 | .0    |
| .03    | 5.454    | .875  | 1.238 | .001  | -17.64 | -.02   | 324.3 | .3    |
| .06    | 4.180    | 1.109 | 1.284 | .006  | -18.38 | -.10   | 336.5 | 1.5   |
| .10    | 3.340    | 1.277 | 1.342 | .022  | -19.34 | -.34   | 352.3 | 5.4   |
| .15    | 2.756    | 1.393 | 1.402 | .057  | -20.33 | -.90   | 369.0 | 14.3  |
| .21    | 2.338    | 1.466 | 1.440 | .122  | -21.03 | -1.94  | 381.3 | 31.0  |
| .28    | 2.033    | 1.505 | 1.434 | .218  | -21.01 | -3.51  | 382.6 | 56.5  |
| .36    | 1.809    | 1.516 | 1.369 | .335  | -20.05 | -5.44  | 368.5 | 88.3  |
| .45    | 1.646    | 1.505 | 1.254 | .452  | -18.24 | -7.40  | 340.4 | 121.3 |
| .55    | 1.529    | 1.476 | 1.113 | .548  | -15.99 | -9.07  | 304.5 | 150.2 |
| .67    | 1.441    | 1.428 | .963  | .621  | -13.53 | -10.39 | 264.4 | 173.8 |
| .82    | 1.380    | 1.359 | .817  | .665  | -11.10 | -11.26 | 224.0 | 190.7 |
| 1.01   | 1.346    | 1.268 | .692  | .679  | -8.95  | -11.65 | 187.3 | 200.0 |
| 1.25   | 1.341    | 1.157 | .595  | .666  | -7.24  | -11.60 | 157.0 | 202.1 |
| 1.55   | 1.362    | 1.031 | .528  | .634  | -5.98  | -11.20 | 134.0 | 198.1 |
| 1.95   | 1.407    | .889  | .484  | .584  | -5.10  | -10.49 | 116.7 | 188.5 |
| 2.45   | 1.468    | .747  | .462  | .526  | -4.59  | -9.58  | 106.0 | 174.7 |
| 3.05   | 1.535    | .619  | .456  | .466  | -4.38  | -8.59  | 100.5 | 158.3 |
| 3.80   | 1.604    | .501  | .461  | .405  | -4.36  | -7.53  | 98.7  | 139.9 |
| 4.70   | 1.668    | .401  | .471  | .348  | -4.47  | -6.49  | 99.8  | 121.1 |
| 5.80   | 1.727    | .316  | .485  | .296  | -4.67  | -5.49  | 102.6 | 102.3 |
| 7.10   | 1.777    | .247  | .499  | .250  | -4.89  | -4.58  | 106.4 | 84.9  |
| 8.70   | 1.826    | .177  | .512  | .201  | -5.19  | -3.61  | 111.4 | 65.2  |
| 10.70  | 1.866    | .131  | .527  | .163  | -5.46  | -2.86  | 116.4 | 50.7  |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 19  
DRAFT = 32.914 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         |       | SINE  | COSINE  | MOMENT |
|-----------------------|---------|--------|-------------------|---------|-------|-------|---------|--------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |       |         |        |
| .000                  | -32.914 | 2.229  | 1.070             | -32.601 | .2806 | .9598 | -8.121  |        |
| 2.139                 | -32.289 | 2.657  | 2.680             | -31.075 | .9135 | .4068 | -27.298 |        |
| 3.220                 | -29.862 | 2.656  | 3.943             | -28.747 | .8390 | .5441 | -21.975 |        |
| 4.665                 | -27.633 | 2.664  | 5.551             | -26.638 | .7471 | .6647 | -16.211 |        |
| 6.436                 | -25.643 | 2.662  | 7.369             | -24.693 | .7134 | .7007 | -12.454 |        |
| 8.301                 | -23.744 | 2.664  | 9.255             | -22.814 | .6979 | .7162 | -9.293  |        |
| 10.209                | -21.885 | 2.663  | 11.199            | -20.995 | .6685 | .7437 | -5.707  |        |
| 12.189                | -20.105 | 2.663  | 13.227            | -19.269 | .6272 | .7788 | -1.785  |        |
| 14.264                | -18.434 | 2.664  | 15.308            | -17.607 | .6207 | .7841 | 1.075   |        |
| 16.352                | -16.781 | 2.660  | 17.292            | -15.839 | .7076 | .7066 | 1.011   |        |
| 18.232                | -14.898 | 2.663  | 19.161            | -13.944 | .7164 | .6977 | 3.380   |        |
| 20.090                | -12.990 | 2.664  | 21.081            | -12.100 | .6683 | .7439 | 7.595   |        |
| 22.072                | -11.210 | 2.663  | 23.051            | -10.307 | .6781 | .7350 | 9.952   |        |
| 24.029                | -9.404  | 2.664  | 24.979            | -8.470  | .7015 | .7127 | 11.861  |        |
| 25.928                | -7.535  | 2.664  | 26.886            | -6.610  | .6949 | .7191 | 14.739  |        |
| 27.843                | -5.684  | 1.332  | 28.326            | -5.225  | .6892 | .7245 | 16.922  |        |
| 28.808                | -4.766  | 1.332  | 29.291            | -4.307  | .6892 | .7245 | 18.254  |        |
| 29.774                | -3.848  | 2.663  | 30.703            | -2.894  | .7163 | .6978 | 19.353  |        |
| 31.632                | -1.941  | 2.663  | 32.544            | -.970   | .7286 | .6849 | 21.583  |        |
| 33.456                | 0.000   |        |                   |         |       |       |         |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | 1.186  | 0.000  | -4.38    | 0.00     | 167.8  | 0.0    |
| .01             | 5.067    | .358    | 1.195  | .000   | -4.45    | -.00     | 168.4  | .0     |
| .03             | 3.677    | .570    | 1.217  | .001   | -4.63    | -.01     | 170.0  | .0     |
| .06             | 2.847    | .733    | 1.251  | .004   | -4.92    | -.03     | 172.4  | .2     |
| .10             | 2.288    | .857    | 1.297  | .014   | -5.31    | -.11     | 175.9  | .8     |
| .15             | 1.891    | .948    | 1.346  | .038   | -5.76    | -.29     | 180.0  | 2.1    |
| .21             | 1.600    | 1.012   | 1.388  | .084   | -6.17    | -.64     | 184.1  | 4.9    |
| .28             | 1.382    | 1.055   | 1.402  | .156   | -6.41    | -1.23    | 187.2  | 9.6    |
| .36             | 1.217    | 1.080   | 1.374  | .251   | -6.32    | -2.03    | 185.9  | 16.4   |
| .45             | 1.091    | 1.089   | 1.300  | .357   | -5.84    | -2.98    | 185.4  | 24.8   |
| .55             | .996     | 1.086   | 1.193  | .454   | -5.05    | -3.91    | 180.1  | 33.7   |
| .67             | .919     | 1.072   | 1.064  | .536   | -4.02    | -4.78    | 172.3  | 42.6   |
| .82             | .858     | 1.044   | .929   | .592   | -2.85    | -5.51    | 162.7  | 51.1   |
| 1.01            | .813     | 1.002   | .805   | .619   | -1.69    | -6.02    | 152.5  | 58.5   |
| 1.25            | .786     | .945    | .706   | .617   | -.66     | -6.31    | 142.7  | 64.4   |
| 1.55            | .777     | .875    | .635   | .592   | .17      | -6.40    | 133.9  | 68.9   |
| 1.95            | .784     | .789    | .588   | .550   | .85      | -6.30    | 125.9  | 71.9   |
| 2.45            | .805     | .698    | .564   | .499   | 1.33     | -6.06    | 119.3  | 73.1   |
| 3.05            | .836     | .608    | .555   | .445   | 1.64     | -5.71    | 114.4  | 72.5   |
| 3.80            | .872     | .520    | .557   | .391   | 1.83     | -5.28    | 110.9  | 70.1   |
| 4.70            | .909     | .440    | .565   | .341   | 1.92     | -4.80    | 108.7  | 66.1   |
| 5.80            | .945     | .367    | .576   | .294   | 1.95     | -4.28    | 107.8  | 60.6   |
| 7.10            | .978     | .303    | .589   | .254   | 1.93     | -3.76    | 107.8  | 54.2   |
| 8.70            | 1.008    | .245    | .602   | .218   | 1.90     | -3.22    | 108.4  | 46.9   |
| 10.70           | 1.034    | .193    | .614   | .186   | 1.87     | -2.69    | 109.2  | 39.3   |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING - 5 COEFFICIENTSSTATION 20  
DRAFT = 32.932 FEET

| ENDPOINTS OF SEGMENTS |         |        | SEGMENT MIDPOINTS |         | SINE  | COSINE | MOMENT  |
|-----------------------|---------|--------|-------------------|---------|-------|--------|---------|
| H-BRDTH               | HEIGHT  | LENGTH | H-BRDTH           | HEIGHT  |       |        |         |
| .000                  | -21.908 | 1.809  | .904              | -21.908 | .0000 | 1.0000 | .904    |
| 1.809                 | -21.908 | 1.718  | 2.650             | -21.734 | .2032 | .9791  | -1.823  |
| 3.491                 | -21.559 | 1.797  | 3.940             | -20.781 | .8660 | .5000  | -16.027 |
| 4.389                 | -20.003 | 1.809  | 4.837             | -19.217 | .8692 | .4944  | -14.313 |
| 5.284                 | -18.431 | 1.809  | 5.734             | -17.647 | .8672 | .4980  | -12.447 |
| 6.184                 | -16.862 | 1.806  | 6.708             | -16.126 | .8151 | .5793  | -9.258  |
| 7.231                 | -15.390 | 1.809  | 7.774             | -14.667 | .7996 | .6005  | -7.060  |
| 8.317                 | -13.944 | 1.808  | 8.876             | -13.233 | .7859 | .6184  | -4.910  |
| 9.435                 | -12.523 | 1.809  | 10.009            | -11.824 | .7727 | .6348  | -2.782  |
| 10.583                | -11.125 | 1.807  | 11.171            | -10.439 | .7597 | .6503  | -.666   |
| 11.758                | -9.752  | 1.809  | 12.411            | -9.126  | .6923 | .7217  | 2.639   |
| 13.064                | -8.500  | 1.809  | 13.716            | -7.874  | .6923 | .7217  | 4.447   |
| 14.369                | -7.248  | 1.809  | 15.030            | -6.631  | .6824 | .7310  | 6.462   |
| 15.691                | -6.014  | 1.809  | 16.359            | -5.404  | .6742 | .7385  | 8.438   |
| 17.027                | -4.795  | 1.809  | 17.695            | -4.185  | .6742 | .7385  | 10.247  |
| 18.363                | -3.575  | 1.809  | 19.043            | -2.979  | .6592 | .7520  | 12.356  |
| 19.723                | -2.383  | 1.809  | 20.405            | -1.789  | .6567 | .7542  | 14.214  |
| 21.087                | -1.195  | .904   | 21.426            | -.896   | .6609 | .7505  | 15.488  |
| 21.765                | -.598   | .904   | 22.105            | -.299   | .6609 | .7505  | 16.392  |
| 22.444                | 0.000   |        |                   |         |       |        |         |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | .590   | 0.000  | -.93     | 0.00     | 30.9   | 0.0    |
| .01             | 2.440    | .160    | .593   | .000   | -.95     | -.00     | 31.0   | .0     |
| .03             | 1.824    | .260    | .600   | .000   | -.98     | -.00     | 31.1   | .0     |
| .06             | 1.446    | .342    | .611   | .001   | -1.03    | -.00     | 31.4   | .0     |
| .10             | 1.183    | .409    | .627   | .003   | -1.10    | -.01     | 31.7   | .0     |
| .15             | .990     | .461    | .647   | .009   | -1.19    | -.03     | 32.1   | .1     |
| .21             | .843     | .502    | .667   | .021   | -1.29    | -.08     | 32.6   | .3     |
| .28             | .730     | .534    | .686   | .041   | -1.39    | -.16     | 33.1   | .6     |
| .36             | .641     | .556    | .698   | .073   | -1.47    | -.29     | 33.6   | 1.1    |
| .45             | .570     | .572    | .696   | .115   | -1.50    | -.47     | 33.9   | 1.9    |
| .55             | .514     | .581    | .679   | .166   | -1.47    | -.70     | 34.0   | 3.0    |
| .67             | .465     | .586    | .642   | .224   | -1.36    | -.98     | 33.8   | 4.3    |
| .82             | .423     | .584    | .585   | .283   | -1.15    | -1.30    | 33.1   | 6.0    |
| 1.01            | .388     | .576    | .514   | .333   | -.85     | -1.61    | 31.9   | 7.8    |
| 1.25            | .360     | .560    | .443   | .365   | -.52     | -1.86    | 30.5   | 9.5    |
| 1.55            | .341     | .536    | .381   | .376   | -.20     | -2.04    | 28.9   | 11.1   |
| 1.95            | .329     | .502    | .332   | .368   | .08      | -2.15    | 27.3   | 12.6   |
| 2.45            | .327     | .461    | .300   | .347   | .31      | -2.18    | 25.8   | 13.7   |
| 3.05            | .331     | .416    | .281   | .319   | .48      | -2.16    | 24.6   | 14.6   |
| 3.80            | .341     | .369    | .272   | .287   | .60      | -2.09    | 23.4   | 15.1   |
| 4.70            | .354     | .323    | .269   | .255   | .69      | -1.98    | 22.5   | 15.3   |
| 5.80            | .369     | .277    | .271   | .223   | .73      | -1.83    | 21.7   | 15.1   |
| 7.10            | .384     | .236    | .275   | .193   | .75      | -1.67    | 21.2   | 14.4   |
| 8.70            | .400     | .197    | .280   | .165   | .75      | -1.48    | 20.8   | 13.4   |
| 10.70           | .415     | .161    | .287   | .140   | .74      | -1.28    | 20.6   | 12.0   |

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SL-7 - NORMAL FULL LOAD DEPARTURE  
CONFORMAL MAPPING -5 COEFFICIENTS

STATION 21  
DRAFT = 32.950 FEET

| ENDPOINTS OF SEGMENTS |        |        | SEGMENT MIDPOINTS |        |        | SINE   | COSINE | MOMENT |
|-----------------------|--------|--------|-------------------|--------|--------|--------|--------|--------|
| H-BRDTH               | HEIGHT | LENGTH | H-BRDTH           | HEIGHT |        |        |        |        |
| .000                  | -6.703 | .673   | .337              | -6.703 | 0.0000 | 1.0000 | .337   |        |
| .673                  | -6.703 | .673   | 1.010             | -6.703 | 0.0000 | 1.0000 | 1.010  |        |
| 1.347                 | -6.703 | .337   | 1.515             | -6.703 | .0000  | 1.0000 | 1.515  |        |
| 1.684                 | -6.703 | .337   | 1.852             | -6.703 | .0000  | 1.0000 | 1.852  |        |
| 2.020                 | -6.703 | .664   | 2.274             | -6.489 | .6456  | .7637  | -2.453 |        |
| 2.527                 | -6.275 | .673   | 2.776             | -6.048 | .6742  | .7385  | -2.027 |        |
| 3.025                 | -5.821 | .673   | 3.273             | -5.594 | .6742  | .7385  | -1.354 |        |
| 3.522                 | -5.367 | .673   | 3.771             | -5.140 | .6742  | .7385  | -.680  |        |
| 4.020                 | -4.913 | .673   | 4.268             | -4.685 | .6742  | .7385  | -.007  |        |
| 4.517                 | -4.458 | .673   | 4.766             | -4.231 | .6742  | .7385  | .667   |        |
| 5.014                 | -4.004 | .673   | 5.263             | -3.777 | .6742  | .7385  | 1.340  |        |
| 5.512                 | -3.550 | .673   | 5.763             | -3.327 | .6637  | .7480  | 2.103  |        |
| 6.015                 | -3.103 | .673   | 6.268             | -2.881 | .6596  | .7517  | 2.811  |        |
| 6.521                 | -2.659 | .673   | 6.775             | -2.437 | .6596  | .7517  | 3.485  |        |
| 7.028                 | -2.215 | .673   | 7.281             | -1.993 | .6596  | .7517  | 4.158  |        |
| 7.534                 | -1.771 | .673   | 7.787             | -1.549 | .6596  | .7517  | 4.831  |        |
| 8.040                 | -1.327 | .673   | 8.293             | -1.105 | .6596  | .7517  | 5.505  |        |
| 8.546                 | -.883  | .673   | 8.799             | -.661  | .6596  | .7517  | 6.178  |        |
| 9.052                 | -.439  | .673   | 9.308             | -.219  | .6512  | .7589  | 6.921  |        |
| 9.563                 | 0.000  |        |                   |        |        |        |        |        |

| FREQ.<br>PARAM. | A'<br>33 | N'<br>Z | M<br>S | N<br>S | M<br>S.R | N<br>S.R | I<br>R | N<br>R |
|-----------------|----------|---------|--------|--------|----------|----------|--------|--------|
| .00             | INFINITY | 0.000   | .057   | 0.000  | -.20     | 0.00     | .9     | 0.0    |
| .01             | .537     | .030    | .057   | .000   | -.20     | -.00     | 1.0    | .0     |
| .03             | .426     | .050    | .058   | .000   | -.20     | -.00     | 1.0    | .0     |
| .06             | .356     | .067    | .058   | .000   | -.20     | -.00     | 1.0    | .0     |
| .10             | .305     | .083    | .059   | .000   | -.21     | -.00     | 1.0    | .0     |
| .15             | .265     | .097    | .059   | .000   | -.21     | -.00     | 1.0    | .0     |
| .21             | .234     | .109    | .060   | .000   | -.21     | -.00     | 1.0    | .0     |
| .28             | .208     | .120    | .061   | .001   | -.22     | -.00     | 1.0    | .0     |
| .36             | .187     | .129    | .062   | .001   | -.22     | -.00     | 1.0    | .0     |
| .45             | .169     | .137    | .064   | .002   | -.23     | -.01     | 1.1    | .0     |
| .55             | .154     | .143    | .065   | .003   | -.23     | -.01     | 1.1    | .1     |
| .67             | .141     | .149    | .066   | .005   | -.24     | -.02     | 1.1    | .1     |
| .82             | .128     | .154    | .067   | .008   | -.24     | -.03     | 1.1    | .1     |
| 1.01            | .115     | .159    | .068   | .013   | -.25     | -.05     | 1.2    | .2     |
| 1.25            | .104     | .162    | .068   | .020   | -.25     | -.08     | 1.2    | .3     |
| 1.55            | .094     | .164    | .066   | .029   | -.24     | -.12     | 1.1    | .5     |
| 1.95            | .085     | .164    | .061   | .040   | -.22     | -.17     | 1.1    | .7     |
| 2.45            | .078     | .162    | .054   | .051   | -.19     | -.21     | .9     | .9     |
| 3.05            | .073     | .157    | .047   | .058   | -.16     | -.25     | .8     | 1.1    |
| 3.80            | .069     | .151    | .040   | .063   | -.13     | -.27     | .7     | 1.2    |
| 4.70            | .067     | .142    | .035   | .064   | -.11     | -.29     | .6     | 1.3    |
| 5.80            | .067     | .131    | .030   | .063   | -.09     | -.29     | .5     | 1.3    |
| 7.10            | .067     | .120    | .028   | .060   | -.08     | -.28     | .4     | 1.3    |
| 8.70            | .068     | .107    | .026   | .056   | -.07     | -.27     | .4     | 1.3    |
| 10.70           | .071     | .094    | .025   | .052   | -.06     | -.25     | .3     | 1.2    |